PHILOSOPHICAL TRANSACTIONS.

VII. Contributions to Terrestrial Magnetism.—No. VI.

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§ 10. Observations made on Board Her Majesty's Ships Erebus and Terror, from June 1841 to August 1842, in the Antarctic Expedition under the command of Captain Sir James Clark Ross, R.N., F.R.S.

I HAVE now to lay before the Royal Society the results of the Magnetic Observations made at sea by the Antarctic Expedition during the second year of its operations in the southern hemisphere. Leaving Hobarton early in July 1841, the ships proceeded in the first instance to Sydney in Australia, and from thence to the Bay of Islands in New Zealand, where they remained until the return of the season of navigation in the high latitudes. Quitting New Zealand in November, the ice was met with and entered in a somewhat lower latitude than in the preceding year, and in a longitude considerably to the east of the former track. The obstacles which the ice presented to their progress appear to have been greater than on the former occasion; they were however surmounted, and in February 1842 the ships again reached the ice barrier, or glacier, in latitude 78°, by which they had been stopped in the preceding year. After an unsuccessful endeavour to turn the eastern extremity of the glacier, the advance of the season compelled their return to the lower latitudes; they quitted the Antarctic Circle in March 1842, and keeping nearly in the 60th parallel, crossed the whole breadth of the southern Pacific Ocean to the Falkland Islands, where they arrived in April.

I proceed at once to the examination in detail of the magnetic observations made during this period.

MDCCCXLIV.

Deductions of the Constants a and b in the Corrections for the Ship's attraction.

1. In the Erebus.—For the constants a and b to be employed in computing the corrections of the declination, we have the observations on each of the 32 principal points of the compass at Hobarton, in October 1840 and June 1841. We have also a similar series at Port Louis, in the Falkland Islands, in August 1842. The observations at Hobarton have been already discussed in No. V.* Those at Port Louis were as follows:—

Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.
N. N. by w. N.N.W. N.W. by N. N.W. N.W. by w. W.N.W. W. by N.	+ 0 12·7 -0 04·1 -0 33·6 -0 50·1 -1 02·3 -1 00·6 -1 49·3 -2 09·6	w. w. by s. w.s.w. s.w. by w. s.w. s.w. s.w. s.s.w. s.s.w. s.s.by w.	-2 15·8 -2 21·2 -2 21·3 -2 4·3 -1 8·0 -1 3·3 -1 17·3 -0 38·6	s. by E. s.s.e. s.e. by s. s.e. s.e. by e. e.s.e. by e. e.s.e. by s.	+ 0 00·1 + 0 43·9 + 1 12·7 + 1 41·4 + 1 55·5 + 2 06·9 + 2 18·9 + 2 16·4	E. by N. E.N.E. by E. N.E. by N. N.E. by N. N.N.E.	+2 07·4 +1 54·0 +1 44·0 +1 16·5 +0 50·9 +0 40·5 +0 41·2 +0 27·7

August 19, 1842.

The values of the constants deduced from the observations at Hobarton were, a=+.0272; b=+.986. The values from the observations at the Falkland Islands are, a=+.0292; b=+.984.

The values of a at Hobarton were derived from two series, one in October 1840, when the ship had recently passed through the low magnetic latitudes, and the other in June 1841, on her return from the highest magnetic latitudes of the southern hemisphere; the two series separately considered give a=+.0235 in 1840, and .0309 in 1841; we have therefore the following values:—

- +·0267 in the Thames, where the ship had been stationary for several years.
- +·0235 at Hobarton, on her first arrival from the low latitudes.
- +:0305 on her return to Hobarton from the very high southern magnetic latitudes.
- +·0292 at the Falkland Islands in 1842, on her second return from the very high southern latitudes.

The variations in these values is in accordance with the view expressed in the preceding Number of these Contributions \uparrow , that when a ship changes her magnetic latitude, the corresponding change in the induced portion of her magnetism may not be instantaneous; that some portions of her iron may be of a quality intermediate between perfectly soft iron, which would undergo instantaneous change, and iron permanently magnetic; and that when changing rapidly her geographical position, she may be liable to be more or less in arrear, in regard to her magnetic condition, of her actual locality at any particular time. In a ship in which this should be the case, a table computed with any one value of a would not apply equally to one portion

^{*} Philosophical Transactions, 1843, Part II. pp. 152-154.

of her voyage in which she might be sailing from lower into higher inclinations, and to another portion in which she might be returning from higher into lower magnetic latitudes. The voyage under consideration comprised two such portions; and I have therefore employed two tables for the Erebus, one computed with 0267 for the period when the ship was increasing the dip, and the other with 0288 for the period when she was decreasing the dip. The differences are insignificant, except when the inclination is very high; the greater part of the declinations observed in the high dips were antecedent to the 1st of March 1842, when the ship commenced her return to the lower latitudes; for these the table computed with a=0267 has been employed, and appears to answer better than the corrections computed either by the values resulting from the observations at Hobarton before the commencement, or by those at the Falkland Islands after the conclusion of the voyage.

2. In the Terror.—For the values of a and b in the Terror, we have observations on each of the thirty-two principal points of the compass at Hobarton in October 1840, and a second series in June 1841, as follows:—

Ship's head by	Disturban	ce towards	the west.	Ship's head by	Disturbance towards the west.			
compass.	1840.	1841.	Mean.	compass.	1840.	1841.	Mean.	
N. by W. N.N.W. N.W. by N. N.W. by W. W.N.W. W. by N. W. W. by S. W.S.W. S.W. by W. S.W. S.W.	+ 0 42.4 -0 23.6 -1 20.6 -2 20.6 -3 25.6 -3 56.6 -4 01.6 -4 44.6 -4 42.6 -4 23.6 -3 23.6 -3 23.6 -1 37.6	-0 52 -0 59 -0 03 -0 58 -2 12 -2 26 -2 51 -3 34 -3 43 -4 34 -4 01 -3 50 -4 22 -3 41	-1 10 -1 12 -2 12 -3 04 -3 14 -3 29 -4 06 -4 14	E. E. by N. E.N.E. N.E. by E. N.E. N.E. by N.	-0 11.6 +0 52.4 +1 56.4 +2 38.4 +3 19.4 +4 00.4 +4 43.4 +4 24.4 +4 11.4 +3 27.4 +3 02.4 +3 03.4 +2 11.4 +1 26.4	-0 06 +0 43 +2 08 +2 57 +3 48 +5 25 +4 58 +4 27 +4 02 +3 27 +3 04 +3 01	-0 33 +0 23 +1 20 +2 23 +3 08 +3 54 +4 4 4 +4 4 4 +4 07 +3 16 +3 08 +2 33 +1 29 +0 37	

We have also a series at Port Louis, in the Falkland Islands, in August 1842, as follows:—

Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.
N. by w. N.N.W. N.W. by N. N.W. by N. W.W. by W. W.N.W. W. by N.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	w. w. by s. w.s.w. s.w. by w. s.w. s.w. s.w. s.w. s.s.w. s.s.w. s. by w.	-2 30 -2 21 -2 12 -2 21 -1 33 -1 05 -0 47 -0 45	s. by E. s.s.e. by E. s.e. by E. s.e. by E. e.s.e. by E. E.s.e. by s.	-0 16 -0 08 0 00 +0 47 +1 35 +2 17 +3 04 +2 33	E. by N. E.N.E. N.E. by E. N.E. by N. N.N.E. N. by E.	$\begin{array}{c} +2 & 46 \\ +2 & 27 \\ +1 & 58 \\ +1 & 39 \\ +1 & 13 \\ +1 & 11 \\ +0 & 34 \\ +0 & 27 \end{array}$

From these observations we have the following values of the constants:—

Hobarton
$$a=+.0275$$
; $b=+.979$
Falkland Islands . . . $a=+.0293$; $b=+.994$.

These values are nearly the same as those derived from the observations in the Erebus at the same periods, and appear to require no special remark; the same tables have been employed in the declination corrections of both ships during the voyage under notice; the values of the constants in these tables were as follows:—

a=.0267 when the ships were sailing from the lower into the higher latitudes; a=.0288 when sailing from the higher into the lower latitudes; b=+.984 in both cases.

Deduction of the Corrections on account of the Ship's attraction for the Observations of Inclination.

1. In the Erebus.—The spot in the ship in which Mr. Fox's apparatus for the observations of inclination and intensity was employed, was a few feet in advance (towards the bow), and about two feet lower in height, than the position of the standard compass.

The values of a and b derived from the observations with the compass needle apply in strictness only to the spot in which that compass was stationed; it may be proper, therefore, before we employ them for the observations with Mr. Fox's apparatus, to show that nearly similar values for the constant a in particular (the more important constant) are deducible from the observations of inclination and intensity, independently of those made with the compass needle. For this purpose we may employ equation (1.), Phil. Trans., 1843, Part II. p. 147, viz.

$$\frac{\varphi'}{\Lambda'\varphi}\cos\theta'\cos\zeta' = \cos\theta\cos\zeta + a\sin\theta,$$

obtaining by its means the value of a from the observations of inclination and intensity made at Hobarton and Port Louis. As A' is known to differ very slightly, if at all, from unity, we have from equation (1.),

$$a \sin \theta = \frac{\varphi'}{\varphi} \cos \theta' \cos \zeta' - \cos \theta \cos \zeta.$$

 φ and θ are furnished by the mean of the observations of inclination and intensity on the sixteen points of the compass, having approximate corrections applied to each of them; φ' and θ' by the (uncorrected) observations on the different points.

From the general aspect of the observations at both stations, we may conclude that the same symmetrical distribution of the iron existed in reference to the position of Mr. Fox's apparatus as in the case of the standard compass, and consequently that at the north and south points the value of ζ' and ζ coincided, being equal in the one case to 0°, and in the other to 180°. At Hobarton (in June 1841) we have $\varphi = 1.83$, $\theta = -70^{\circ} 39'$; φ' at north 1.812, at south 1.854; θ' at north $-71^{\circ} 56'$, at south $-69^{\circ} 14'$:

Hence

at north,
$$-.944a = +.307 - .331$$
 at south, $-.944a = -.359 + .331$; whence $a = +.0275$.

At Port Louis (August 1842) we have $\varphi = 1.32$; $\theta = -52^{\circ} 05'$; φ' at north = 1.279, at south = 1.346; θ' at north = -52° 50′, at south = -51° 33; hence

at north,
$$-.789a = +.5920 - .615$$
 at south, $-.788a = -.6367 + .615$; whence $a = +.0310$.

The accordance between these values and those deduced from the observations with the standard compass is fully sufficient to justify the inference that the effect of the ship's attraction was very nearly the same at the spot where Mr. Fox's apparatus was used, as at that at which the standard compass was fixed.

We may obtain c either by equation (11.), Phil. Trans., 1843, Part II. p. 148,

$$c\cos\zeta + d\tan\theta = \sqrt{(\cos\zeta + a\tan\theta)^2 + b^2\sin^2\zeta}$$
. $\tan\theta'$;

or from the observations of inclination and intensity, independently of the values of a and b, by the equation

$$\frac{\varphi'}{\varphi}\sin\theta' = c\cos\theta\cos\zeta - d\sin\theta.$$

Confining ourselves to the north and south points, and to those points on either side of N, and S, from which c may be most advantageously derived, the observations at Hobarton give the following values to be employed in the equations:

N.;
$$\zeta'=0$$
; $\zeta=0$; $\theta'=-71^{\circ} \, 56'$; $\varphi'=1.812$.

N.N.E. $\{N.N.E.\}$; $\{\zeta'=22^{\circ} \, 30'$; $\{\zeta=21^{\circ} \, 03'\}$; $\{\theta'=-71^{\circ} \, 55'\}$; $\{\varphi'=1.812\}$.

N.E. $\{N.W.\}$; $\{\zeta'=45^{\circ} \, 0'\}$; $\{\zeta=42^{\circ} \, 12'\}$; $\{\theta'=-71^{\circ} \, 48'\}$; $\{\varphi'=1.816\}$.

S.E. $\{N.W.\}$; $\{\zeta'=135^{\circ} \, 0'\}$; $\{\zeta=131^{\circ} \, 17'\}$; $\{\theta'=-69^{\circ} \, 56'\}$; $\{\varphi'=1.847\}$.

S.S.E. $\{N.W.\}$; $\{\zeta'=157^{\circ} \, 30'\}$; $\{\zeta=155^{\circ} \, 24'\}$; $\{\theta'=-69^{\circ} \, 38'\}$; $\{\varphi'=1.850\}$.

S; $\{\zeta'=180^{\circ} \, 0'\}$; $\{\zeta=180^{\circ} \, 0'\}$; $\{\varphi'=1.854\}$.

 $\{\theta=-70^{\circ} \, 39'\}$; $\{\varphi=1.83\}$.

Substituting these values in the first of the above equations (11.), we have at

N.
$$1.000c - 2.85d = -2.828$$
;
N.N.E. $934c - 2.85d = -2.832$;
N.E. $N.W.$ $741c - 2.85d = -2.841$;
S.E. $S.W.$ $-3.660c - 2.85d = -2.853$;

S.S.E.
$$S.S.W.$$
 $\left\{ \begin{array}{l} -.909c - 2.85d = -2.876; \\ S.S.W. \end{array} \right\}$

Changing the signs of the three last equations, and summing, we have

$$5.24c = +.071$$
; whence $c = +.014$.

To obtain c from the observations of inclination and intensity alone, we have at

N.
$$\cdot 331c - \cdot 94d = -\cdot 941$$
;
N.N.E. $\cdot 309c - \cdot 94d = -\cdot 942$;
N.E. $\cdot 222c - \cdot 94d = -\cdot 943$;
S.E. $\cdot 218c - \cdot 94d = -\cdot 948$;
S.S.E. $\cdot 301c - \cdot 94d = -\cdot 948$;
S. $\cdot 31c - \cdot 94d = -\cdot 947$.

Changing the signs of the three last equations, and summing, d is eliminated as before, and

$$c = \frac{+.017}{1.71} = +.010.$$

From the observations at Port Louis, we have the following values to be employed in the equations:

N.
$$\zeta'=0$$
; $\zeta=0$; $\theta'=-52^{\circ} 50'$; $\varphi'=1\cdot279$;
N.N.E. $\Sigma'=0$; $\Sigma'=$

Substituting these values in equation (11.), we obtain

$$c = \frac{+.094}{5.24} = +.018;$$

or from the observations of inclination and intensity alone,

$$c = \frac{+.051}{3.22} = +.016.$$

The correspondence in the value of the constants obtained from the observations at Hobarton and Port Louis, being the commencing and concluding stations of the voyage new under consideration, is fully as good as could be desired; and a table formed from them has been employed for the correction of the observations made between Hobarton and the Bay of Islands, and during the return of the Expedition from the high latitudes to the Falkland Islands commencing with the 1st of March 1842. In those portions of the voyage the ship was passing from the higher to the lower magnetic latitudes, in which circumstance they corresponded with the observations at Hobarton and Port Louis, which were both made on the return from the vicinity of the magnetic pole. But if we attempt to apply the same table to the observations made under the reverse circumstances, namely, when the ship was passing from the lower to the higher latitudes (and such was the case with the greater part of the observations which we have to correct in the present voyage), we find that the tabular numbers, where the N. and S. points are approached, furnish a decided over compen-On days when observations have been made at or near the N. and S. points, if we seek in the table for the corrections which should bring the results in accord with each other, we find that the corrections which will do so belong to a dip which is always some degrees less than the true terrestrial dip. It appeared desirable, therefore, if possible, to form a table for the correction of the observations of this portion of the voyage, derived from those observations themselves. Fortunately we have a better opportunity of doing this than might have been anticipated. The progress of the Expedition was so much impeded by ice in the early part of January 1842, that from the 6th to the 16th inclusive, the Erebus was the whole time between the latitudes of -65° 54' and -66° 14', and between the longitudes of 204° 33' and 202° 02'; the weather and all other circumstances being favourable, the inclination was observed in the course of those eleven days with the ship's head on seventeen different points of the compass, sufficiently distributed, and particularly towards the north points and south points, where the effect of the ship's attraction is greatest, and is in opposite directions. From the observations at north and south it is not difficult to obtain an approximate value of a, which should bring the corrected results at those points into accord. The value thus obtained is about + 023. I have collected the observations during the period referred to into the following table, taking, for the sake of simplicity, only those observations which were made by the direct method, which, however, comprises by far the greater part of the observations of that period. I have then computed the corrections, first, with the values of the constants, such as they are given by the observations made for their determination at Hobarton and the Falkland Islands (being the commencement and close of the voyage), viz. a = +.028; b = +.984; c = +.015 and d = 1; and second, with a = +.023, b, c and d, as before; and have placed the two series of corrected results in the table, with columns showing in both cases the difference of the corrected result, on each point, from the mean result. A comparison of those columns seems conclusive in favour of the application

of the smaller value of a to those observations which were made when the saip was in progress from the lower to the higher latitudes. If a be taken as it was found at Hobarton and the Falkland Islands, not only are the differences generally greater, but they are systematically so; evidencing an over compensation where the north and south points are approached; whilst with the smaller value of a the differences are greatly diminished in amount, and exhibit no appearance whatsoever of system. They are such as may well be supposed to have been occasioned partly by observation error, and partly by small differences of geographical position in which the observations themselves were made.

Ship's head	Number	Inclination	a	of the Const c = +.028. ; $c = +.015$		0	of the Const a = +.023. ; $c = +.015$	
by compass.	vations.	observed.	Computed corrections.	Inclinations corrected.	α-β.	Computed corrections.	Inclinations corrected.	α-β.
N. N.N.E. N.W. N.E. by E. W. E. E. by S.	1 2 2 3 2 1 3	-80 58 -81 00 -80 42 -80 35 -80 50 -79 58 -79 50 -79 45	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	β. - 79 26 - 79 33 - 79 30 - 79 23 - 79 49 - 79 41 - 79 33 - 79 46	$ \begin{array}{r} -20 \\ -13 \\ -26 \\ -23 \\ +3 \\ -5 \\ -13 \\ -00 \\ \end{array} $	+ 1 16 +1 12 +1 00 +1 00 +0 55 +0 14 +0 14 -0 01	β. -79 42 -79 48 -79 42 -79 35 -79 55 -79 44 -79 36 -79 46	$ \begin{array}{rrrr} & -3 \\ & +3 \\ & -3 \\ & -10 \\ & +10 \\ & -1 \\ & -9 \\ & +1 \end{array} $
s.w. by w. s.w. \frac{3}{4} w. s.w. \frac{1}{2} w. s.e. s.w. s.w. \frac{1}{2} s. s.s.e. s. by w. s.	3 1 1 3 1 3 5	-79 19 -79 30 -79 10 -79 08 -78 52 -78 48 -78 28 -78 28 -78 32	-0 38 -0 42 -0 46 -0 55 -0 55 -1 02 -1 13 -1 29 -1 31	-79 57 -80 12 -79 56 -80 03 -79 47 -79 50 -79 41 -79 57 -80 03	$+11 \\ +26 \\ +10 \\ +17 \\ +1 \\ +4 \\ -5 \\ +11 \\ +17$	-0 31 -0 34 -0 38 -0 45 -0 45 -0 50 -1 05 -1 13 -1 14	-79 50 -80 04 -79 48 -79 53 -79 37 -79 38 -79 33 -79 46	$ \begin{array}{r} + 5 \\ + 19 \\ + 3 \\ + 8 \\ - 8 \\ - 7 \\ - 12 \\ - 2 \\ + 1 \end{array} $
Means	36			$-79 \ 4$	6=a		$-79 \ 4$	$5=\alpha$

The mean of the observations in the table thus corrected is -79° 45'; the corresponding geographical position is -66° 04', and 203° 17'.5, if we take as such the middle point of the geographical space in which the ship was detained from the 6th to the 16th of January. The inclination observed on the ice on the 16th of January, in lat. -65° 49', long. 202° 02', with needles whose poles were reversed, was -79° 39'.5. We can derive no precise conclusion in regard to the value of d, from observations which are not identical in locality; but the accordance of the results obtained on board and on the ice, in geographical positions so little different, is quite sufficient to show that the error involved by assuming d as unity must be, at the utmost, very inconsiderable.

The tables for the correction of the inclination in the Erebus have therefore been computed with the following values for the constants, viz. from New Zealand to the end of February 1842, being the portion of the voyage in which the ship was in pro-

gress from the lower into the higher inclinations, a=+.023, b=+.984, c=+.015 and d=1: and for the remainder of the voyage a=+.028, b, c and d, as before.

In the Terror.—The place in which Mr. Fox's apparatus was used in the Terror was about the same distance from the position of the standard compass, and in the same direction, as in the Erebus. A series of observations were made with it for the purpose of furnishing materials for the determination of the constants, at Hobarton in June 1841, and at the Falkland Islands in August 1842; and the inclination was also observed with the ship's head on several points of the compass during the detention of the ships by the ice between the 6th and 16th of January 1842. In the case of the Erebus, we have found these latter observations of principal use in furnishing the values of the constants which apply to the greater part of the observations of the voyage; it may, therefore, be advisable to commence with the discussion of the corresponding series in the Terror.

Inclinations observed on board Her Majesty's ship Terror with needle F.C.B. used direct, during her detention by the ice from the 6th to the 16th of January 1842, between the latitudes of -65° 45' and -66° 20', and longitudes of 201° 46' and 204° 04'.

Ship's head by compass.	Number of observations.	Inclination observed.	Ship's head by compass.	Number of observations.	Inclination observed.
N. N. $\frac{1}{2}$ E. N. $\frac{5}{4}$ E. N.N.E. N.E. by E. E. $\frac{1}{2}$ N. E. E. by S. E. S.E. S.S.E. S. by E.	4 2 1 3 2 1 1 6 1 1 2 1 1	-81 19·5 -81 14 -80 50 -80 57 -80 48 -80 26 -79 57 -79 45 -79 33 -79 21 -79 04 -78 42 -78 37	s. s. \frac{3}{4} w. s. by w. s.w.by w. \frac{1}{2} w. s.w. by s. s.w. \frac{1}{2} w. s.w.by w. w.s.w. w. by s. w. \frac{1}{4} s. n.w. n. by w.	6 1 1 3 3 1 5 2 1 2 2	-78 30 -78 21 -78 48 -78 50 -79 00 -79 08 -79 08 -79 37 -80 05 -80 07 -81 09 -81 15

These observations manifest the general systematic character of the disturbance occasioned by the ship's attraction; they furnish indeed a remarkable example of the success with which the effect of the ship's iron on the inclination may be investigated by observations made at sea. The disturbance appears to have not been strictly symmetrical, inasmuch as the inclinations observed on the western points somewhat exceed in amount those observed on the corresponding eastern points; the same circumstance took place in the observations at Hobarton; but at the Falkland Islands, on the contrary, the inclinations observed on the eastern points were generally somewhat the higher. A similar occasional departure from strict symmetry has before been noticed in the effect of the ship's iron on the compass needle*; in that case also

^{*} Philosophical Transactions, 1843, Part II. p. 152.

the disturbance in the same ship was sometimes greater on the eastern, and sometimes on the western points; these small irregularities, having no uniform character, are regarded as included amongst those varying accidents which are classed generally under the name of observation error. It is proper, however, in consequence of this occasional irregularity, that the data from which constants are to be derived for general corrections should consist of the mean of observations on corresponding points on the east and west sides of the compass; in this view we have as available observations in the preceding table those on the following points of the compass.

North													81	19.5
N.W.			•			•.,	•						}-80	50.5
$W_{\cdot \frac{1}{4}} S_{\cdot \cdot}$		•			•		•		•	•,		•		50.5
$E_{-\frac{1}{4}}S_{-\frac{1}{4}}$	(fro	m	E . :	anc	lΕ	$\cdot \frac{1}{2}$	S.)	٠	•				} -79	90 B
W. by S	.		•		•								70	40
E. by S.			•									•		49
W.S.W.	•			•							•	•	70	00
E.S.E.	•	•										•		29
S.E. (fr	om	E	.S.I	E. a	and	S.	S.E	(.)						04.9
South	•	•	•					•	•	•	•		78	30

We have here 2° $49'\cdot 5$ for the difference between the inclinations observed with the ship's head north and south; the value of a which will give that amount for the sum of the corrections at north and south when the dip is between -79° and -80° , (neglecting c as too small in such case to require consideration), is about $+\cdot 026$. The observations at north were four in number,—those at south six, and on different days,—they were as follows:—

North.	South.					
January 8, -81 19	January 7, $-\mathring{7}8$ 28					
8, -81 20	8, -78 31					
8, -81 18	11, -78 28					
13, -81 21	13, -78 25					
What are 1 and 1 a	13, -78 33					
Mean 81 19.5	14, -78 34					
	Mean 78 30					

From the accord which these observations respectively exhibit, it is clear that we should not be justified in taking a value of a which should differ much from $+\cdot026$.

If we now refer to the observations which were made in the Terror soon after her arrival at the Falkland Islands, when the ship's head was placed on the principal points of the compass for the purpose of determining the values of the constants, we shall

find that a value of a taken near $+ \cdot 026$ will by no means bring the results on the N. and S. points, or on those approaching the N. and S. points, into accord; and that as we have already found in the dip corrections of the Erebus, and in the declination corrections of both ships, a considerably higher value of α is required for the observations on the return from the high latitudes, than for those when the ship was in progress from the lower to the higher dips.

We have no observations at the Falkland Islands (made at the spot in the ship where Mr. Fox's apparatus was used) either of the direction of the compass needle, or of the force acting on the horizontal needle: we must therefore obtain a and b directly from the observations of Inclination and Intensity. The observations gave as follows:--

Ship's head.	Inclination observed. $\theta = -51^{\circ} 56'$.	Intensity observed. $\varphi = 1.336$.		
	ď	φ'		
N. N.N.E. N.N.W. N.E. N.W. E.N.E. W.N.W.	$ \begin{vmatrix} -52 & 46 \cdot 5 & -52 & 46 \cdot 5 \\ -52 & 51 \\ -52 & 43 \end{vmatrix} -52 & 47 \\ -52 & 47 \\ -52 & 45 \end{vmatrix} -52 & 46 \\ -52 & 52 \\ -52 & 38 \end{vmatrix} -52 & 45 \\ -52 & 31 $	$ \begin{array}{ccc} 1.320 & 1.320 \\ 1.315 & 1.314 \\ 1.313 & 1.313 \\ 1.312 & 1.313 \\ 1.336 & 1.322 \\ 1.336 & 1.322 \\ 1.336 & 1.332 \end{array} $		
W. E.S.E. W.S.W. S.E. S.W. S.S.E. S.S.W.	$ \begin{vmatrix} -52 & 13 \\ -52 & 16 \\ -51 & 46 \end{vmatrix} -52 & 01 $ $ \begin{vmatrix} -51 & 32 \\ -51 & 32 \end{vmatrix} -51 & 32 $ $ \begin{vmatrix} -51 & 09 \\ -51 & 21 \end{vmatrix} -50 & 53 & -50 & 53 $	$ \begin{vmatrix} 1.334 \\ 1.355 \\ 1.355 \\ 1.345 \\ 1.350 \\ 1.359 \\ 1.364 \\ 1.368 \\ 1.368 \\ 1.367 \\ 1.370 \\ 1.370 \\ 1.370 $		

For a, we have from equation (1.),

$$a\sin\theta = \frac{\varphi'}{\varphi}\cos\theta'\cos\zeta' - \cos\theta\cos\zeta,$$

whence we obtain, from the observations on the N. and S. points, a = +.0311, and from those on the N.N.E. and N.N.W., S.S.E. and S.S.W. points, α also = $+\cdot0311$.

In the Erebus we have found a for the spot in the ship where Mr. Fox's apparatus was used = +.023, from the observations made when the ship was in progress to the southward; and = +.029 at Hobarton and the Falkland Islands. The corresponding values in the Terror are +.026 and +.031.

In the case of the Terror, therefore, I have employed separate tables for the corrections for the ship's attraction, viz. a taken as $\pm .028$ in the passage from Hobarton to New Zealand; as + 026 in the passage to the higher latitudes; and as + 031 during the return from the high latitudes to the Falkland Islands.

For b and c, we obtain from the observations at the Falkland Islands as follows:— In the case of b, we have from equation (2.),

$$b\cos\theta = \frac{\varphi'}{\varphi}\cos\theta'\sin\zeta'\csc\zeta;$$
o 2

the observations at N.E., N.W., S.E. and S.W. give b=+.984; those at E.N.E., W.N.W., E.S.E. and W.S.W., b=.984; and those at E. and W. b=.982.

In the case of c, we have from equation (3.),

$$\frac{\varphi'}{\varphi}\sin\theta' = c\cos\theta\cos\zeta + d\sin\theta;$$

from the observations at N. to N.E. and N.W. inclusive, and from S. to S.E. and S.W. inclusive, eliminating d, we have

$$c = +.009$$
.

The constant d is perhaps the most difficult of the constants to ascertain satisfactorily, as its value derivable from the observations depends on a knowledge of the true geographical dip at the place of observation, free from what is now known as station error. Experience has fully shown the general fact, that inclinations observed on land cannot safely be assumed as free from local disturbance. The discrepancies of gravitation at the Falkland Islands are well known from the experiments with the pendulum; and from the geological character of these islands, we might be prepared to expect the existence of magnetic discrepancies also. By the needles in both ships, the inclination was found a third of a degree higher at the magnetic observatory on shore than when observed on board in the harbour; if the observatory dip were to be assumed as an undisturbed one, we should obtain d in both ships considerably less than unity, whereas from the comparison of the observations in both ships in the preceding December and January, with the inclination observed at the same time on the ice over a deep sea, where no local attraction can be imagined to exist, we have d (as far as the small differences of geographical position will permit us to judge) differing scarcely, if at all, from unity in either ship. The preference is certainly due to the deduction from the results obtained on the ice. Taking therefore d=1, c = +.01, b = .984 and a = +.026, we have the corrections, and the corrected inclination, of the observations in the Terror between the 6th and 16th of January as follows:

Ship's head.	No. of observations.	Inclination observed.	Correction.	Corrected Inclination.
N. N.W. N.E. W. \frac{1}{4} S. E. \frac{1}{4} S. W. by S. E. by S. W.S.W. E.S.E. S.W. S.E.	4 4 9 4 6 6	-81 19.5 -80 58.5 -79 58.5 -79 49.0 -79 29.0 -79 04.5 -78 30.0	+ î 26 +1 09 +0 12 -0 01 -0 17.5 -0 51.5 -1 24.5	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

Slight differences in the corrected results must be looked for, as the observations were not all taken precisely at the same geographical spot: those which appear in the table are, however, very slight; the accord produced by the corrections seems as

satisfactory as could be wished or expected; and I have accordingly taken the above stated values of b, c, and d, for the whole period under notice.

On a general review of the examination to which the observations in the Erebus and Terror in this and the preceding voyage have been subjected, in reference to the magnetic influence of their iron, we find reason to conclude from the consistent experience of both voyages, that the disturbance in them was altogether such as would be occasioned by the magnetism induced in the soft iron of the ship by the magnetism of the earth,—if we permit ourselves to include as possessing the quality of softness, certain portions of iron which, though not permanently magnetic, do still retain polarity, and require some time to conform to the changes in magnetical relations induced by changes of geographical position. It is not improbable that this may be a general case in sailing vessels similar to the Erebus and Terror; but we should by no means be warranted in deriving a corresponding inference in regard to ships which contain steam machinery, and still less in the case of iron vessels. may possibly possess permanent magnetism strictly so called; in addition to induced magnetism, and temporarily-abiding polarity. It is very desirable that we should have some means of judging of what may be expected in vessels of these The knowledge would be valuable were it only for the compass corrections necessary for the ordinary purposes of navigation; and it appears indispensable before a correct judgment can be formed of the confidence to which methods may be entitled, which have been already, or may hereafter be devised, to supersede these corrections by the employment of compensating forces. It is not necessary that steam or iron-built ships should perform voyages like those of the Erebus and Terror to procure this knowledge; a voyage from the British Channel to the Tropics would be sufficient; the ship should be swung before her departure from these islands, and immediately on her arrival in the Tropics, and at intervals of three or six months during her continuance there; the experiment should also be repeated on her return to England before any material alteration is made in the distribution of her iron.

Index Correction.

Index Correction of R. F. 5 for the Observations of the Inclination in the Erebus.—
The observations at sea with this needle having been made in the one position of the instrument only, viz. with the face of the circle towards the east, and the marked side of the needle towards the observer,—we have to obtain the index correction, by comparing the inclinations observed in the same manner on shore, or on the ice, with the results given at the same places by needles of which the poles were reversed and the needle and circle used in the eight ordinary positions.

The stations which furnish this comparison are Hobarton, Sydney, New Zealand, the Falkland Islands, and two stations on the ice in the latitudes of -63° 23' and -65° 49'. The results of the observations at Hobarton with needles with which the complete process for determining the inclination was gone through, were given in No. V. of these Contributions*. Those at the other five stations are as follows:—

^{*} Philosophical Transactions, 1843, Part II. p. 165.

Observations of the Inclination, with Needles whose Poles were reversed, made at Garden Island, Sydney, July 1841.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. July 20. 20. 20. 20.	2 15 p.m.	R 4 R 10 R 6 R 7 C 1 C 2	$\begin{array}{c} \alpha - 6^{\circ}2 & 5^{\circ}2 \cdot 5 \\ \beta - 62 & 46 \cdot 5 \\ \alpha - 62 & 57 \cdot 5 \\ \beta - 62 & 33 \cdot 7 \\ \alpha - 62 & 50 \cdot 1 \\ \beta - 62 & 58 \cdot 5 \\ \alpha - 62 & 53 \cdot 9 \\ \beta - 62 & 51 \cdot 9 \\ \alpha - 62 & 48 \cdot 2 \\ \beta - 62 & 45 \cdot 6 \\ \alpha - 62 & 49 \cdot 6 \\ \beta - 62 & 40 \cdot 5 \\ \end{array}$	$ \begin{cases} -62 & 49.5 \\ -62 & 45.6 \\ -62 & 54.3 \\ -62 & 52.9 \\ -62 & 46.9 \\ -62 & 45.1 \\ -62 & 49.1 \end{cases} $	Needles belonging to H.M.S. Erebus. Needles belonging to H.M.S. Terror. General Mean.

Observations of the Inclination, with Needles whose Poles were reversed, made at the Bay of Islands, New Zealand, August to November 1841.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. August 23. 23. 24. 24. 24. October 5. 12. 26.	h m 2 10 p.m. 3 10 p.m. 8 40 a.m. 9 45 a.m. 11 00 a.m. 1 10 p.m. 4 00 p.m. 7 00 a.m. 6 35 a.m. 9 35 a.m. 10 35 a.m.	R 10 R 4 R 10 R 6 R 7 R 4 R 10 R 6 R 7 C 1	α direct.		Needles belonging to H.M.S. Erebus.
23. November 6.	9 00 A.M. 11 30 A.M. 9 00 A.M. 10 30 A.M.	C 2 C 1 C 2	$\begin{array}{c} \alpha = 59 & 30^{\circ}0 \\ \beta = 59 & 27^{\circ}8 \\ \alpha = 59 & 27^{\circ}8 \\ \beta = 59 & 22^{\circ}7 \\ \alpha = 59 & 32^{\circ}5 \\ \beta = 59 & 28^{\circ}1 \\ \alpha = 59 & 20^{\circ}8 \end{array}$	$ \begin{cases} -59 & 28.9 \\ -59 & 27.0 \\ -59 & 30.3 \\ -59 & 26.8 \end{cases} $	Needles belonging to H.M.S. Terror.
	,			-59 31.9	General Mean.

Observations of the Inclination with Needles whose Poles were reversed, made on the ice.

Date.	Lat.	Long.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. December 19.	-63 23	210 02	R 4	$\begin{bmatrix} \alpha - 77 & 23.1 \\ \beta - 77 & 23.4 \end{bmatrix}$	-77 23·3 -77 23·3	
	-65 59 $-65 59$		R 4	$\begin{bmatrix} \alpha - 79 & 32.0 \\ \beta - 79 & 24.7 \\ \alpha - 79 & 35.6 \end{bmatrix}$	$\begin{bmatrix} -79 & 28.4 \\ -79 & 33.6 \end{bmatrix} -79 & 31.0$	
1842. January 16.		202 02	R 4		*	Needles belonging to H.M.S. Erebus.
16.	-65 49	202 02	R 6	$ \begin{vmatrix} \alpha - 79 & 40.5 \\ \beta - 79 & 34.4 \\ \alpha - 79 & 36.2 \\ \beta - 79 & 42.9 \end{vmatrix} $	$-79 \ 39.6 > -79 \ 39.5$	
16.	—65 49	202 02	R 7	$\begin{bmatrix} \alpha - 79 & 41.8 \\ \beta - 79 & 41.0 \end{bmatrix}$	−79 41·4 	

Observations of the Inclination, with Needles whose Poles were reversed, made at the Magnetic Observatory at Port Louis, in the Falkland Islands, April to August 1842.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842. April 12. 12. 13. 15. 15. 19.	h m 1 30 p.m. 3 30 p.m. 3 30 p.m. 8 20 A.m. 3 10 p.m. 8 00 A.m. 3 30 p.m.	R 4 R 6 R 7 R 4 R 4 R 4 R 4 R 4	α direct. β reversed. α -52 33·5 β -52 16·7 α -52 26·0 β -52 32·0 α -52 30·8 β -52 30·9 α -52 36·8 β -52 16·3 α -52 39·9 β -52 12·4 α -52 36·9 β -52 16·2 α -52 36·3 β -52 16·2 α -52 36·8 β -52 16·8 α -52 36·8 β -52 16·8 α -52 36·8 β -52 16·8 α -52 36·8 β -52 16·8 α -52 36·8 β -52 15·3	$\left.\begin{array}{c} & & & \\ -52 & 25 \cdot 1 \\ -52 & 29 \cdot 0 \\ \end{array}\right\} -52 & 26 \cdot 6 \\ -52 & 26 \cdot 2 \\ -52 & 27 \cdot 3 \\ -52 & 26 \cdot 3 \\ -52 & 26 \cdot 5 \\ -52 & 26 \cdot 1 \end{array}\right\}$	Remarks. Needles belonging to H.M.S. Erebus.
26. 26. 29. May 3. 3. 6.	3 30 p.m. 8 00 a.m. 8 00 a.m. 3 30 p.m. 8 00 a.m.	R 4 R 4 R 4 R 4 R 4 R 4 R 4 R 4	$\begin{array}{c} \alpha -52 & 35.9 \\ \beta -52 & 10.3 \\ \alpha -52 & 36.0 \\ \beta -52 & 08.7 \\ \alpha -52 & 38.3 \\ \beta -52 & 18.8 \\ \alpha -52 & 35.8 \\ \beta -52 & 36.4 \\ \alpha -52 & 36.3 \\ \beta -52 & 16.9 \\ \alpha -52 & 36.3 \\ \beta -52 & 17.1 \\ \alpha -52 & 37.3 \\ \beta -52 & 14.9 \\ \end{array}$	$ \begin{cases} -52 & 23 \cdot 1 \\ -52 & 22 \cdot 3 \\ -52 & 28 \cdot 6 \\ -52 & 21 \cdot 1 \\ -52 & 26 \cdot 8 \\ -52 & 26 \cdot 7 \\ -52 & 26 \cdot 1 \end{cases} $	

Observations of Inclination. (Continued.)

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842. May 10.	h m 10 30 A.M.	R 4	$\alpha = 52 31.2$	} -52 28.2]
10.	3 00 р.м.	R 4	$\beta - 52 \ 25.2$ $\alpha - 52 \ 24.3$	$\left.\right\} -52 \ 27.5$	
13.	8 00 а.м.	R 4	$ \begin{vmatrix} \beta - 52 & 30.6 \\ \alpha - 52 & 36.7 \\ \beta - 52 & 14.5 \end{vmatrix} $	$\left. \begin{array}{l} -52 \ 25.6 \end{array} \right.$	
13.	3 30 р.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 25.3$	
17.	8 00 а.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 25.5$	-
17.	3 30 р.м.	R-4	$\alpha - 52 \ 33.4$	$\left.\right\} -52\ 25.5$	
20.	8 00 а.м.	R 4	$\beta -52 \ 17.7$ $\alpha -52 \ 36.8$	$\left.\right\} -52 \ 25.0$	
20.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 23.7$	
24.	8 00 а.м.	R 4	$\beta = 52 \ 13.0$ $\alpha = 52 \ 36.5$	$\left.\right\} -52 \ 27.7$	-
24.	3 30 р.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left. \begin{array}{c} 1 \\ -52 & 27.7 \end{array} \right $	
27.	8 00 а.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 23.0$	
27.	3 30 р.м.	R 4	$\beta - 52 \ 12.5$ $\alpha - 52 \ 32.8$	$\left.\right\} -52\ 23.4$	
June 1.	8 00 а.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52\ 26.5$	
1.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{2}^{1}$ -52 25.7	
4.	8 00 а.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52\ 26.5$	Needles belonging to H.M.S. Erebus.
4.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\}$ -52 26.6	
7.	8 00 а.м.	R 4	$ \begin{vmatrix} \beta - 52 & 16.9 \\ \alpha - 52 & 36.4 \end{vmatrix} $	$\left.\right _{2}^{2} -52 25.9$	
7.	8 00 а.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{2}^{2}$	
10.	8 00 A.M.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left. \begin{array}{c} -52 & 27.4 \end{array} \right.$	
10.	3 30 р.м.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right _{-52\ 26\cdot 8}$	
14.	8 00 а.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right \left52 \ 26.0 \right $	
14.	3 30 р.м.	R 4	$\begin{bmatrix} \beta - 52 & 16.2 \\ \alpha - 52 & 41.3 \\ \beta - 50 & 13.2 \end{bmatrix}$	$\left. \begin{array}{c} 1 \\ -52 \ 27.3 \end{array} \right $	
17.	8 00 A.M.	R 4	$ \begin{vmatrix} \beta - 52 & 13.2 \\ \alpha - 52 & 34.8 \\ \beta - 52 & 14.7 \end{vmatrix} $	$\left.\right _{2}^{3}$	
17.	10 00 а.м.	R 6	$\alpha - 52 \ 20.4$	$\left. \begin{array}{c} 1 \\ -52 \ 24.2 \end{array} \right.$	
17.	11 00 а.м.	R 7	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{-52\ 27.8}$	
17.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{-52}^{23.8}$	
21.	8 00 A.M.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{2}^{2}$	
21.	3 30 р.м.	R 4	$ \begin{vmatrix} \beta - 52 & 18.6 \\ \alpha - 52 & 29.7 \\ \beta - 52 & 19.9 \end{vmatrix} $	$\left52 \ 24.8 \right.$	

Observations of Inclination. (Continued.)

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842. June 28.	h m 8 00 A.M.	R 4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	} -52 21.5	<u> </u>
July 1.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 20.7$	
5.	8 00 а.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left \begin{array}{c} 1 \\ -52 & 21.5 \end{array} \right $	
8.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right _{2}^{3}$	
12.	8 00 а.м.	R 4	$\alpha - 52 34.1$	$\left.\right\}$ -52 23.0	
15.	3 30 р.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 22.7$	
19.	8 00 а.м.	R 4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\} -52 \ 22.2$	
22.	3 30 г.м.	R 4	$\begin{vmatrix} \beta - 52 & 11.6 \\ \alpha - 52 & 31.8 \\ \beta & 52 & 14.8 \end{vmatrix}$	$\left.\right\} -52 \ 23.3$	
August 2.	8 00 а.м.	R 4	$\begin{vmatrix} \beta - 52 & 14.8 \\ \alpha - 52 & 32.6 \\ \beta - 52 & 16.1 \end{vmatrix}$	$\left.\right\} -52 \ 24.3$	Needles belonging to H.M.S. Erebus.
9.	8 00 а.м.	R 4	$ \begin{vmatrix} \beta - 52 & 16 \cdot 1 \\ \alpha - 52 & 33 \cdot 4 \end{vmatrix} $	$\left \begin{array}{c} 1 \\ -52 & 22.6 \end{array} \right $	
12.	3 30 р.м.	R 4	$ \begin{vmatrix} \beta - 52 & 11.9 \\ \alpha - 52 & 32.7 \end{vmatrix} $	$\left \begin{array}{c} 1 \\ -52 & 23.2 \end{array} \right $	
16.	8 00 а.м.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \right = 52 \ 20.0$	
19.	3 30 р.м.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \right _{-52}^{25\cdot 2}$	
23.	8 00 а.м.	R 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left \begin{array}{c} 1 \\ -52 & 22.0 \end{array} \right $	
23.	9 00 а.м.	R 6	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right\} = 52 \ 22.5$	
23.	10 00 а.м.	R 7	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right _{2}^{3}$	
April 15.	8 00 а.м.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 1 \\ 1 \end{vmatrix} = 52 \ 34.3$	h
15.	3 00 р.м.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right _{-52}^{1}$ 35.5	
19.	8 45 A.M.	C 1	$ \begin{vmatrix} \beta - 52 & 24.9 \\ \alpha - 52 & 43.3 \\ 2 & 52 & 20.3 \end{vmatrix} $	$\left \right _{-52\ 31\cdot 8}$	
19.	3 45 р.м.	C 1	$ \begin{vmatrix} \beta - 52 & 20.2 \\ \alpha - 52 & 42.8 \\ \beta - 52 & 31.6 \end{vmatrix} $	$\left.\right _{-52\ 32\cdot 2}$	
June 15.	8 00 а.м.	C 1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right\}$ -52 32.4	
15.	9 00 а.м.	C 2	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left \begin{array}{c} 1 \\ -52 & 29.4 \end{array} \right $	
15.	3 00 а.м.	C 1	$\beta -52 20.9$ $\alpha -52 39.9$	$\left.\right _{-52\ 31\cdot7}$	
15.	3 40 а.м.	C 2	$\beta - 52 \ 23.4$ $\alpha - 52 \ 35.4$	$\left.\right\} = 52 \ 29.3$	Needles belonging to H.M.S. Terror.
July 26.	8 40 а.м.	C. 1	$\beta - 52 \ 23.2$ $\alpha - 52 \ 44.9$	$\left.\right _{2}^{3}$	
26.	10 30 а.м.	C 2	$ \begin{vmatrix} \beta - 52 & 23.5 \\ \alpha - 52 & 38.6 \\ \beta - 52 & 15.3 \end{vmatrix} $	$\left.\right _{2.52}^{10}$	
August 17.	10 00 а.м.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right _{2}^{3}$ -52 35.7	
17.	10 30 а.м.	C 2	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right\} -52 \ 25.1$	
23.	. 9 30 а.м.	C 1	$\beta - 52 \ 14.1$ $\alpha - 52 \ 39.9$	$\left.\right\} -52 \ 32.4$	
23. 23.			$ \begin{vmatrix} \beta - 52 & 24.9 \\ \alpha - 52 & 33.8 \\ \beta - 52 & 19.2 \end{vmatrix} $	$\left \frac{1}{2} \right = 52 \ 26.5$	J
		,	p - 52 132	-52 26.2	General Mean.

From these observations we have the true inclination at these six stations as follows:—

On ice, lat	. —	$ {65}$	49.]	Lor	ıg.	$2\overset{\circ}{0}2$	ó	2			$ {79}$	39.5
On ice, lat	.—	63	23.]	Lor	ıg.	210	0	2			77	23.3
Hobarton	•	٠			•				•	•	•	70	40.7
Sydney .	•			•		•	•		•	•	•	62	49.1
New Zeala	\mathbf{nd}		•	•	•							59	31.9
Falkland I	sla	nd	s.									52	26.2

The observations with R. F. 5, at the same stations, and at the same spots on shore, or on the ice, gave as follows:—

On Ice. Lat65° 49'. Long. 202° 02'.	On Ice. Lat63° 23'. Long. 210° 02'.	Hobarton.	Sydney.	New Zealand.	Falkland Islands.
Face East $-79 35.6$	$-7\overset{\circ}{7}$ 15.5	$-7\overset{\circ}{0}\ 2\overset{\prime}{6}\cdot 4$	$-6\overset{\circ}{2}\ 4\overset{'}{6}\cdot 3$	$-5^{\circ}9 \ 2^{'}9.8$	$-5\overset{\circ}{2}\ 3\overset{\prime}{2}\cdot 9$
Face West -80 39.2	-78 20.3	-71 20.3	- 63 44·3	$-60\ 27.9$	-53 34.7
$Mean = \frac{-80 \ 07.4}{}$	$-77 \ 47.9$	-70 53.4	$-63\ 15.3$	-59 58·8	-53 03.8

We have thus the following index corrections:—

Face East
$$-3.8$$
 -7.8 -14.3 -2.8 -2.1 $+6.7$
Face West $+59.7$ $+57.0$ $+39.6$ $+55.2$ $+56.0$ $+68.5$
Mean correction $+27.9$ $+24.6$ $+12.7$ $+26.2$ $+26.9$ $+37.6$

and the difference of the results with the face east and face west as follows:-

From the signs and numerical values of the corrections of the mean results with R. F. 5, we may infer that the axis of rotation in this needle deviated from the centre of gravity in the longitudinal direction, so as to cause the south end of the needle slightly to preponderate. From the differences of the results with the face east and face west, it appears that there was also a small deviation in the axis of rotation from the centre of gravity in the perpendicular direction. In the results with the face east, these two sources of error partially counteracted each other, so that the index correction with the face east amounted at no time to more than a very few minutes.

The corrections which have been applied to the observations have been taken from the following table, in which the correction for -70° has been taken as -5'.8, and the change in the correction, corresponding to an increase of one degree in the south dip, as -0'5. In forming this table the determinations on land have been allowed a greater weight than the determinations upon the ice, the latter consisting of fewer observations, and being made probably under circumstances less favourable for this particular purpose.

Table of Index correction	s for l	R. F. 5	face East.	between	-52° and	-85° .
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$ \begin{array}{c cccc} +3.2 & -6 \\ +2.7 & -7 \\ +2.2 & -7 \\ +1.7 & -7 \\ +1.2 & -7 \end{array} $	$ \begin{array}{c cccc} & -5.8 \\ & -6.3 \end{array} $
$ \begin{vmatrix} +2.7 \\ +2.2 \\ +1.7 \end{vmatrix} $	$ \begin{array}{c cccc} & -5.8 \\ & -6.3 \end{array} $
+1.7 -7	
, ,	9 - 6.8
11.0	~ - 00
	73 - 7.3
+0.7 -7	
+0.2 -7	_
-0.3 -7	· · · · · · · · · · · · · · · · · · ·
-0.8 -7	•
-1.3 -7	
- 1	
- 11	
-3.8	
1.9	B4 −12·8
-4-9 8	35 -13.3
	-1·8

Index Correction of F. C. B. for the Observations of Inclination in the Terror.—The observations of inclination at sea in this ship were all made with the face of the instrument towards the east, and with the marked face of the needle towards the observer. We may examine the index corrections consequently in the same manner, and by comparison with the same complete determinations as in the case of the needle of the Erebus; confining the comparison however to the land stations, because F. C. B. was not observed with at either of the ice stations.

The inclinations taken with this needle were observed both direct and with the aid of deflectors; the deflectors employed were a spare needle as "deflector N" and "deflector S"; and the magnets of the apparatus, either used separately as "magnet N," or "magnet S," or conjointly as "magnets N S." From some instrumental accident, the inclinations observed with "deflector N" were always considerably in defect of the others when the face of the circle was east; with a corresponding excess with the face west, on the few occasions on shore when the observations were made in both positions. As the observations at sea were exclusively with the face east, it has been necessary on this account to consider separately those amongst them which were taken with "deflector N," and to obtain a distinct index correction for them. We will first examine the index corrections required for the direct observations, and for those with the other deflectors.

The observations with F. C. B. on shore at the four land stations, where the com-

plete process for determining the true inclination was gone through with other needles, were as follows:—

		Hobarton.	Sydney.	New Zealand.	Falkland Islands.
	Face East -	$-70^{\circ}17.3^{\circ}$	$-\overset{\circ}{62}\ \overset{\circ}{22\cdot4}$	-5850.6	$-5^{\circ}1^{\circ}3^{\prime}8^{\cdot}4$
Observed	Face East - Face West -	-70 44.8	-62 56.5	-60 02·8	$-52\ 57.2$
Mean		- 70 31·1	$-62 \ 39.5$	$-59\ 26.7$	-52 17.8
True i	inclination -	-70 40.7	$-62\ 49.1$	-59 31.9	$-52\ 26.3$
	Face East	-23.4	-26.7	— 41·3	-47.9
Index corrections	Face West	+ 4.1	+ 7.4	+30.9	+30.9
	Mean	- 9.7	- 9.6	- 5.2	- 8.5
Differences face E	Cast and West	27.5	34.1	$72 \cdot 2$	78.8

The corrections of the mean results with F. C. B. at the four stations accord well within the limits of observation error. On examining the differences in the results with the face east and face west, and the corrections severally required in the two positions at the four stations, it appears probable that a very slight derangement of some part of the instrument took place between the observations at Sydney and those at the Bay of Islands, which caused the partial results with the face east and face west to diverge more from each other than they had done previously, but without affecting the mean results. A note which accompanied the observations to England shows that Captain Crozier considered that some slight change had taken place in the amount of the index correction with the face east, but was unable to assign its date or its cause. In the absence of any distinct evidence in these respects,—and in consideration of the insufficiency of the means of assigning the precise amount of the change,—I have preferred the employment of an arithmetical mean of the index corrections observed at the four stations (-35') during the whole course of the voyage. The uncertainty arising from this source cannot amount to more than a very few minutes in any portion of the voyage.

For the index correction with deflector N we have,

H	Iobarton.	Sydney.	New Zealand.	Falkland Islands.
Face East	$6\overset{\circ}{9}\ 3\overset{'}{3}\cdot 5$	-61 36·7	$-5\overset{\circ}{7}\ 5\overset{'}{8}\cdot 0$	$-50^{\circ}54.4^{\circ}$
Face West —	71 25.9	-63 00·7	$-60\ 12.3$	- 53 31·3
Mean —	70 29.7	$-62 \ 18.7$	-59 05.1	-52 12.8
True inclination —	70 40.7	-62 49.1	- 59 31.9	$-52\ 26.3$
Index correction, face East	-67.2	$\phantom{00000000000000000000000000000000000$	-93.9	-91·9
Mean index correction, face Ea	st	81	!	

Elements of Calculation of the Intensity Observations.

1. With Weights.—The observations of the intensity of the magnetic force, during the period now under consideration, were made in both ships with Mr. Fox's apparatus; those in the Erebus with the same circle which had been used in the previous voyage, and those in the Terror with a circle of the same size as that of the Erebus, being the property of Captain Crozier, and received by him at Van Diemen Island. The needle employed to show the angles of deflection in the Erebus, marked R. F. 5, was not the same which had been used for that purpose in the voyage of 1840–1841, namely, R. F. 4, which now in its turn was used as a deflector. The weights employed in deflecting the intensity needle were 1, 2, 3, 4, 5 and 6 grains: the angles of deflection obtained with one grain were however too small to yield results of the same satisfactory nature as those derived from the weights from two to six grains, and I have not therefore taken them into the account. The mounted needle in the Terror was marked F. C. B., a spare needle C being used as a deflector, in addition to the deflecting magnets belonging to the apparatus. The weights were 1, $1\frac{1}{2}$, 2, $2\frac{1}{2}$, 3 and $3\frac{1}{2}$ grains.

At Hobarton we have the deflections occasioned by the constant weights on the needle of the Erebus, April 1841, as follows:—

]	Defle	ction.	Therm.					Therm.
Face East.	$^{ m grs.}_{ ho}$	$\overset{\circ}{13}$	02.8	$ {60}$	Face West.	$\mathbf{c}^{\mathbf{grs}}$.	$\overset{\circ}{13}$	14.5	$ {60}$
	3	19	37.2	60		3	19	55.5	60
Face East.	4	26	47.7	60	Face West.	4	27	02.7	5 8
	5	34	23.5	60		5	34	51.5	58 58
	6	42	55.7	61		6	43	07:3	58

and in the needle of the Terror as follows:-

At Sydney, in July 1841, the deflections with the same weights were—

				E	REBU	s.								TERI	ROR	•			
		Defl	ection.	Ther.			Defle	ection.	Ther]	Defle	ction.	Ther.]	Defle	ction.	Ther.
	$\mathbf{r}^{\mathrm{grs.}}$		57.4	$\overset{\circ}{56}$. 1	grs. 2	$\overset{\circ}{14}$	32.6	${\bf 6\overset{\circ}{4}}$		$\operatorname{grs.}$	$\overset{\circ}{13}$	08.8	$ {60}$		$\int 1$	$1\overset{\circ}{2}$	44.1	$ {60}$
East.	3	21	13.7	55				51.4	63	نډ	$1\frac{1}{2}$	20	02.0	60	st.	$1\frac{1}{2}$	19	03.3	60
e E	4	29	09.2	55	\$ \{	4	29	32.1	64	East	2	27	00.7	60	We	2	26	01.2	60
Face	5	37	43.3	55	Fac	5	37	38.9	63	ace	$2\frac{1}{2}$	34	25.2	60	ace	$2\frac{1}{2}$	33	17.7	60
	ackslash 6	46	51.7	55	L	6	47	32.4	63	ĒΨ	3	42	06.9	60	1	3	41	35.2	60
											$3\frac{1}{2}$	51	13.5	60		$3\frac{1}{2}$	51	02.1	60

Taking 1.82 as the provisional value of the intensity at Hobarton (Phil. Trans. 1843, Part II. p. 186)*, we have its value at Sydney, by the needles of the two ships, as follows:—

	Erebu	JS.		Terro	R.
grs.	Face East.	Face West.	grs.	Face East.	Face West.
2	1.703	1.662	1	1.691	1.674
3	1.687	1.667	$1\frac{1}{2}$	1.685	1.712
4	1.683	1.680	2	1.708	1.705
5	1.680	1.704	$2\frac{1}{2}$	1.692	1.709
6	1.698	1.688	3	1.709	1.715
	1.690	1.680	$3\frac{1}{2}$	1.703	1.687
	1.6	585 		1.698	1.700
				1.0	599

At the Bay of Islands in New Zealand, in August and October 1841, the deflections were as follows:—

EREBUS.

				August.		October.
		Deflection.	Ther.	Deflection.	Ther.	Deflection. Ther. Deflection. Ther.
	$\mathbf{c}^{\mathbf{grs.}}$	14 59.3	$\overset{\circ}{59}$	$(\mathring{15} \ \overset{\circ}{23} \cdot 3)$	$ {60}$	$(1\overset{\circ}{4}\overset{\circ}{43}\cdot 2\overset{\circ}{68}\overset{\circ}{15}\overset{\circ}{11}\cdot 1\overset{\circ}{64}$
East.	3	22 47.5	5 9	g 23 17·9	59	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
е Е	4	30 55.0	59	$\geqslant 30\ 26.9$	59	
Face	5	40 10.5	58	$\begin{bmatrix} 40 & 52.0 \end{bmatrix}$	6 0	$\begin{bmatrix} 39 & 59 \cdot 3 & 70 & \frac{9}{12} \\ 39 & 59 \cdot 3 & 70 & \frac{9}{12} \\ 39 & 51 \cdot 0 & 65 \end{bmatrix}$
	6	50 38.1	58	51 26.0	61	L50 35·0 71 L51 38·7 65

TERROR.

					August							0	ctober.			
		Defl	ection.	Ther.		Def	lection.	Ther.		Def	lection.	Ther.		Defl	ection.	Ther.
	$\int 1$	$\overset{\circ}{14}$	$03 \cdot 2$	$\overset{\circ}{59}$		$\int_{0.01}^{\circ}$	2 4·3	$\overset{\circ}{59}$		$\bigcap_{i=1}^{\circ}$	51.7	$ {64}$		$\mathring{13}$	26.8	$ {64}$
ئد	$1\frac{1}{2}$	21	17.9	59	ئِ	20	30.2	59	ئد	20	53.0	64	ئب	20	16.4	64
East.	2	28	22.1	59	West.	27	46.9	59	East.	28	22.4	64	West.	27	38.8	64
Face	$2\frac{1}{2}$	36	50.7	59	Face]	35	43.0	59	Face	37	05.6	64	Face	35	45.1	64
E.	3	44	58.3	59	띥	44	38.7	59	1	45	02.2	64	F	44	47.7	64
	$\lfloor 3 \frac{1}{2} \rfloor$	55	09.9	59		55	23.7	59		55	19.1	64		55	26.4	64

whence we have the intensity at the Bay of Islands, by the needles of the two ships, as follows:—

^{*} 1.82 + e being the true value, in which e is a small correction to be determined hereafter, applicable to the whole series of observations depending on Hobarton as a primary station.

		Ereb	Us.				TERRO	OR.	
	Au	gust.	, . O	ctober.		Au	gust.	- O	ctober.
$2^{\mathrm{grs.}}$	Face East.	Face West. 1:571	Face East. 1.620	Face West. 1.593	grs.	Face East. 1.584	Face West. 1.592	Face East. 1.606	Face West. 1.588
3	1.578	1.568	1.583	1.570	$l\frac{1}{2}$	1.601	1.595	1.620	1.616
4	1.597	1.633	1.619	1.586	2	1.633	1.605	1.633	1.613
5	1.594	1.590	1.603	1.591	$2\frac{1}{2}$	1.596	1.607	1 587	1.606
6	1.604	1.591	1.608	1.588	3	1.622	1.619	1.621	1.616
	1.593	1:591	1.607	1.586	$3\frac{1}{2}$	1.618	1.594	1.616	1.594
	1.5	92	1.5	596		1.609	1.602	1.614	1.605
		1.5	94			1	1.6	1:0	609

At Port Louis in the Falkland Islands, in July and August 1842, the deflections were—

							LREB	US.							
		Deflection.	April. Ther.		Defl	ection.	Ther.		Defl	ection.	Ther.	Aug		ection.	Ther.
	$^{ m grs.}_{ m ar{2}}$	18 31.1	45	ſ	$ {18}$	50.4	$\overset{\circ}{42}$, i'7	57.1	37		(18	$32 \cdot 9$	39
East	3	27 42.7	45	West.	2 8	30.0	42	East.	27	43.3	37	West.	28	26.6	40
		37 58.5	43		38	51.0	41	e E	37	40.4	37		39	05.3	40
Face	5	48 55.9	43	Face	51	27.9	41	Face	49	31.4	38	Face	51	19.2	40
	6	66 49.8	43	L	68	40.3	41		67	23.4	38		l 69	35.7	40

TERROR.

				Αj	pril.							Jul	у.					A	lugus	t.			
		Deflection.	Ther.		Defle	ection.	Ther.		Defle	ection.	Ther.		Defle	ction.	Ther.		Defle	ection.	Ther.		Defi	lection.	Ther.
	1	16 56.5			1								1			1					1		
st.	$1\frac{1}{2}$	25 36.6	43	est.	24	36.9	43	ıst.	25	34.3	41	est.	24	27.9	41	ıst.	25	37.3	38	est.	24	30.1	38
e Ea	2	34 47.2	43	ĕ.	33	44.9	43	se Ea	34	47.8	41	e W	33	49.5	41	e Ea	34	24.4	38	e We	33	57 ·8	38
	1 4	45 34 1			l .				Į.				1			- 1							
	13	57 39.1	43		l 58	17.8	43		l 57	48.7	41		158	19.5	41		.57	43.6	38		57	35.7	38

whence we have the intensity at Port Louis, by the needles of the two ships, as follows:—

Erebus.						Terror.								
	$\mathbf{A}_{\mathbf{I}}$	oril.	Aug	gust.		Ap	ril.	Jv	ıly.	Aug	ust.			
$2^{ ext{grs.}}$	Face East. 1.291	Face West. 1.288	Face East.	Face West. 1.306	grs.	Face East. 1.316	Face West. 1:316	Face East. 1.323	Face West. 1.301	Face East. 1.311	Face West. 1.315			
3	1.311	1.296	1.310	1.299	$1\frac{1}{2}$	1.331	1.338	1.333	1.345	1.331	1.344			
4	1.331	1.315	1.339	1.309	2	1.356	1:342	1.355	1.339	1.369	1.335			
5	1.361	1.326	1.347	1.329	$2\frac{1}{2}$	1.336	1.334	1.338	1.339	1.341	1.333			
6	1.345	1.332	1.339	1.324	3	1.353	1.333	1.350	1.333	1.352	1.344			
	1.328	1.311	1.333	1.313		1:338	1.332	1:340	1.331	1:341	1:334			
	1.3	20	1.3	23		1.3	35	1.3	36	1.3	37			
	telepolitical control	1.3					and a graph of the state of the	1.3	36	Santa and Santa				

Besides the four land stations at which the intensities shown by the needles of the two ships have been thus compared, we have also one ice station in lat. -65° 47', long. 202° 08', at which similar comparisons may be instituted. The deflections and intensities were as follows:—

		Erebu	s.			Terror.		
		Deflection.	Ther.	Intensity.		Deflection.	Ther.	Intensity.
Face East.	$egin{pmatrix} ext{grs.} \ 2 \ 3 \ 4 \ 5 \ 6 \ \end{pmatrix}$	12 13·0 18 32·4 24 49·3 32 02·4 39 31·4	50 54 54 54 55	1·940 1·921 1·952 1·936 1·946 1·939	$egin{array}{c} { m Egs.} \\ { m 1} \\ { m 1} rac{1}{2} \\ { m 2} \\ { m 2} rac{1}{2} \\ { m 3} \\ { m 3} rac{1}{2} \\ \end{array}$	11 25·4 17 08·3 23 02·9 29 16·2 36 17·4 43 23·5	53 53 53 53 53 53	1·940 1·957 1·979 1·955 1·935 1·932
								1 900

Collecting these several results in one view, we have as follows:—

	Erebus.	TERROR.	DIFFERENCE.
Intensity at Hobarton	. 1.82	1.82	(Erebus in defect.)
Intensity at Sydney	. 1.685	1.699	'014 or 8 parts in 1000
Intensity at the Bay of Islands	. 1.594	1.607	'013 or 8 parts in 1000
Intensity on ice, lat. $-65^{\circ} 49'$, long. $202^{\circ} 09'$	$2' \ 1.939$	1.950	·011 or 7 parts in 1000
Intensity at Port Louis, Falkland Islands	. 1.322	1.336	·014 or 10 parts in 1000

The difference between the results given by the needles of the two ships, though small, is so consistently shown at all the stations during the voyage, that we cannot hesitate to attribute it to the occurrence of a change of corresponding amount in the magnetism of one needle or the other, between the observations at Hobarton in April 1841, and those at Sydney in July of the same year. If we further compare the intensities observed at sea by the two ships on the passage from Hobarton to Sydney, we find that a similar difference prevails in them; and we are therefore led to the conclusion, either that the needle of the Terror gained, or that the needle of the Erebus lost, a very small portion of magnetism, in the period between the observations at Hobarton in April 1841, and the departure of the Expedition from that port in the following July. Now experience has shown that a loss of magnetism is no unfrequent occurrence, whilst a gain is extremely rare, happening only, as far as we know, from such an accident as the contact of a needle with a more powerful magnet than itself. We may therefore conclude with great probability that the needle of the Erebus sustained a small loss of magnetism between April and July 1841, antecedent to all the observations of the voyage, causing the intensities derived with it, when computed in reference to the angles of deflection observed at Hobarton in April 1841, to require to be increased about one hundredth part, or more precisely 8 parts in 1000, in order

to bring them into strict relation with 1.82, taken as the value of the force at Hobarton. This correction being applied, all the intensities observed throughout the voyage by the two ships are in accordance (subject only to errors of observation), forming a consistent series of relative determinations, resting on 1.82 and 1.336, assumed provisionally as the values of the intensity at Hobarton and Port Louis, the commencing and concluding stations of the series. The correction is made in the Table which exhibits the intensities observed on board the two ships, and the geographical positions to which they belong; it is also made in the results inserted in the Map. The correctness of the values assumed at the base stations, 1.82 at Hobarton and 1.336 at Port Louis, remains to be proved by absolute determinations which have yet to be made at those two stations. The absolute intensities observed by the Expedition itself, with the instruments and according to the method prescribed in the instructions of the Royal Society, certainly have not the necessary precision. preceding Number of these Contributions are stated the results of five determinations which were obtained by Captain Ross at Hobarton in 1840 and 1841, with the 15-inch magnets of his observatory magnetometers; and of twenty-two determinations obtained by Lieut. Kay at the magnetic observatory at that station, with similar instruments, Captain Ross's mean result was 4.573, the partial results in 1841 and 1842. varying from 4.491 to 4.626. Lieut. Kay's mean result in 1841 was 4.553, the partial results (ten in number) varying from 4.509 to 4.601; and in 1842 4.513, the partial results (twelve in number) varying from 4.443 to 4.568. In 1843 Lieut. Kay received the auxiliary apparatus supplied in compliance with the revised instructions of the Royal Society, published in 1842. The magnets of this apparatus were 12 inches in length. The following Table exhibits the results obtained with this instrument in thirteen determinations made with it, between June 23rd and July 1st, 1843. determination is deduced from two series of observations of deflection; in the first six instances the distances were 4.505 and 6.005 feet; in the remainder, 4.0 and 5.3 feet. The moment of inertia of the deflecting magnet was computed from the length, breadth and mass of the bar.

June 23.	4.509	J une 27.	4.557
24.	4.515	28.	4.505
24.	4.528	28.	4.504
26.	4.510	29.	4.549
26.	4.523	29.	4.527
27.	4.583	30.	4.466
		July 1.	4.479

Mean of the 13 determinations 4.520

Here also it is obvious, from the discrepancy of the partial results, that the angles of deflection afforded by these magnets at the prescribed distances, viz. the least distance being not less than four times the length of the bar, were still too small; and that before any final conclusion be arrived at, it is desirable that we should await the MDCCCXLIV.

results which will be obtained with the smaller apparatus described by Lieut. RIDDELL in his "Magnetical Instructions for the use of Portable Instruments," &c. In this apparatus the suspended and deflecting magnets are respectively 3.0 and 3.67 inches in length. Meanwhile we may derive, as a provisional value, the arithmetical mean of the four mean results already stated; allowing to each an equal weight, we have,

which, with the other necessary data stated in the preceding Number of these Contributions, would give the value of the total intensity at Hobarton 1.81 to 1.372 in London*.

* Since these pages were written I have received the details of the observations of ten distinct determinations of the absolute horizontal intensity at the magnetic observatory at Hobarton, made in August 1843 with deflecting and suspended magnets respectively of 9.18 inches and 7.50 inches in length. The deflecting distances were the same throughout, being 3.2893 and 4.3393 feet. The calculation of these observations not having been yet received from Lieut. KAY, the results have been computed by Lieut. RIDDELL, R.A., F.R.S., so far as the materials hitherto furnished permit. They give the value of X';—being the absolute horizontal intensity (X), uncorrected for the difference in the magnetic moment of the deflecting bar produced by the earth's inducing action in the different positions in which the bar is placed in the experiments of deflection and in those of vibration; viz. 1° perpendicular to the magnetic meridian, and 2° in the plane of the meridian. We owe the suggestion of a correction due to this cause to Dr. Lamont: but the necessary data for computing it, for the particular bars employed by Lieut. KAY on this, or on the former occasions, have not yet been received. Observations made at the Cape of Good Hope and at Woolwich, with similar bars, have given results which show that the correction may possibly prove to be of nearly the same amount for the larger and smaller bars, in which case the relative values will be but little affected, and we may estimate that the value of X at Hobarton will be about 0.02 less than X'. In the expression which has been employed in these Contributions for the absolute horizontal intensity (1.82+e at Hobarton and 3.72+e at London, e being a small quantity to be supplied hereafter), the correction here referred to will form a portion of e. The following Table exhibits the abstract of the observations made in August 1843 with 9.18 and 7.50 inch bars.

	De	eflecting Ma	ignet.		Bifilar Mag	
Gottingen Mean Time.	N T.	37.1 -	Temperature	Values of X'.	k=000229.	q = 000224.
·	No.	Value of m' .	during deflection.		Reading.	Temp.
d h					-	_
1843. Aug. 20 19.0	9.18 inch.	6.256	54.6	4.5052	165.1	5 2-0
21 11.5	9.18 inch.	.259	49.6	•5034	168.6	49.1
21 16:5	9·18 inch.	.251	51.9	•5043	165.3	49.1
21 19.5	9.18 inch	•261	53.7	•4993	168.3	50.0
22 11.0	9.18 inch.	$\cdot 227$	48.0	•5177	165.4	49.3
22 19.5	9.18 inch.	•243	54.5	•5025	164:6	50.7
23 10.8	9·18 inch.	.259	50.7	•4884	161.0	51.2
23 18.1	9·18 inch.	.244	52.4	•5005	162.2	51.0
	9·18 inch.	·240	52.0	. •4982	163.9	51.3
25 11.4	9·18 inch.	.252	49.4	•4953	165.3	51.5
		6.249	51.7	4.5015	165.0	50.5

The mean value of the results, 4.501, is considerably different from the mean deduced in the text from all

At the Falkland Islands there were two determinations of the absolute horizontal intensity made by Captain Ross at the Magnetic Observatory at Port Louis, one in September 1842, being 6.87, and a second in November of the same year, being 6.32. They were both made with 15-inch magnets; the angles of deflection were observed at four distances, but amounted only to 56'.8, 31'.9, 21'.4, and 12'.9 in the first experiment, and to 1° 49'.9, 1° 01'.6, 41'.5, and 25'.1 in the second experiment.

These values of the horizontal intensity would give that of the total intensity at Port Louis respectively 1.609 and 1.367. It is obvious that we can draw no conclusion whatsoever from these numbers, and that we must wait for the confirmation or correction of the value given by the needles of Mr. Fox's instrument, until absolute determinations can be procured with instruments capable of affording more satisfactory results. Steps have been taken to obtain such determinations at the Falkland Islands from Captain Sullivan, R.N., and at Sydney and New Zealand from the Surveying Expedition under Captain Blackwood, R.N.; when these arrive, we may learn whether any and what final correction will require to be applied to the intensities now provisionally deduced from the observations with Mr. Fox's needles, in the Erebus and Terror. We may expect to receive these determinations before the time when the results now presented to the Royal Society will have to be combined with those of the preceding and succeeding years, in a general calculation of the magnetic lines in the southern hemisphere.

2. With Deflectors.—In the Erebus, the spare needle R. F. 4 was employed,—as "deflector S," with its south pole opposite to the division of the circle which the south pole of the mounted needle had previously indicated as the dip;—and as "deflector N," with its north pole similarly applied to the opposite division of the circle. The angles of deflection varied in different localities during the voyage, in round numbers as follows:—Deflect. S from 52° to 71°; and deflect. N from 49° to 67°. For obtaining the equivalent weights to the deflecting force of the deflectors at these angles, we have the comparative observations with deflectors and weights at Hobarton, Sydney, New Zealand, the Falkland Islands, and on the ice in lat. —65° 47′, long. 202° 08′. The angles of deflection caused by the weights have been already stated;

the preceding observations; yet from the improvement which it is natural to suppose practice must have made in the observers, and from the reduced discrepancies of the partial results with the smaller bars, the mean of the ten results in August 1843 would seem entitled to a preference over the earlier and more numerous results. Judging by what has been done at Woolwich with the 2·45 and 3 inch magnets, and at the Cape of Good Hope with 3·0 and 3·67 inch, we may expect with them a still further and considerable reduction in the discrepancies of the partial results; but it would not be safe, with the comparisons which we have now before us, to feel full confidence that there will be no apparently constant or systematic difference between the results of the larger and smaller bars. Reviewing the whole subject, we can as yet, therefore, only consider ourselves as being in progress towards such accuracy in determining the ratio of the intensity at different places by the absolute method, as shall be superior to that with which it was previously obtained by the employment of well-selected needles in relative determinations.

those by the deflectors, with the equivalent weights deduced from the comparison, are collected in the following Table.

Station.	Date.	Intensity deduced by	b	deflection y		valent ghts.
		weights.	Def. S.	Def. N.	Def. S.	Def. N.
Hobarton Sydney New Zealand On ice Falkland Islands .	July 1841 Aug. and Oct. 1841 January 1842	1.939	56 28·6 59 10·2 61 46·9 54 03·1 71 11·8	53 02.6 55 37.0 57 59.0 50 35.0 67 10.3	grs. 7·39 7·05 6·84 7·65 6·10	grs. 7·08 6·77 6·58 7·30 5·93

By projecting these angles and weights, and proceeding in the manner described in the Third Number of these Contributions*, the values of w' in the following Table were obtained for each deflector, corresponding to each angle of deflection v'; and employing these values of w', the intensities I' entered in the general table of observations have been computed by the formula

$$I' = \frac{1.82 \sin 5\hat{6} \ 28.6}{7.39} \cdot w' \csc v' = 2.053w' \csc v'.$$

Besides the observations with the spare needle R. F. 4, employed as a deflector, angles of deflection were occasionally observed with the magnets N and S, belonging to the apparatus of the Erebus, used conjointly; their magnetism, however, was so much inferior to that of R. F. 4, that, even when both were used together, their joint effect was less than the half of either pole of R. F. 4; their results would consequently be much inferior in precision to those of R. F. 4, and I have not therefore employed them.

	D	ef. S.		,			D	ef. N.		
v'. u	'. v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	37 59 6 60 55 61 64 62 13 63 32 64	grs. 7·11 7 01 6·91 6·82 6·73 6·64 6·55	66 67 68 69 70 71 72	grs. 6 47 6 39 6 31 6 24 6 17 6 10 6 03	\$\frac{49}{50}\$ 51 52 53 54 55	grs. 7·49 7·38 7·27 7·17 7·07 6 97 6 86	56 57 58 59 60 61 62	grs. 6·76 6 67 6·57 6·48 6·40 6·33 6 26	63 64 65 66 67	grs. 6·19 6·13 6·06 6·00 5·94

In the Terror, the spare needle marked C was employed both as "deflector N" and "deflector S." The magnets belonging to the apparatus were also used, N separately, and N and S conjointly. Observations were also occasionally made with magnet S, but its magnetism was so feeble, and the deflections obtained with it consequently so small in comparison with the others, that the results are not entitled to the same confidence, and have not therefore been taken into the account. The equivalent weights have been obtained, as in the Erebus, from the comparative observations with weights and deflectors at Hobarton, Sydney, New Zealand, the Falkland

Islands, and on the ice in lat. -65° 47', long. 202° 08'. I have also, in the case of the Terror, availed myself of a comparison of the weights and deflectors made on the 3rd, 4th and 5th of December 1841, at sea, when the weather was extremely favourable, and the ship did not materially change her position. From the observations on these days we have as follows:—

December	Intensity	Angles of deflection by									
1841.	deduced by weights.	Def. N.	Def. S.	Mag. N.	Mag. N S.						
3 A.M. 3 P.M. 4 5	1·783 1·778 1·773 1·779	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	34 06·7 34 06·3 34 22·0 34 29·4	30 44·1 30 46·1 30 48·7 30 46·1	40 52·8 40 45·8 40 56·3 40 54·9						
Mean	1.778	36 42.5	34 16.0	30 46.2	40 52.5						

The several comparisons from which the equivalent weights are derived, together with the weights so derived, are collected in the following Table.

Station.	Date.	Intensity deduced by weights.	Angles of deflections by								Equivalent weights.				
			Deflector N.		Deflector S.		Magnet N.		Magnets N S.		Deflector N.	Deflector S.	Magnet N.	Magnets NS.	
Hobarton Sydney New Zealand At Sea On Ice Falkland Islands	April 1841 July 1841	1.778	38 39 36 33	05·9 36·8 42·5 47·6	35 36 34 31	15·7 57·8 16·0 16·1	31 32 30 28	47.2 50.8 46.2 52.7	41 42 40 38	45·3 58·4 52·5 45·7	2·736 2·675 2·773 2·829	grs. 2·613 2·560 2·525 2·613 2·640 2·324	grs. 2·391 2·336 2·276 2·374 2·456 2·042	grs. 3·059 2·953 2·861 3·036 3·184 2·510	

The equivalent weights for each deflector, and for each half degree of deflection, have been obtained in the manner already described, for the angles of deflection and equivalent weights in the preceding Table, and are subjoined; by their aid the intensities I' entered in the general table of observations have been computed by the formula

 $I' = 3832w' \csc v'$.

Def	N.	Def. S.						Magnet N.						Magnets NS.						
v'. w'.	v.	w'.	v'	·	w'.	v'	'.	w'.	v	′ .	w'.	v	'.	w'.	v	′.	w'.	ı	·.	w'.
33 30 2.834 34 00 2.826 34 30 2.817 35 00 2.809 35 30 2.800 36 00 2.777 37 00 2.765 37 30 2.753 38 00 2.738	39 30 40 00 40 30 41 00 41 30 42 00 42 30 43 00 43 30 44 00 44 30 45 00	2.660 2.638 2.615 2.593 2.571 2.548 2.524 2.488 2.448 2.423	31 32 32 33 33 34 34 35 35 36 36	30 00 30 00 30 00 30 00 30	2.639 2.634 2.627 2.619 2.611 2.602 2.591 2.580 2.567 2.554	38 39 39 40 41 41 42	00 30 00 30 00 30 00 30	2·485 2·464 2·444 2·423 2·403 2·382 2·361 2·341 2·321	28 29 30 30 31 31 32 32	30 00 30 00 30 00 30 00 30	2.464 2.446 2.426 2.406 2.387 2.367 2.346 2.323	35 35 36	00 30	2.126 2.085 2.040	37 38 39 39 40 41 41 42 42	30 00 30 00 30 00 30 00 30	3·240 3·210	44 45 45 46 46	00 30 00 30 00	2.766 2.714 2.660 2.604 2.544

General Remarks.—If we take a general view of the magnetic declination in the southern hemisphere, particularly in the best-known portion of it, comprised between the tropics and the Antarctic Circle, we find that the phenomena present the same obvious and decided features of a duplicate system as do those of the northern hemisphere. If, following any of the geographical parallels, we carry our attention round the hemisphere, we find it divided into four spaces, in which opposite characteristics in regard to the direction of the needle alternately present themselves. the spaces the change in the pointing of the needle, as the space is traversed in the direction of the parallel, is continuous and progressive towards the west, and in the other two continuous and progressive towards the east. If, for example, commencing with the meridian of 30° E. or thereabouts, we trace the parallel of -45° round the hemisphere, always proceeding in an easterly direction till we return to the meridian at which we began, we shall find that we first pass through a space in which the direction of the north end of the needle becomes progressively more and more easterly, either by the decrease of westerly or increase of easterly declination; we next pass into a second space, on entering which the continuity is broken, the progressive movement of the north end of the needle towards the east is arrested, and its direction becomes now more and more westerly as we advance; thence we pass, successively, into a third space which has the same characteristic as the first, and into a fourth which has the same as the second.

The spaces here spoken of must be distinguished from those which are characterized by the exclusive prevalence of either east or west declination: they have a more simple and pure magnetical relation, implying the predominance within each space of one or the other of the two systems of magnetic forces which govern the direction It may happen, or it may not happen, that in one of these spaces the of the needle. direction of the needle may coincide in some point or points with the geographical meridian; when this occurs, the space will comprise both east and west declination; when it does not happen, the declination throughout the space will be exclusively east or exclusively west as the instance may be: but in either case, the change in the direction of the needle is always continuous and uniform in character throughout the space. It is well known that if the magnetic declination be computed on the supposition of a single central magnetic axis, there will be found two, and only two such spaces in each hemisphere. The systematic discordance which the declinations in the northern hemisphere presented when compared with the declinations so computed, and their agreement with the phenomena deducible from a double system of forces, led Halley to embrace the latter hypothesis. The declinations in the southern hemisphere present an arrangement strictly analogous to that in the northern, and conduct to the same conclusion, be that conclusion what it may.

If, with Halley, we view the declinations in the Southern Pacific as principally influenced by the weaker system of forces, or by that to which is also to be ascribed the high intensity of the magnetic force in the same quarter, we should be prepared

to expect that if the geographical limits of the adjacent spaces, having the characteristics referred to, were determined at different epochs, the alteration in the position of the spaces, if any, would show the existence of a secular change in the system itself; that it would indicate the direction of such change; and, if the intervals were sufficiently long in reference to the precision with which the determinations were made, the average rate of the movement of translation might also be inferred.

In this view a knowledge of the geographical position of the limiting lines, or of lines drawn so as to separate one of these spaces from the next, may have a particular value. In the part of the Pacific Ocean which is now referred to, the separating lines, as for distinction they may be called, coincide nearly in direction with geographical meridians, and are therefore crossed nearly at right angles by vessels pursuing a course from east to west, or from west to east. Prior to our own times, the epoch of Captain Cook's voyages is perhaps that in which the observations of the declination in the Southern Pacific may be regarded with the most confidence. The determinations of that period have been collected by M. Hansteen into a map, of which he assigns the year 1770 as the mean epoch. It is one of those published in the Atlas of the Magnetismus der Erde, and comprehends the results obtained by Byron, CARTERET, WALLIS, Cook in three voyages, Ekeberg also in three voyages, and ABERCROMBIE. If in this map we draw lines separating the spaces which have the opposite magnetic characteristics referred to, and compare them with the corresponding lines which we may draw in Erman's map of the Declination in 1827-1830, published in the Magnetic Instructions of the Royal Society, we find an effect of secular change very distinctly shown in the altered position of the separating lines. These lines, A and B, are drawn in the accompanying Plate*, where the two epochs, 1770, and 1827-1830, are brought into comparison. In the map of 1827-1830, the separating lines occupy a considerably more westerly position than in the earlier map, the difference amounting to about 10° of longitude. Hence we are led to the conclusion, that the spaces in the Southern Pacific, distinguished by certain magnetic characteristics, undergo a movement of translation, of which the general direction is from east to west. This direction is the opposite to that in which the change is known to take place in the corresponding quarter in the northern hemisphere (viz. in the Siberian quarter), where the secular movement is from west to east.

We are not without earlier, though possibly it may be supposed less precise, evidence of the effect of secular change in the Southern Pacific. From Halley's chart of the variation lines for 1700, we are enabled to draw the separating line B for that epoch, when we find it to have been between the longitudes of 305° and 310°. In a still earlier map drawn by Hansteen for the year 1600 (Magnetismus der Erde, Atlas, No. 1), representing the observations of the very able and scientific navigators of that period, we find the position of the same line to have been about 333° of east longitude.

In the observations of Captain Ross's voyage, we have the most recent evidence of the progressive westerly movement of the magnetic phenomena in the Southern Pacific. The separating lines A and B, deducible from the observations in 1842, are seen in the Plate to be in both cases considerably to the west of those derived from the observations of 1827–1830.

The whole body of evidence therefore, from the earliest observations to the latest, is consistent in showing a progressive movement to the westward of the spaces in the Southern Pacific, characterized by certain magnetic peculiarities, which in Halley's view indicated the proximity and predominance of the weaker system of forces. It is worthy of notice that the rate of progression, deduced from the changes of position shown at the several epochs, differs much less from a uniform rate than might have been anticipated from the nature of the evidence we possess, even supposing the actual rate to have been uniform in nature; whilst the magnitude of the whole change which appears to have taken place since the phenomenon became the subject of observation, in round numbers 50° of longitude in two centuries and a half, can scarcely fail to fix the attention. These are facts which, when the true physical causes of the magnetism of the globe shall occupy the earnest attention of philosophers, will probably attain an importance which at present perhaps we scarcely sufficiently estimate. But an endeavour to place distinctly before our minds facts of which the explanation must be deemed an essential condition of a satisfactory solution of this great problem, may not be without its use even at the present time. It may be also useful to call the attention of navigators to the value which may hereafter attach to determinations which may be made with instruments which are on board every ship, and in constant employ for the ordinary purposes of navigation. The position of the lines separating the spaces which have been the subject of discussion, has the advantage of being even more easily determined by observations on board ship than that of any particular declination line; in crossing them, the declination, if previously decreasing, will then begin to increase, and if previously increasing will begin to decrease; the determination is therefore independent of compass error, which is a much more prevalent source of error than is generally supposed; and if the ship's course be steady for some days together, which in the latitudes in question is very frequently the case, it is also in a great measure independent of the disturbance occasioned by the ship's iron. A very cursory inspection of the general table of the declinations observed by the Erebus and Terror suffices to show that they must have crossed the separating line (A) about the 15th of March 1842, when their latitude was about -59° and longitude 221°; and the line (B) about the 27th or 28th of the same month in latitude about -59°, and longitude 275° *.

Should the circumstance occur that one of the separating lines in the course of its progressive change of place should pass over a magnetic observatory, the epoch of its passage would be precisely determined. There is some reason for believing that

^{*} The line A passes through the culminating points of the southerly inflexion of the declination lines, of which the present position is shown in the Declination Map at the close of this paper to be about 220° east longitude. The line B passes through the culminating points of the northerly inflexion of the declination lines about the longitude of 276°.

such an event is now taking place at the Cape of Good Hope. If we examine Erman's map of the Declination in 1827-1830, published in the magnetic instructions of the Royal Society, we find one of the separating lines in the neighbourhood of the Cape of Good Hope, and if we compare this map with those of earlier epochs, we find the position of that line progressively more and more to the east as we ascend in the order of time. Hence we should be led to expect that about this period it might be found to pass over the meridian of the Cape. The observations which have been made daily at the magnetic observatory at the Cape, since its establishment in 1841, give reason to believe that the westerly declination which had been increasing for above two centuries, attained its maximum in the year 1842 or 1843. In April 1841 the declination was 29° 05' west, in and April 1844 29° 06' west*. The earliest observations at the Cape with which I am acquainted, are those of Davis in 1605, and Keeling in 1609. (Purchas, Book iv. ch. 6. § 1. and Book iii. ch. 6. § 4.) According to these observations the declination in 1605 was 0° 30′ east, and in 1609 0° 12′ west . The line of no declination probably therefore passed over the Cape about the year 1607, and in 235 years the westerly declination has increased from 0° to 29°, (omitting the odd minutes,) or at an annual average rate of 7'.4. Observations at several intermediate epochs show that the progression of this change was at least not very far from being an uniform one. If we divide the whole period into four equal parts, we should have

In the appendix of Hansteen's Magnetismus der Erde, p. 24, we have the record of actual observations as follows:—

In the year 1667			$\mathring{7}$	15	W.
In the year 1724	•		$\begin{cases} 16 \\ 16 \end{cases}$	27	W.
In the year 1780					

We may therefore conclude that the westerly declination at the Cape, which for above 200 years had increased at an average rate of about 7'·4 a year, or a degree in about eight years, has been for the last three years nearly stationary, having arrived at a maximum of 29° and a few minutes about the year 1843; and that a decreasing progression may now be expected \cdot\(\text{.} \). Ships passing the Cape, on a voyage to the

^{*} The observations at the magnetic observatory at the Cape of Good Hope, preparing for the press, will show the mean declination in each month of the years referred to.

[†] See also, for the latter observation, Hansteen's Magnet. der Erde. Anhang. S. 146.

[‡] Captain FitzRoy observed 28° 30' in 1836; at that epoch, consequently, the maximum had not been reached. Sir Edward Belcher, in 1842, observed 29° 13'.

east, will find that the westerly variation, which increases the whole way from the Brazils to about the meridian of the Cape, begins there to diminish, and continues to diminish, passing into easterly variation increasing, for above 100 degrees of longitude east of the Cape. The separating line which now passes through the Cape divides spaces distinguished by opposite magnetic characteristics; on the west side of the Cape the north end of the needle moves to the west, and on the east side to the east, as east longitude increases.

The maps which exhibit the results of the observations in the two ships, of the Declination, Inclination and Intensity, in the voyage of 1841–1842, and the isogonic, isoclinal, and isodynamic lines traced approximately in conformity with them, are a continuation of the maps published in No. V., which embodied in a similar manner the results of the preceding voyage. The results in the Erebus are distinguished from those in the Terror by a different character, for the purpose of permitting the degree of accordance in the two series of independent determinations to be readily judged of by the eye. These maps afford the best reply to those who have expressed doubts of the success of observations of the inclination and intensity made at sea.

Magnetic lines, drawn from observations made in parts of the globe to which observation had not previously extended, are the proper test by which we may judge of the degree of approximation with which the values of the numerical elements have been obtained in a general mathematical theory of terrestrial magnetism, such as M. Gauss's. The portion of the observations of the Antarctic Expedition which has been placed before the Royal Society in No. V. and in the present number of these Contributions, permits us already to form some conclusion on this point. Plate XIII. exhibits the lines of one of the magnetic elements, i. e. the intensity, computed by M. Gauss's theory, and drawn in Plates XVIII. and XIX. of the Atlas des Erdmagnetismus, compared with the lines which are the direct results of observation.

The very imperfect resemblance between the two systems of lines is of course no impeachment of the sufficiency of the theory, with corrected numerical elements, to represent the natural phenomena in parts of the globe which observation may not have reached. The degree of approximation to which it will do this must depend upon the extent and correctness of the observation-basis from whence the numerical elements are derived, and upon the order of the magnitudes comprehended in the calculation.

The evidence which the plate affords, that the calculations in the elaborate work referred to differ so widely from the facts in the southern latitudes, shows how much observations were wanting in those latitudes for the purpose of perfecting the theory; and is an ample justification (if indeed any justification were necessary) of the exertions which the last few years have witnessed to obtain them.

Since these pages were written I have received from Mr. Archibald Smith the following note. Regarding it as a continuation of the memorandum with which he

was so obliging as to favour me, printed in the last number of these Contributions, I avail myself of this oportunity of giving it an early circulation.

"The apparent changes in the values of the constants a, b, c and d, in the Erebus and Terror (Contributions, No. V., p. 153), seem to show that those vessels had an appreciable quantity of magnetism, which was so far permanent, as to retain for a considerable time traces of the inductive force to which they had been exposed, and perhaps some strictly permanent magnetism. It seems, therefore, desirable to introduce into the expressions in the memorandum printed at p. 147 of Contribution No. V., terms which will represent such forces.

"Suppose, then, as in the memorandum, that φ represents the total magnetic force of the earth at the place of observation, θ the inclination, ζ the azimuth of the ship's head, reckoning from N. to W., and that φ' , θ' , ζ' represent the values of the same quantities shown by an instrument at a fixed position in the vessel, and affected by the attraction of the iron in the vessel; and let P, Q, R represent the attraction of the permanent magnetism in the vessel to the bow, to the starboard side, and vertically downwards. The fundamental equations of the former memorandum become by the introduction of these terms,

$$\varphi' \cos \theta' \cos \zeta' = \varphi \left[A' \cos \theta \cos \zeta + B \cos \theta \sin \zeta + C \sin \theta \right] + P$$

$$\varphi' \cos \theta' \sin \zeta' = \varphi \left[D \cos \theta \cos \zeta + E' \cos \theta \sin \zeta + F \sin \theta \right] + Q$$

$$\varphi' \sin \theta' = \varphi \left[G \cos \theta \cos \zeta + H \cos \theta \sin \zeta + K' \sin \theta \right] + R.$$

"In these equations A', B, C, D, E', F, G, H and K' are constants depending on the distribution of the soft iron in the ship, and perhaps on the temperature and other circumstances.

"If we suppose, as before, that the soft iron is symmetrically disposed, the equations (1.) (2.) and (3.) of the former memorandum become,

$$\frac{\phi' \sin \theta'}{A' \phi \cos \theta} = c \cos \zeta + d \tan \theta + \frac{R}{A' \phi \cos \theta} \cdot \cdot \cdot \cdot \cdot \cdot \cdot (3.)$$

"Let H represent the horizontal force $= \varphi \cos \theta$, H' the affected horizontal force $= \varphi' \cos \theta'$, and let $a \tan \theta + \frac{P}{A'H} = L$, $\frac{Q}{A'H} = M$, and $d \tan \theta + \frac{R}{A'H} = N$. The last equations become

$$\frac{H'}{A'H}\cos\zeta' = \cos\zeta + L \quad . \quad . \quad . \quad (1 a.)$$

$$\frac{H'}{A'H}\sin\zeta' = b\sin\zeta + M (2 a.)$$

$$\frac{H'\tan\theta'}{A'H} = c\cos\zeta + N (3 a.)$$

"By the introduction of the same quantities, the equations numbered from (4.) to (14.) in the former memorandum become

$$\frac{H'}{A'H} = \cos \zeta \cos \zeta' + b \sin \zeta \sin \zeta' + L \cos \zeta' + M \sin \zeta' \quad . \quad . \quad (4.5)$$

and representing $\zeta - \zeta'$, or the deviation, by δ ,

$$\sin \delta = \mathbf{L} \sin \zeta' - \mathbf{M} \cos \zeta' + (1 - b) \sin \zeta \cos \zeta' (6.)$$

$$= \frac{2}{1+b} L \sin \zeta' - \frac{2}{1+b} M \cos \zeta' + \frac{1-b}{1+b} \sin (\zeta + \zeta') (7.)$$

$$= (\cos \zeta + \mathbf{L}) \sec \zeta' \tan \theta' (10.)$$

$$= \sqrt{(\cos \zeta + L)^2 + (b \sin \zeta + M)^2} \cdot \tan \theta \cdot . \quad . \quad . \quad . \quad (11.)$$

$$\tan \theta' = \frac{c}{b} \cdot \frac{\cos \zeta + \frac{1}{c} N}{\sin \zeta + \frac{1}{b} M} \sin \zeta' (12.)$$

$$= c \frac{\cos \zeta + \frac{1}{c} N}{\cos \zeta + L} \cdot \cos \zeta' (13.)$$

$$= \frac{c \cos \zeta + N}{\sqrt{(\cos \zeta + L)^2 + (b \sin \zeta + M)^2}} \cdot \cdot \cdot \cdot \cdot \cdot \cdot (14.)$$

" Equation (7.) may also be put under the form

$$\sin \delta = \frac{2}{1+b} \sqrt{\mathbf{L}^2 + \mathbf{M}^2} \sin (\zeta' - \mu) + \frac{1-b}{1+b} \sin (\zeta + \zeta'),$$

$$= \frac{2}{1+b} \mathbf{L} \sec \mu \sin (\zeta' - \mu) + \frac{1-b}{1+b} \sin (\zeta + \zeta'),$$

where

in which $\tan \mu = \frac{M}{L}$, and μ represents the displacement of the line of no deviation towards the starboard side.

"By means of these equations we can determine A', L, b, M, c, N, from observations made at sea alone. The first four of these quantities furnish the corrections for the horizontal force and the declination. There is greater difficulty in obtaining the correction for the inclination. It will be observed that θ only occurs in these equations involved in the quantities L and N. If there were no permanent magnetism in the vessel, it would be necessary, in order to determine the correcting factors a and d, that observations of the inclination on shore, and corresponding observations on board, should be made in at least one magnetic latitude. If there is any appreciable permanent magnetism, observations of the inclination on shore and on board, and of the horizontal force, should be made in at least two magnetic latitudes. This would be sufficient if a, P, d, R remained absolutely constant. As that appears not to be

the case, as many observations as possible should be made of the inclination on shore and on board, with corresponding observations of the horizontal force. Such observations should be made with great care when the vessel is on or near the magnetic equator and before and after any rapid change of magnetic latitude, and whenever the vessel returns to a place where the observations have been made before on board the same vessel, under the same circumstances as to the distribution of her iron.

"When the permanent magnetism is symmetrically distributed, Q = 0 and M = 0, and the other constants may be easily, and probably with great accuracy, determined from the following equations. The small letter suffixed to the symbol of a function indicating the affected value observed with the vessel's head on the N., W., S., E. (affected) points,

$$d \tan \theta + \frac{R}{A'H} = N = \frac{H_n \tan \theta_n + H_s \tan \theta_s}{H_n + H_s} \cdot \cdot \cdot \cdot \cdot \cdot \cdot (18.)$$

$$c = \frac{H_n \tan \theta_n - H_s \tan \theta_s}{H_n + H_s} \cdot \cdot \cdot \cdot \cdot \cdot (19.)$$

"The values of H_n , H_s , H_s , H_w , are given by the square of the number of vibrations of a horizontal needle made in a given time, and beginning to vibrate in a given arc, and require no correction except for temperature.

"If n, s, represent the number of vibrations made by such a needle in the same time, with the ship's head successively on the north and south points, and if Δ represent the value of δ when $\zeta' = \pm 90$, the values of L and Δ are given by the following simple expressions:—

" If
$$\tan \lambda = \frac{n}{s}$$
,

$$L = \cos 2 \lambda$$
. (20.)

$$\Delta = 90^{\circ} - 2 \lambda$$
. (21.)

The equations (18.) and (19.) may be put under the form

$$d \tan \theta + \frac{R}{A'H} = N = \frac{\varphi_n \sin \theta_n + \varphi_s \sin \theta_s}{\varphi_n \cos \theta_n + \varphi_s \cos \theta_s} \cdot \cdot \cdot \cdot \cdot (22.)$$

$$c = \frac{\varphi_n \sin \theta_n - \varphi_s \sin \theta_s}{\varphi_n \cos \theta_n + \varphi_s \cos \theta_s} \cdot \cdot \cdot \cdot \cdot (23.)$$

and the values of N and c obtained, but probably with less accuracy, from observations of the total intensity and inclinations made with a Fox's instrument.

"Note.—The last equation in the former memorandum is erroneous. The value of ψ cannot be obtained from two observations of the true azimuth of the ship's head, when $\zeta_1' + \zeta_2' = 180$, independently of a."

General Table of the Declinations observed on board Her Majesty's Ships Erebus and Terror, between May 1841 and August 1842.

Lat.	Long.	Ship.	No. of observa- tions.	Declina- tion.	Lat.	Long.	Ship.	No. of observations.	Declina- tion.
· /	0 /			o /	°C 1'0	or's to	T 1	1.0	$-1^{\circ}4$ 47
42 52	147 24	On shore		-10 24	-56 19 -56 54	211 53	Erebus. Erebus.	18 8	$-14 \ 47$ $-13 \ 32$
42 32	14/ 24	at Ho-		-10 24		212 25	Terror.	10	-15 32 $-15 14$
-43 30	147 20	Terror.	4	-12 35	-57 16		Erebus.	13	$-13 \ 14$ $-13 \ 54$
$-42 \ 40$	148 45	Erebus.	2	-10 06	-58 21	213 00	Terror.	9	-17 34
		Terror.	5	-11 49	-58 20		Erebus.	12	-14 37
		Erebus.	2	-951	-6249	212 13	Erebus.	12	-20 14
-40 51	149 21	Terror.	5	-11 11	-6246		Terror.	15	-20 03
•		Erebus.	10	-11 01	-63 19	1 1	Erebus.	6	-20 39
		Terror.	8	-10 38	-63 23	210 05	On ice.	5	-19 59
-37 14		Erebus.	13	-931	-63 23	209 43	Erebus.	14	-20 44
-37 10	151 32	1	10	-11 32	-63 21	209 48 206 55	Terror.	17	$ \begin{array}{r rrr} & -20 & 56 \\ & -22 & 00 \end{array} $
$-33 \ 51$	151 17	On shore		- 9 51	$ \begin{array}{rrr} -64 & 29 \\ -64 & 48 \end{array} $	206 10	Erebus. Terror.	9	-22 55
-00 01	101 1/	$\left\{\begin{array}{c} \text{at Syd-} \\ \text{ney.} \end{array}\right\}$	• • • •	- 3 31	-64 54		Erebus.	8	-22 51
-33 56	151 00	Terror.	4	-11 18	-65 14		Erebus.	8	$\begin{bmatrix} -22 & 51 \\ -21 & 51 \end{bmatrix}$
-33 54		Erebus.	2	-10 07	-65 30		Erebus.	8	_22 46
	162 47		10	-14 26	-66 04		Erebus.	4	-24 13
-33 33		Erebus.	8	-12 02	-65 32	204 57	Terror.	7	-24 27
-33 41		Erebus.	8	-13 34	-66 22	203 40	Erebus.	11	-25 36
$-33 \ 48$			16	-13 40	-66 04		Erebus.	8	-2659
$-33 \ 32$			7	-13 27	$-66\ 10$		Terror.	7	-27 24
	168 04	- CALOA	12	-15 02	-66 16	204 39	Erebus.	10	-26 36 $-25 55$
$\begin{bmatrix} -33 & 42 \\ -34 & 15 \end{bmatrix}$	1	13100000	11	$\begin{vmatrix} -12 & 54 \\ -13 & 45 \end{vmatrix}$	-66 15 $-66 04$		Erebus.	16	-25 48
$-34 ext{ } 15 \\ -34 ext{ } 31$			9 11	$-13 45 \\ -13 56$	-66 02	204 00	Erebus. Terror.	18	-26 48
$-34 \ 31$ $-34 \ 32$			5	$-13 \ 42$	-66 00		Erebus.	11	-25 26
0.00	-, -,	On shore,		10 12	-6558		Terror.	11	-25 00
-35 16	174 00	Bay of		-13 36	-65 57	204 14	Erebus.	13	-25 24
		Islands.			-65 58	203 54	Terror.	11	-25 59
-36 39		Erebus.	11	-14 24	-65 55		Erebus.	17	-24 58
-38 03			10	-14 55	-65 47		On ice.	6	-25.15
-38 02		221010401	13	-14 44	-6559		Terror.	15	$-26^{\circ} 24$
-39 29			11	-1655	-67 38		Erebus.	9	-27 46
$-39 10 \\ -40 51$			13 11	$\begin{vmatrix} -14 & 43 \\ -12 & 57 \end{vmatrix}$	$\begin{bmatrix} -67 & 40 \\ -67 & 20 \end{bmatrix}$	1	Terror.	9 8	$\begin{vmatrix} -28 & 19 \\ -27 & 36 \end{vmatrix}$
	$183 \ 28$		19	$\begin{bmatrix} -12 & 57 \\ -15 & 13 \end{bmatrix}$	$\begin{bmatrix} -67 & 20 \\ -67 & 19 \end{bmatrix}$		Erebus.	11	-27 30 $-28 37$
-41 09 $-42 02$			11	-13 13 -14 24	$\begin{bmatrix} -67 & 19 \\ -67 & 19 \end{bmatrix}$		Terror. Erebus.	8	$\begin{vmatrix} -28 & 37 \\ -28 & 12 \end{vmatrix}$
	183 59	Erebus.	13	$-16 \ 35$	-67 20		Terror.	11	_28 33
-47 05			11	-15 17	-68 32		Erebus.	14	-30 25
-47 32	184 52	Erebus.	11	-15 45	-68 24	199 57	Terror.	13	-3243
-48 53	186 48	Erebus.	15	-16 23		199 45	Erebus.	13	$-32\ 33$
	188 32	Terror.	7	-1652			Terror.	7	-30 47
	189 00	1	8	-1751	$-70 \ 10$		Erebus.	9	-35 42
-49 57			7	-16 36			Terror.	11	$\begin{bmatrix} -38 & 55 \\ -38 & 21 \end{bmatrix}$
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		12	-18 23 $-18 18$			Erebus.	11 12	-38 21 $-38 17$
	$\frac{19z}{192}$ 30		8	$-16 \ 37$			Terror. Erebus.	10	$\begin{bmatrix} -38 & 17 \\ -37 & 35 \end{bmatrix}$
	194 53		18	-15 16			Erebus. Terror.	17	$\begin{bmatrix} -37 & 33 \\ -37 & 19 \end{bmatrix}$
-51 50			8	-15 14			Erebus.	ii	-36 28
	202 14		10	-13 58			Terror.	5	-40 45
-53 05	204 33	Terror.	11	-14 54			Erebus.	1	-45 37
$-53 \ 10$		Erebus.	12	-13 06			Terror.	2	-5148
	209 24		8	-14 26		173 14	Erebus.	3	-77 17
-56 20	211 40	Terror.	14	-15 14	1				

Observations of	Declination.	(Continued.)
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Lat. Long.	Ship. No. obser tion	a- becina-	Lat.	Long.	Ship.	No. of observations.	Declina- tion.
-75 40 174 56 -76 48 182 33 -76 54 182 17 -76 12 191 40 -76 42 194 37 -76 42 194 37 -76 46 194 40 -78 03 197 31 -77 57 197 54 -77 44 198 07 -75 17 195 06 -74 49 193 56 -71 56 186 36 -71 56 186 36 -71 08 184 54 -70 58 184 03 -70 10 180 20 -69 50 180 16 -68 17 183 27 -68 02 183 35 -67 30 185 00 -67 25 186 42 -65 51 190 25 -65 07 192 24 -63 33 194 53 -62 26 195 40 -62 20 196 15 -61 00 199 00 -61 02 199 25 -60 20 205 12 -60 26 203 26 -60 16 212 59 -60 05 213 51	Terror. 5 Erebus. 6 Terror. 2 Erebus. 10 Terror. 8 Erebus. 10 Terror. 8 Erebus. 10 Terror. 5 Erebus. 6 Erebus. 2 Erebus. 5 Terror. 3 Terror. 3 Terror. 7 Erebus. 12 Erebus. 14 Terror. 4 Terror. 6 Erebus. 7 Erebus. 17 Erebus. 17 Erebus. 18 Terror. 4 Terror. 4 Terror. 4 Terror. 4 Erebus. 5 Terror. 4 Erebus. 5 Terror. 4 Erebus. 5 Terror. 4 Erebus. 6 Erebus. 6 Erebus. 7 Erebus. 10 Erebus. 11 Erebus. 12 Erebus. 13 Erebus. 14 Erebus. 4 Erebus. 4 Erebus. 4 Erebus. 4 Erebus. 4	-76 03 -86 23 -82 28 -70 22 -79 57 -81 23 -88 01 -88 08 -64 33 -62 17 -45 11 -39 20 -38 26 -30 50 -27 32 -28 50 -29 46 -27 32 -25 02 -23 40 -21 57 -19 41 -19 51 -19 49 -18 20 -17 31 -17 19	-58 58 -59 04 -60 18 -60 14 -60 02 -59 17 -58 28 -58 40 -58 36 -58 46 -59 00 -59 01 -59 02 -59 04 -58 55 -58 21 -58 30 -58 30 -58 32 -58 29 -57 35 -56 46 -52 14 -52 16	222 00 227 00 229 00 236 30 240 31 245 40 251 52 255 20 257 50 258 07 267 56 268 34 272 04 272 04 276 26 279 48 280 27 282 05 283 40 283 33 288 54 294 30 301 06 301 53	Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Terror. Erebus. Terror. Terror. Erebus.	4 1 4 3 3 1 1 4 3 4 7 3 8 9 1 4 5 7 10 8 7 8 10 8 10 8 10 10 10 10 10 10 10 10 10 10 10 10 10	-16 03 -17 01 -17 49 -20 57 -20 56 -20 48 -20 14 -22 46 -21 47 -23 28 -24 46 -26 13 -25 25 -26 25 -26 17 -26 51 -27 13 -27 04 -26 18 -28 25 -27 13 -25 04 -26 18 -26 18 -26 18 -26 18 -26 18 -26 18 -26 18 -26 29 -17 36

^{*} The mean monthly results with the magnetometers of the Expedition at the observatory at Port Louis at the Falkland Islands were as follows:—

The easterly declination appears to be decreasing very rapidly at the Falkland Islands.

General Table of the Inclinations observed on board Her Majesty's Ships Erebus and Terror, between May 1841 and August 1842.

Lat.	Long.	Ship.	No. of observations.	Inclination.	Lat.	Long.	Ship.	No. of observations.	Inclination.
$-\mathring{43} \stackrel{\circ}{00}$	148 28	Erebus.	5	-7°0 2′5	$-40^{\circ} 47$	102 02	Erebus.	5	-62 21
-43 00 $-42 43$		Terror.	5 8	$-70 25 \\ -70 44$		183 05	Terror.	15	$-62 \ 21$ $-61 \ 56$
$-42 \ 13$	1 1	Erebus.	}	$-69 \ 37$	$-40 \ 4z$ $-41 \ 34$	1 1	Terror.	7	-62 57
-42 13 -40 51	1	Terror.	5 4	-69 05	-41 49		Erebus.	5	-63 28
		Erebus.	t :	-69 05 $-68 41$		1 _1			$-63 \ 46$
-4055	149 12		4				Terror.	7	$-64 \ 44$
-38 17		Terror.	4	-6657		183 03	Erebus.	5	
-3750	1 . 1	Erebus.	4	-66 36	-43 56	1 1	Terror.	15	-65 22
-3728	151 30	Terror.	4	-66 22	-45 40	183 20	Erebus.	5	$-66 \ 35$
-37 21	151 33	Erebus.	5	-66 01		183 18	Terror.	14	-66 43
-36 21	151 39	Terror.	3	-66 11		184 40	Erebus.	5	-67 56
-36 01	151 48	Erebus.	4	-6504		184 42	Terror.	14	-67 32
-34 06	1	Terror.	4	-6258		186 25	Terror.	15	-68 40
-3351		Erebus.	19	-6247	$-48 \ 43$		Erebus.	6	-69 05
$-33 \ 51$	1 7	Terror.	7	-62 59*	-	187 23	Terror.	15	-68 59
-33 51	151 17	Erebus.	8	-62 48*	-49 23	188 29	Erebus.	9	$-69 \ 41$
-3351		Terror.	11	-6252		189 19	Terror.	14	-68 55
$-33 \ 51$		Erebus.	7	-6242		191 20	Terror.	14	$-68 \ 43$
-33 58		Terror.	8	$-62 \ 30$	-50 24		Erebus.	10	$-69 \ 43$
_		Erebus.	5	-6247	-50 38		Terror.	14	-69 25
-33 56	156 38	Terror.	4	$-61 \ 46$	-5148		Terror.	15	-69 51
$-33 \ 51$		Erebus.	5	-62 07		196 20	Erebus.	10	-70 21
$-33 \ 31$	160 20	Terror.	4	-61 04	-5228	199 05	Terror.	11	-70 10
-33 27	160 43	Erebus.	5	-61 30	-5251	203 56	Terror.	8	-70 01
-3342	164 05	Terror.	4	-60 52	-5254	203 00	Erebus.	11	-7044
-33 38	163 42	Erebus.	5	$-60 \ 48$	-53 01	205 08	Erebus.	6	$-70\ 10$
-33 38	166 28	Erebus.	5	-60 07	-5312	205 40	Terror.	15	-69 52
-3344		Terror.	10	-5955	-54 31	208 46	Terror.	11	$-70\ 10$
-33 33	167 38	Terror.	9	-5958	-5453	209 24	Terror.	12	-70 21
-33 22		Erebus.		-5939	-55 01	209 47	Erebus.	10	-7058
-33 00	1	Terror.	9	-58 43	-55 50	211 10	Erebus.	10	-71 28
-3258		Erebus.		-5904	-5614	211 43	Terror.	14	$-71 \ 41$
-3212		Erebus.		-58 33	-5639		Erebus.	10	-72 18
-3211		Terror.	11	-5728	-5606		Erebus.	6	-7208
$-33\ 57$		l		-5824	-56 40		Terror.	12	-72 00
-33 55			5	-5824	-57 06		l .	12	-72 14
-34 29		·		-58 26	-5757			10	-7309
	172 06		7	-58 14	-58 38			11	$-73 \ 45$
-34 15			10	-58 48	-58 39			11	$-73 \ 45$
	173 43		7	-59 00	-61 12			14	-75 32
	174 00	1	3	-59 36	-6118			11	$-75 \ 32$
	174 00			-59 31†‡				8	$-76 \ 37$
	174 00		14	-59 251	$-62 \ 40$			7	$-76 \ 36$
	174 23		(-59 28	$-63 \ 11$			12	$-70 \ 30$ $-77 \ 37$
	176 17		12	-59 20	-63 23			5	-77 26
_36 07	177 34			-59 54			Erebus.	4	-77 25§
30 2/	177 54	Erebus.		-60 34	-63 23			3	-77 239 $-77 30$
_ 20 16	179 51	Terror.	15	$-60 \ 37$	-62 26	200 00	Terror.	10	-77 53
	182 17		17	$-60 \ 37$ $-61 \ 21$	$-63 \ 49$			10	-77 56
	182 30		11	$-61 \ 34$	$-63 \ 47$			5	
	182 57		16	$-61 \ 15$	-64 25			1	-77 57
-09 ZI	100 01	Terror.	10	-01 10	-04 23	200 29	Terror.	14	-78 30

^{*} On shore at Garden Island, Sydney; inclination by needles whose poles were reversed, -62° 49'·1.

[†] Correct; in page 174 it is printed by mistake -59° 29'.

[‡] On shore at the Bay of Islands, New Zealand; inclination by needles whose poles are reversed, -59° 31'.9.

[§] On ice; the inclination observed with needles whose poles were reversed, was -77° 23'.3.

General Table of Inclination. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Inclination.	Lat.	Long.	Ship.	No. of observations.	Inclination.
-64 42	206 17	Erebus.	0	-78 20	-69 53	182 51	Terror.	- 7	$-8\overset{\circ}{4}\overset{\circ}{09}$
	1 - 1	Erebus.	8	-78 20 $-78 57$		181 09	Erebus.	7	$-84 09 \\ -84 06$
	206 03 205 04	Terror.	11			180 57	Terror.	9 8	-84 20
	1 1	Terror.	15 13			181 46	Erebus.	6	-85 04
	204 19	Terror.				1	Terror.		
	204 19	Terror.	13 11	$-79 28 \\ -79 30$		181 50 181 03	Terror.	9	$-84 59 \\ -85 22$
	204 08	Erebus.		$-79 \ 30 \\ -79 \ 31*$		180 06	Erebus.	9	$-86 \ 02$
-65 59	204 03	Terror.	22	$-79 \ 39$		173 36	Erebus.	$\tilde{\tilde{6}}$	-86 52
	204 03 203 50	Terror.	8_ 10	$-79 \ 39$ $-79 \ 39$		173 40	Terror.	13	-87 05
-66 06	203 30	Erebus.	12	-79 53		173 08	Erebus.	5	-86 59
-66 19	203 41	Terror.	12	$-80 \ 01$		175 13	Erebus.	6	$-86 \ 44$
	203 09	Erebus.	13	-79 57		174 58	Terror.	8	-87 03
$-66 \ 21$	203 23	Terror.	6	-80 03		181 03	Erebus.	5	$-86\ 46$
	203 59	Terror.	9	-79 52		181 35	Terror.	8	-86 56
	203 34	Erebus.	42	-79 55	* -	184 30	Erebus.	6	-86 07
	1	Terror.	12	$-79 50 \\ -79 51$		184 58	Terror.	8	$-86 \ 30$
-66 01	204 02	Terror.	12	$-79 51 \\ -79 50$		191 10	Terror.	9	-85 59
-66 11	204 21	Erebus.	14	$-79 \ 44$		193 43	Erebus.	2	$-85\ 18$
-66 13		Erebus.	11	$-79 \ 34$		194 42	Erebus.	$\tilde{6}$	-85 25
-65 59	1,	Erebus.	14	-79 38	-7648	194 21	Terror.	15	-85 12
		Terror.	14	$-79 \ 47$	-77 05	194 38	Erebus.	5	-85 24
-6553		Terror.	10	$-79 \ 51$		197 25	Terror.	9	-84 49
-6611		Terror.	13	-7948		197 48	Erebus.	5	-84 49
-6612		Erebus.	8	$-79 \ 35$		199 24	Terror.	8	$-85 \ 35$
-6608	,	Terror.	11	$-79 \ 35$		193 45	Erebus.	6	-84 49
-6549		Erebus.	4	-79 47 †		1	1	9	-85 46
-65 50		Terror.	13	-79 38			!	5	-84 38
-6609	1	Erebus.	9	-79 33			Terror.	7	-85 08
-67 02		Terror.	12	-80 22	-72 01	187 35		5	-84 10
-66 39		Erebus.	6	-80 01	-71 01	187 37	Terror.	9	-84 56
-67 12		Terror.	10	-80 06	-7108	184 59		6	,-84 04
-67 36	204 00	Erebus.	9	-80 22	-71 12	184 20		10	$-84 \ 37$
	204 17	Terror.	15	-80 43	-6954	179 55		8	-84 30
-6747	204 17	Terror.	15	-80 48	-6952	180 04	Erebus.	5	-83 34
-67 16	203 20	Terror.	16	-80 44	-6944	179 53	Erebus.	5	-83 31
-67 19			11	-80 26		183 10		7	-82 26
	201 34	Terror.	18	—80 35		183 25		10	-82 13
-67 57		1	7	$-80 \ 46$	-67 37		3	15	-81 33
	199 57		14	-81 18	-67 31				-81 51
	199 52		11	-81 14	-67 09	1		7	-81 03
$-68 ext{ } 46$		l	11	-81 33		188 10		1	-81 02
-68 59		i		-81 54	-65 18			10	-7942
-6852			7	$-82\ 30$	-65 21		1	f	-79 19
	192 25			$-82 \ 35$	$-63 \ 30$			7	-78 30
	192 17		10	-83 00	$-63 \ 30$	194 29			-78 11
-70 05			9	-83 20	-02 17	195 5	Terror.	7	-77 30
	7 191 11		1	-82 51	-62 16	196 1	Erebus.		-7717
	6 189 00			-83 07	-61 06	198 0	Terror.		-7632
	8 186 01			-83 18	-61 11 60 50	1 198 4	Erebus.		-7634
-70^{19}			17	-83 23	-00 50	200 1	l Erebus.		-75 33
	185 31			$-83 \ 35$	-00 5	7 199 0			-75 08
	2 185 38		10	-83 30		204 4			-75 08 74 91
	1 183 50			$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	60 1	5 208 0	6 Terror. 4 Erebus		$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
-09 50	6 184 48	Terror.	8	-04 03	1 -00 1	J 211 4	r Erepus	• 0	-/4 21

^{*} The inclination observed in Lat. -65° 59', Long. 204° 14', with needles whose poles were reversed, was -79° 31'.0.

 $[\]dagger$ Observed on ice; inclination with needles whose poles were reversed, -79° 39'.5,

General Table of Inclination. (Continued.)

Lat. Long.	Ship.	No. of observations.	Inclination.	Lat.	Long.	Ship.	No. of observations.	Inclination.
-60 16 211 52 -59 58 216 28 -59 24 218 55 -59 07 219 12 -58 53 222 27 -59 04 228 09 -59 39 232 48 -59 45 233 55 -60 09 236 11 -60 16 236 11 -60 21 237 02 -60 22 237 14 -60 20 237 54 -60 01 241 31 -59 17 245 40 -59 11 246 37 -59 15 248 12 -58 26 251 42 -58 26 251 42 -58 26 251 42 -58 33 254 45 -58 35 255 10 -58 42 257 44 -58 45 257 58 -58 45 257 58 -58 58 267 18	Terror. Terror. Erebus. Terror. Erebus. Terror. Erebus. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror.	8 7 11 17 7 9 7 5 4 11 5 10 9 5 10 5 6 7 5 10 5 8	-74 14 -73 36 -73 38 -73 38 -73 38 -73 25 -72 57 -72 54 -72 51 -73 01 -73 00 -72 45 -73 08 -72 40 -71 29 -71 24 -71 26 -71 04 -70 55 -70 50 -70 16 -70 11 -69 50 -69 47 -68 00	-59 01 -58 54 -58 51 -58 25 -58 23 -58 31 -58 29 -58 36 -58 31 -57 21 -57 22 -57 26 -57 11 -56 37 -54 48 -54 50 -52 54 -52 34 -52 03 -51 42 -51 32	271 58 272 06 276 18 277 05 279 44 280 03 281 38 282 10 285 36 289 36 289 36 289 36 291 36 292 14 294 34 294 46 297 21 298 08 300 27	Erebus. Terror.	6 5 8 7 6 8 5 9 5 7 5 8 6 7 5 7 4 5 5 3 7 8 2 5	-67 39 -67 01 -66 53 -66 10 -65 27 -64 44 -63 48 -63 41 -63 00 -63 05 -61 36 -61 15 -59 52 -58 51 -59 02 -59 01 -59 52 -59 01 -50 48 -52 36* -52 15*

^{*} Observed on shore at the Falkland Islands; the Inclination with needles whose poles were reversed, was $52^{\circ} 26'2$.

General Table of the Intensity of the Magnetic Force, from the observations made on board Her Majesty's Ships Erebus and Terror, between April 1841 and August 1842.

Lat.	Long	Ship.	No. of ob-	Intensity.	Lat.	Long	Ship.	No. of ob-	Intensity.
Lat.	Long.	Snip.	servations.	London = 1.372.	Lat.	Long.	smp.	servations.	London = 1.372.
0 /	0 /				· ,	0 /			
-43 00	148 28	Erebus.	2	1.853		183 06	Terror.	8	1.707
-43 03	148 20	Terror.	2	1.849	-45 39	183 18	Terror.	8	1.733
-42 13	149 29	Erebus.	2	1.823	-4629	184 00	Erebus.	4	1.744
-4224	149 30	Terror.	2	1.822		184 37	Terror.	8	1.753
-4054	149 13	Erebus.	2	1.818	-48 18	185 54	Terror.	10	1.772
-40 51	149 28	Terror.	2	1.814	-49 04	187 11	Erebus.	7	1.767
-38 17	150 22	Terror.	2	1.795		186 54	Terror.	10	1.772
-37 31	151 09	Erebus.	3	1.769	-49 27	189 13	Erebus.	5	1.773
-3728	151 30	Terror.	2	1.758	-4924	187 23	Terror.	11	1.772
$-34 \ 35$	151 30	Erebus.	3	1.734	-49 27	189 51	Terror.	14	1.775
	151 25	Terror.	3	1.738	-49 50	190 46	Terror.	10	1.766
	151 17	Erebus.	14	1.698*	-50 14	191 06	Erebus.	7	1.780
	151 17	Terror.	16	1.699*	8	191 39	Terror.	6	1.771
•	151 17	Erebus.	6	1.719	-5042	192 11	Terror.	14	1.777
	151 17	Terror.	4	1.719	-51 34		Erebus.	5	1.806
	154 07	Erebus.	2	1.708		194 00	Terror.	10	1.794
	153 35	Terror.	4	1.703	-52 13		Terror.	9	1.799
	157 18	Erebus.	2	1.680	-5243	201 40	Erebus.	7	1.822
	156 38	Terror.	2	1.679	-5252	204 31	Terror.	20	1.820
	160 43	Erebus.	2	1.668		205 08	Erebus.	$\tilde{5}$	1.825
	160 20	Terror.	2	1.671		206 14	Terror.	10	1.834
	163 42	Erebus.	2	1.655		209 16	Terror.	13	1.814
	163 50	Terror.	$\frac{\tilde{4}}{4}$	1.658		210 00	Erebus.	6	1.846
•	166 23	Erebus.	2	1.638		211 43	Terror.	8	1.836
$-33 \ 44$		Terror.	5	1.627	-56 38	211 30	Erebus.	8	1.851
	167 40	Erebus.	2	1.630		211 50	Terror.	10	1.841
	167 37	Terror.	5	1.600		212 06	Terror.	8	1.843
	169 20	Erebus.	2	1.620		212 40	Erebus.	4	1.866
	169 20	Terror.	4	1.604		212 59	Terror.	8	1.863
	171 02	Terror.	6	1.589		213 09	Terror.	14	1.878
. 3	171 52	Erebus.	6	1.596	$-58 \ 45$	213 19	Erebus.	7	1.888
*	1 : - 1	Terror.	6	1.601		213 52	Terror.	14	1.892
		Terror.	5	1.597	$-61 \ 20$	213 57	Erebus.	4	1.923
-34 13 $-34 24$		Terror.	4	1.619	$-62 \ 34$	212 34	Terror.	10	1.916
9	1	Erebus.	26	1.607+		212 53	Erebus.	2	1.937
-35 16	174 00	Terror.	24	1.608+		209 37	Terror.	8	1.910
-35 16	174 00	Terror.	2	1.610		210 02	Erebus.	2	1.952
	174 00	Erebus.	2	1.620		210 02	Erebus.	2	1.938
	177 27	Terror.	4	1.616		207 33	Terror.	8	1.927
	173 39	Erebus.	2	1.624		208 26	Erebus.	$\stackrel{\circ}{6}$	1.945
	175 39	Erebus.	$\begin{bmatrix} z \\ 2 \end{bmatrix}$	1.625		206 36	Erebus.	8	1.948
$-30 \ 27$ $-38 \ 13$		Terror.	8	1.634		206 19	Terror.	8	1.943
1	1 - 1	****	2	- 0-1-	-65 26				1.931
$-38 17 \\ -38 54$		Erebus. Terror.	10	1.627 1.640	-66 00	204 00	Terror. Erebus.	8 15	1.971
-38 34 $-39 10$		Erebus.	4	1.628	-65 50		Terror.	8	1.950
$\begin{bmatrix} -39 & 10 \\ -40 & 02 \end{bmatrix}$		Terror.	16	1.652	-66 33	003 00	Erebus.		1.981
-40 02 $-40 47$		Erebus.	2	1.672	-66 09	203 51	Terror.	4 5	1.949
$-40 \ 47$ $-41 \ 34$		Terror.	10	1.666	-66 09	200 01	Erebus.		1.970
-41 34 $-41 49$	100 40	Erebus.	2	1.684	-66 07	204 00	Terror.	11	1.944
$-41 49 \\ -42 40$		Terror.	$\frac{z}{4}$	1.682	-66 10	003 50	Erebus.	18	1.973
$-42 \ 40$ $-43 \ 32$			2	1.714	-65 57	203 KE	Terror.	12 14	1.949
	100 09	Elenus.	2	1 / 1 1	-00 07	~00 00	Terror.	14	1 343

^{*} On shore at Garden Island, Sydney.

[†] On shore at the Bay of Islands, New Zealand.

[‡] Observed on ice.

General Table of the Intensity of the Magnetic Force. (Continued.)

Lat	Long	Shin	No. of ob-	Intensity.	Tot	Long	Chin	No. of ob-	Intensity.
Lat.	Long.	Smp.	servations.	London = 1.372.	Lat.	Long.	Smp.	servations.	London = 1.372.
-68 29 -68 46 -68 52 -69 29 -70 00 -70 14 -70 18 -70 23 -70 27 -70 28 -72 41 -72 46 -74 58 -75 05 -75 42 -76 33 -77 02	202 02 202 08 203 40 204 17 204 12 202 15 202 24 201 34 199 57 199 55 199 39 198 24 191 36 196 16 185 16 185 33 181 20 181 41 181 46 173 34 173 17 174 14 180 09 181 37	Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Terror. Terror. Erebus. Terror.	12 6 10 8 10 10 6 6 8 8 9 13 10 8 9 15 10 8 9 15 10 8 4	1.945 1.959 * 1.948 * 1.976 1.960 1.965 1.967 1.946 1.935 1.955 1.995 1.996 1.966 2.001 1.965 1.966 2.001 1.965 1.983 1.996 1.988 1.999 2.001 1.988 1.999 2.001 1.989 2.008 2.024 2.006 2.021 2.007	$\begin{array}{c} -67 & 24 \\ -66 & 56 \\ -65 & 17 \\ -63 & 30 \\ -63 & 05 \\ -61 & 57 \\ -61 & 07 \\ -60 & 19 \\ -60 & 15 \\ -59 & 13 \\ -59 & 22 \\ -58 & 33 \\ -58 & 49 \\ -59 & 01 \\ -59 & 29 \\ -60 & 18 \\ -60 & 05 \\ -60 & 17 \\ -60 & 20 \\ -59 & 31 \\ -58 & 36 \\ -58 & 33 \\ -58 & 36 \end{array}$	203 42 207 52 209 55 216 28 218 14 220 27 221 25 227 43 231 53 236 31 235 56 236 38 237 55 247 29 247 27 245 13 251 42 254 45 255 30	Terror. Terror. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Terror. Terror. Erebus. Terror. Terror. Erebus. Terror.	10 8 4 10 4 6 14 7 4 4 8 4 4 7 4 4 6 6 6 6 4 4 4 7 4 4 8 4 4 7 4 6 6 6 6 7 4 7 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1.978 1.981 1.980 1.955 1.942 1.941 1.916 1.924 1.920 1.881 1.907 1.910 1.900 1.878 1.913 1.897 1.890 1.909 1.884 1.892 1.907 1.907 1.907 1.907 1.907 1.861 1.885 1.824 1.821
$\begin{array}{rrrr} -77 & 02 \\ -76 & 48 \\ -76 & 20 \\ -76 & 24 \\ -77 & 00 \\ -77 & 13 \end{array}$	181 37 184 46 191 26 184 54 194 38 193 52		1			255 30 258 13 267 50 272 06 272 35 276 18		1	
$\begin{array}{c cccc} -77 & 14 \\ -75 & 20 \\ -74 & 50 \\ -73 & 10 \\ -72 & 24 \\ -72 & 03 \\ -71 & 34 \\ -71 & 08 \end{array}$	189 21 188 47 187 40 186 09 184 59	Terror. Terror. Terror. Erebus. Terror. Erebus. Terror. Terror. Terror.	4 10 4 2 4 4 10 10	2·001 1·992 2·003 1·999 2·000 1·990 1·999 1·999 2·009	$\begin{array}{c} -58 & 27 \\ -58 & 27 \\ -58 & 36 \\ -57 & 23 \\ -57 & 16 \\ -55 & 42 \\ -56 & 03 \\ -52 & 40 \\ -52 & 54 \end{array}$	280 20 282 04 285 33 290 34 292 01 295 57 295 54 299 52 300 57	Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus. Terror. Erebus.	12 5 4 8 5 8 3 9 5	1.672 1.652 1.648 1.592 1.544 1.495 1.478 1.355 1.367
$ \begin{array}{r rrrr} -69 & 48 \\ -68 & 09 \end{array} $	179 55 179 56 183 10 183 25	Terror. Erebus. Terror. Erebus.	4 4 4 4	1·999 1·994 1·981 1·981	$-52 ext{ } 05 $ $-51 ext{ } 32 $ $-51 ext{ } 32$	301 39 301 53 301 53	Terror. Erebus. Terror.	8 24 30	1·340 1·333† 1·336†

^{*} Observed on ice,

[†] On shore at the Falkland Islands.

Declinations observed on board Her Majesty's Ship Erebus, between June 1841 and August 1842.

The Observers are distinguished in the column of Initials as follows:—R. Captain Ross; S. Lieut. Sibbald; W. Lieut. Wood; T. Mr. Tucker, Master; Sm. Mr. Smith, and O. Mr. Oakley, Mates; Y. Mr. Yule, Second Master. East Declination is characterised by the sign—.

1841.	Posit	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's	Declina-	Correction for index	True Declination.	Remarks.
	Lat.	Long.	Ini	observed.	sinp s neau.		attraction.	tion.	error.	Decimation.	Rer
May 10 19	-42 52 Hobart Diemen		R. R.	$-10^{\circ}24.5$ $-10^{\circ}24.3$	Mean, 7 day Mean, 7 day	s'hourly obs s'hourly obs	servations servations	with Decl	$\left\{\begin{array}{l} \text{lin. No. 1.} \\ \text{lin. No. 2.} \end{array}\right\}$	-10 24	At the
July 7 P.M. 9 P.M. 10 A.M. 10 P.M. 11 P.M.	-42 04 -40 55 -40 26 -37 49	148 07 149 24 149 12 149 34	R. R	-10 36 -11 24 -12 11 -12 44 -13 04 -13 22 -14 01 -14 42 -15 08 -15 06 -14 51 -14 29 -13 51 -13 08 -12 25 -10 29 - 9 26 - 7 38 - 7 03 - 6 19 - 5 36 - 7 03 - 6 19 - 5 36 - 7 03 - 6 04 - 7 01 - 7 30 - 8 40 - 7 01 - 7 30 - 8 40 - 9 57 - 10 56 - 10 55	N. N. by W. N.N.W. N. W. by N. W. W. N.W. W. S.W. S.W. S.W. S.W. S. S.S.W. S. by W. S.W. S. S.S.E. by S. S.E. by S. S.E. by S. S.E. by S. S.E. by S. E. E. by N. E. N.E. N.E. N.E. N.E. N.E. N.E. N.	To obtain corrections for the ship's attraction.	+3 49 +0 39 0 00 0 00 0 00 +0 35 +0 35	-10 17 - 8 41 - 9 36 - 8 52 - 10 47 - 9 57 - 10 21 - 10 04 - 10 34 - 11 18 - 10 42 - 9 43	$ \begin{cases} -0.37 \\ -0.37 \end{cases} $	— 9 51	At the Magnetic Observatory.

1841.	Posit	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
July 12 A.M.	_37 ź4	151 ź7	R. R.	- 6 30 " - 6 11	N.E. N.E.) ° ′	$\begin{array}{c c} -2 & 10 \\ -2 & 10 \end{array}$	- 8 40 - 8 21	<u> </u>	0 /	
12 г.м.	$ \begin{array}{rrrr} -37 & 22 \\ -37 & 17 \\ -37 & 16 \end{array} $	151 39	R. W. S. S. Y. R. S. S.	- 5 39 - 7 53 - 6 06 - 6 37 - 9 36 - 8 34 - 9 33 - 9 45	N.E. N.N.E. N.E. \frac{3}{4} E. N.E. N. by w. N. by w. N. by w. N. by w.	>-66 00	$\begin{vmatrix} +0 & 34 \\ +0 & 34 \\ +0 & 34 \\ +0 & 34 \end{vmatrix}$	- 7 49 - 9 00 - 8 40 - 8 47 - 9 02 - 8 00 - 8 59 - 9 11	}−0 37	- 9 31	re,
13 A.M.	-37 11 -36 26 Garden	151 42	R. T. T.	$ \begin{array}{c cccc} & -9 & 29 \\ & -9 & 09 \\ & -12 & 04 \end{array} $	n. by w. n. n.n.w.	-65 00	$\begin{vmatrix} +0 & 34 \\ 0 & 00 \\ +1 & 03 \end{vmatrix}$	$ \begin{array}{c cccc} -8 & 55 \\ -9 & 09 \\ -11 & 01 \end{array} $			By the magnetometers on shore,
Aug. 3 {	Syd	ney. 151 17	R.	$\begin{bmatrix} -9 & 51.5 \\ -7 & 05 \end{bmatrix}$	Е.] _62 40	_3 13		3 1 0 35	-951.5 -1007	e magneton
	_33 30		T. S. S. O. R.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	E. by N. E. by N. E. by N. E. by N.	$\begin{vmatrix} -6z & 40 \\ -61 & 30 \end{vmatrix}$	$\begin{bmatrix} -3 & 00 \\ -2 & 50 \\ -3 & 03 \end{bmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-10 07 -12 02	Bythe
9 а.м	_33 38	163 50	R. T. R. T.	$ \begin{vmatrix} -6 & 30 \\ -10 & 37 \\ -9 & 45 \\ -9 & 23 \end{vmatrix} $	E. E. E.		$ \begin{vmatrix} -3 & 03 \\ -2 & 56 \\ -2 & 56 \\ -2 & 56 \end{vmatrix} $	$ \begin{array}{r rrrr} -9 & 33 \\ -13 & 13 \\ -12 & 41 \\ -12 & 19 \end{array} $	8	-12 02	
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	166 19	R. T. S. T. W. SM.	-12 53 -10 59 - 9 55 - 9 28 -11 20 - 8 55 - 8 35	N.N.E. s.E. by E. E. by s. E.s.E. E. by N.	-60 10	$\begin{bmatrix} -2 & 59 \\ -2 & 52 \\ -2 & 39 \end{bmatrix}$	-13 41 -13 49 -12 47 -12 27 -14 19 -11 47 -11 14	$\left\langle \begin{array}{c} 1 \\ 1 \\ 1 \end{array} \right\rangle = 0 37$	7—13 34	
11 А.М	. —33 32		Т. W. О. Sм. Т.	$ \begin{array}{c cccc} -10 & 50 \\ -11 & 56 \\ -10 & 46 \\ -10 & 32 \\ -10 & 51 \\ -7 & 46 \\ -10 & 32 \end{array} $	E. by N. N.E. by N. E.S.E. E. \frac{1}{2} N. E.S.E. E. by S. E.	-59 40	$ \begin{array}{r rrrr} & -2 & 56 \\ & -2 & 49 \end{array} $	-13 29 -13 06 -13 48 -13 14 -13 47 -10 48 -13 21		7-13 27	
11 р.м	. —33 31		S. R. R. O. S.	$ \begin{array}{c cccc} - & 9 & 03 \\ - & 11 & 11 \\ - & 11 & 04 \\ - & 11 & 13 \\ - & 10 & 48 \\ - & 9 & 45 \\ \end{array} $	E. by s. E.N.E. E. by N. E. by N.	-59 30	$\begin{bmatrix} -z & 4z \\ -2 & 42 \end{bmatrix}$	$ \begin{array}{c cccc} -11 & 59 \\ -13 & 27 \\ -13 & 20 \\ -14 & 01 \\ -13 & 30 \\ -12 & 27 \\ \end{array} $		-8-	
15 A.M	-33 32 -33 55	167 59 171 58	T. O. S.	$ \begin{array}{c cccc} -10 & 29 \\ -8 & 13 \\ -8 & 02 \\ -8 & 33 \\ -8 & 15 \end{array} $	E. by N. E. by S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	-58 10	$ \begin{vmatrix} -2 & 42 \\ -2 & 47 \\ -2 & 44 \\ -2 & 44 \\ -2 & 47 \end{vmatrix} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 6 7	7 12 54	
16 A.M	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	171 58 172 51		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by s. E. by s. $\frac{1}{2}$ s. N.N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W. N.W. by N. N.W. $\frac{1}{2}$ N.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-11 09 -11 09 -13 18 -11 31 -13 49 -13 49		7-13 56	

1841.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
Aug. 17 A.M. 17 P.M.	-34 37	173 12 173 55	T. S. O. R. O. R. R.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	E. by s. E.S.E. E.S.E. E.S.E. E. by s. ½ s. E. by s. ½ s. E. by s.	>-5°8 1′0	-2 48 -2 48 -2 48 -2 48 -2 48 -2 48 -2 48 -2 48	-14 02 -12 59 -14 08 -13 06 -13 27 -12 13 -14 15		—1°3 5′6	
Aug. & Sept. Nov. 24 A.M. 24 P.M.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	174 00 177 20 177 21 177 47 177 56 177 58	R. SM. O. S. S. O. R. R. T.	-13 36 - 8 57 - 8 51 -10 45 -11 52 - 9 47 -10 38 -10 19	E.S.E. E.S.E. by E. S.E. by E.	-59 40		-11 42 -11 36 -13 21 -14 22 -14 28 -12 23 -13 14 -12 55	\rightarrow -1 20	$-13 \ 36$ $-14 \ 24$	By the magnetometers on shore.
3	-37 59 -38 01 -38 03 -38 22	179 40 179 41 180 10	T. R. R. T. SM. T. SM. O. S. T. R. Y.	-11 20 -10 13 -10 27 -11 54 -11 11 -11 07 -10 29 -11 42 -10 06 -11 15 -10 43 -10 19	s.e. by e. s.e. by e. s.e. by s. s.e. by s. s.e. ½ s. s.e. s.e. ½ s. s.e. s.e. ½ s.	\right\}-60 14	-2 36 -2 36 -1 56 -1 56 -2 09 -1 56 -2 09 -2 22 -2 29 -2 49 -2 32	-13 56 -12 49 -13 03 -13 50 -13 16 -12 25 -13 51 -12 28 -13 24 -13 32 -12 51	-1 20	14 44	
	-39 08	182 29 182 32 182 36 182 40	R. R. T. R. O. T. R. R. R. T. R. SM.	-11 09 -11 26 -10 06 -11 39 -11 29 -10 10 -11 05 -10 37 - 9 39 -10 36 - 9 49 - 9 49 -11 47 -11 09	s.e. ½ e. s.e. by e. s.e. by e. s.e. by e. s.e. by e. s.e. ½ e. s.e. ½ e. s.e. by e. s.e. by e. s.e. by e. s.e. by e. e.s.e. s.e. by e. s.e. by e. s.e. by e. s.e. by e.		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-13 41 -14 06 -12 50 -14 17 -14 13 -13 49 -13 20 -13 32 -13 32 -13 42 -13 45 -13 45 -13 57	$\left \begin{array}{c} \\ \\ \\ \end{array}\right $ -1 20	14 43	
	-40 23 -40 27 -40 22 -40 57 -41 07 -41 09 -41 10	183 03 183 14	S. T. O. S. T. R. O. R. S. R. R. R.		N. N.N.E. $\frac{1}{4}$ E. N.N.E. $\frac{1}{2}$ E. S. by E. S. S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. S.E. by S. S.E. S.E. S.E. S.E. S.E. S.E. S.E.		$\begin{array}{c cccc} -0 & 53 \\ -0 & 58 \\ -0 & 45 \\ -0 & 45 \\ -1 & 46 \\ -1 & 27 \\ -2 & 04 \end{array}$	-12 33 -13 23 -13 39 -12 47 -12 05 -10 56 -10 59 -11 10 -12 05 -12 41 -11 59 -11 15 -10 59	\rightarrow -1 20	12 57	

1841.	Position.	als.	Declination	Direction of	Tuelineties	Correction for ship's	Corrected Declina-	Correction for index	True	Remarks.
1041.	Lat. Lo	eg. Initials.	observed.	ship's head.	Inclination.	attraction.	tion.	error.	Declination.	Rem
Nov. 29 A.M.	_41 28 183	41 Y. T. T.	$ \begin{vmatrix} -\mathring{1}5 & \mathring{2}0 \\ -14 & 41 \\ -11 & 59 \end{vmatrix} $	w.s.w. s.w. ½ s. s. by E.	, ,	$\begin{vmatrix} +3 & 09 \\ +2 & 23 \\ -0 & 47 \end{vmatrix}$	$ \begin{array}{c cccc} -12 & 11 \\ -12 & 18 \\ -12 & 46 \end{array} $		0 /	
·	-41 30 183	Т.	$ \begin{array}{c cccc} -12 & 55 \\ -13 & 02 \\ -10 & 38 \end{array} $	s. by E. s. by E. s. by E.	-63 20	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} -13 & 42 \\ -13 & 49 \\ -11 & 25 \end{vmatrix}$	-1 20	-14 24	
30 A.M.	$\begin{bmatrix} -41 & 31 \\ -43 & 28 \end{bmatrix} 183$	40 O. 04 R. T.	$ \begin{array}{rrrrr} -12 & 15 \\ -13 & 14 \\ -13 & 23 \\ -14 & 02 \end{array} $	s. by E. s. by E. s. \frac{1}{4} E. s.	-65,00		$ \begin{array}{rrrr} -13 & 02 \\ -14 & 01 \\ -13 & 39 \\ -14 & 02 \end{array} $			
Dec. 1 A.M.	$\begin{bmatrix} -43 & 30 & 183 \\ -45 & 30 & 183 \end{bmatrix}$		$ \begin{array}{c cccc} -12 & 49 \\ -12 & 16 \\ -11 & 47 \\ -13 & 08 \end{array} $	s. s.e. by e. ½ e. s.e. by e. s.e. by e.		$ \begin{vmatrix} 0 & 0 \\ -3 & 24 \\ -3 & 18 \\ -3 & 18 \end{vmatrix} $	$ \begin{array}{r rrrr} -12 & 49 \\ -15 & 40 \\ -15 & 05 \\ -16 & 26 \end{array} $)		
2 A.M.	$\begin{vmatrix} -45 & 32 & 183 \\ -46 & 40 & 184 \end{vmatrix}$	11 T. W. 15 S. 18 T.	$ \begin{array}{c cccc} -11 & 02 \\ -10 & 22 \\ -12 & 26 \\ -12 & 30 \end{array} $	s.e. by e. $\frac{1}{2}$ e. s.e. by e. s.e. by e. s.e. by e.		$ \begin{array}{r rrrr} -3 & 24 \\ -3 & 18 \\ -3 & 18 \\ -3 & 44 \end{array} $	$ \begin{array}{r rrrr} -14 & 26 \\ -13 & 40 \\ -15 & 44 \\ -16 & 14 \end{array} $	-1 20	- 16 35	-
		W. Y. Sm. T. T.	$ \begin{array}{c cccc} -11 & 54 \\ -10 & 33 \\ -11 & 24 \\ -12 & 31 \\ -11 & 33 \end{array} $	s.e. by e. s.e. by e. s.e. by e. s.e. by e. e.s.e.	$\left \begin{array}{c} -67 & 55 \end{array} \right $	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{bmatrix} -15 & 30 \\ -14 & 09 \\ -15 & 00 \\ -16 & 15 \\ -15 & 25 \end{bmatrix} $		•	
2 P.M.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13 Sm. 42 S. 50 T. T.	$ \begin{array}{c cccc} -11 & 07 \\ -11 & 28 \\ -11 & 00 \\ -11 & 29 \end{array} $	s.e. by e. e. by s. s.e. $\frac{1}{2}$ e. s.e. by e. $\frac{1}{2}$ e.		$ \begin{array}{ c c c c c c } -3 & 36 \\ -3 & 57 \\ -3 & 24 \\ -3 & 44 \end{array} $	$ \begin{array}{r rrrr} -14 & 43 \\ -15 & 25 \\ -14 & 24 \\ -15 & 13 \end{array} $		7)	
,	-47 32 184 	53 T. W. S. T. O.	$ \begin{array}{c cccc} -10 & 36 \\ -11 & 28 \\ -11 & 32 \\ -10 & 43 \\ -11 & 07 \end{array} $	s.e. by e. s.e. $\frac{1}{2}$ e. s.e. by e. s.e. by e. s.e. $\frac{1}{2}$ e.	-67 55	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r rrrr} -14 & 12 \\ -14 & 52 \\ -15 & 08 \\ -14 & 19 \\ -14 & 31 \end{array} $	\\ \rightarrow -1 20	-15 45	Simple Control of the
3 р.м	$ \begin{array}{c ccccc} -47 & 34 & 184 \\ -47 & 38 & 185 \\ -48 & 50 & 186 \end{array} $	55 R. R. R.	$ \begin{array}{c cccc} -11 & 07 \\ -10 & 27 \\ -9 & 25 \\ -9 & 47 \\ -12 & 19 \end{array} $	S.E. $\frac{2}{4}$ E. S.E. by E. S.E. by E. $\frac{1}{2}$ E N.E. by E. $\frac{1}{2}$ E		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-13 57 -13 01 -13 31 -15 30			
	-48 53 186	S. T.	$ \begin{array}{c cccc} -11 & 26 \\ -11 & 35 \\ -10 & 25 \end{array} $	E.S.E. E. ½ N. S.E. by E. S.E. by E.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 30 15 27 14 12 14 48			
	-48 50 186	Т.	$ \begin{array}{c cccc} -11 & 32 \\ -10 & 48 \\ -10 & 49 \end{array} $	s.e. by e. $\frac{1}{2}$ e s.e. by e. s.e. by e. $\frac{1}{2}$ e s.e. by e.		-347	_15 19 _14 43 _14 36	-1 20	-16 23	
	-48 51 186 -48 54 186	S. R. T.	$ \begin{array}{c cccc} -11 & 20 \\ -10 & 23 \\ -10 & 49 \end{array} $	s.e. by e. s.e. by e. E.s.e. E.s.e.		$ \begin{array}{r rrrr} -3 & 47 \\ -3 & 47 \\ -4 & 04 \\ -4 & 04 \end{array} $	-14 46 -15 07 -14 27 -14 53			
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 53 R. 7 32 R. 8 59 T.	$ \begin{array}{c cccc} & -12 & 35 \\ & -12 & 52 \\ & -11 & 28 \end{array} $	s.e. by e. s.e. ½ e. e. by s. e. by s.		$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{r rrrr} -15 & 29 \\ -16 & 08 \\ -17 & 10 \\ -15 & 46 \end{array} $			manufacture descriptions of the second description descriptions of the second description descriptions of the second description des
5 p.m	_49 31 18	W	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by s. E. by s. E. by s.	-69 40	$\begin{vmatrix} -4 & 18 \\ -4 & 18 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-1 20	—17 51	energie automobile de la constante de la const
	-49 32 18	9 28 R.		E. by s.	J	$\begin{vmatrix} -4 & 18 \\ -4 & 07 \end{vmatrix}$	$\begin{bmatrix} -16 & 53 \\ -15 & 35 \end{bmatrix}$			

1841.	Posi	tion.	ials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected Declina-	Correction for index	True	arks.
1041.	Lat.	Long.	Initials.	observed.	ship's head.	memation.	attraction.	tion.	error.	Declination.	Remarks
Dec. 6 л.м.	-4957	19°1 0'6	R. R. T.	$-1\overset{\circ}{1}$ 47 $-1\overset{\circ}{2}$ 34 $-1\overset{\circ}{2}$ 58	E. by s. E. by s. E. by s.	, ,	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} -16 & 05 \\ -16 & 52 \\ -17 & 16 \end{array} $		0 /	
6 р.м.	-50 04 -50 03	191 15 191 38	O. S. T. T. S.	$\begin{array}{c cccc} -13 & 50 \\ -13 & 13 \\ -14 & 25 \\ -14 & 02 \\ -15 & 52 \\ -12 & 37 \end{array}$	E. by s. E. by s. N.E. $\frac{3}{4}$ E. E. by N. N.E. by N. E.S.E.	$-69 \ 37$	$ \begin{array}{r rrrr} -4 & 18 \\ -4 & 18 \\ -2 & 52 \\ -3 & 53 \\ -1 & 54 \\ -4 & 12 \end{array} $	-18 08 -17 31 -17 17 -17 55 -17 46 -16 49		-18 23	
7 а.м.	$ \begin{array}{rrrr} -50 & 06 \\ -50 & 36 \\ -50 & 51 \end{array} $	191 40 191 44 191 56 192 00 192 20 192 40 192 45	Т. R. S. Sм. S. R. T.	$ \begin{array}{c cccc} -13 & 40 \\ -11 & 21 \\ -11 & 44 \\ -15 & 43 \\ -13 & 39 \\ -13 & 51 \\ -13 & 58 \\ -12 & 42 \end{array} $	E. by S. ½ S. E.S.E. S.E. ½ E. S. by E. ¾ E. E.S.E. S.E. ½ S. E.S.E. S.E. ½ S. S.E. ½ S.	$\left.\right \right\} -69 \ 49$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			-18 18	
8 A.M.	$-51 \ 30$	192 44 193 57 194 00	R. T. T. W. W. T.	-12 42 -12 24 -11 39 -11 54 -11 28 -11 27 -12 48 -13 15	s.e. 2 e. s.e. by s. e. by s.	-70 11	$ \begin{array}{r rrrr} -3 & 26 \\ -4 & 25 \\ -4 & 25 \\ -4 & 25 \end{array} $	-16 22 -15 50 -16 04 -16 19 -15 53 -15 52 -17 13 -17 40			
8 р.м.	51 41	194 03 195 04 195 26	O. T. O. S. T. R. T.	$ \begin{array}{r rrr} -12 & 32 \\ -8 & 21 \\ -8 & 34 \\ -9 & 39 \\ -9 & 54 \\ -8 & 29 \\ -8 & 27 \end{array} $	E. by s. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	-70 11	-4 25 -4 20 -4 20 -4 20 -4 20 -4 20 -4 20	-16 57 -12 41 -12 54 -13 59 -14 14 -12 49 -12 47	-1 20	-15 16	
9 л.м.		195 37 195 46	W. R. R. T. R. T.	- 9 09 - 8 48 - 8 07 - 8 24 - 8 06 - 9 29	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. by S. E. by S. E. by S.		-4 20 -4 20 -4 25 -4 25 -4 25	$ \begin{array}{rrrrr} -13 & 29 \\ -13 & 08 \\ -12 & 32 \\ -12 & 49 \\ -12 & 31 \\ -13 & 59 \end{array} $			
11 P.M.	_52 50	204 00	R. O. T. S. O. T. R.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by s. E. by s. E. $\frac{1}{2}$ N. E. $\frac{3}{4}$ N. E. $\frac{1}{4}$ S. E.		$ \begin{array}{rrrr} -4 & 15 \\ -4 & 12 \\ -4 & 25 \\ -4 & 22 \\ -4 & 27 \end{array} $		-1 20	-13 58	
12 А.М.	-53 10	203 15 205 15 205 18	T. W. SM. Y. O. S. T.	- 7 35 - 7 58 - 6 47 - 7 35 - 7 37 - 7 55 - 7 21	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E. E.S.E.		$ \begin{array}{rrrrr} -4 & 27 \\ -4 & 27 \\ -4 & 20 \\ -4 & 20 \\ -4 & 20 \\ -4 & 20 \\ -4 & 20 \end{array} $	-12 02 -12 25 -11 07 -11 55 -11 57 -12 15 -11 41	J		
12 P.M.		206 10	O. R. T. R. T. W.	- 7 23 - 7 23 - 7 22 - 7 15 - 8 08 - 7 14 - 7 19	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E. S.E. by E. ½ E.	-70 11	-4 20 -4 20 -4 20 -4 20 -4 20 -4 20 -4 10	-11 43 -11 43 -11 42 -11 35 -12 28 -11 34 -11 29	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-13 06	

1841.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's	Declina-	for index	True Declination.	Remarks.
	Lat.	Long.	H				attraction.	tion.	error.		Rej
Dec. 13 A.M.	$-\mathring{5}4 \ \mathring{4}5$	20°9 0′2	S.	- °7 35	E.S.E.) ° ′	$-\mathring{4} \ 2\mathring{7}$	$-12^{\circ}02$		0 /	
	-54 46	209 07	T. R.	$\begin{bmatrix} -7 & 51 \\ -7 & 18 \end{bmatrix}$	s.e. by E. $\frac{1}{2}$ E. s.e. by E. $\frac{1}{2}$ E.		$\begin{vmatrix} -4 & 17 \\ -4 & 17 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			
	-54 48	209 10	T. W.	$\begin{bmatrix} -7 & 06 \\ -7 & 40 \end{bmatrix}$	s.e. by E. $\frac{1}{2}$ E. s.e. by E.	7-70 47	-4 07	-11 23 $-11 47$	1 20	-14 26	
13 р.м.			R. S.	$\begin{vmatrix} -10 & 24 \\ -11 & 36 \end{vmatrix}$	s.e. by e. $\frac{1}{2}$ e. s.e. by e.		$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{vmatrix} -14 & 41 \\ -15 & 43 \end{vmatrix}$			
14 A.M.	-56 06	210 20 211 33	S. T.	$-11 20 \\ -12 31$	s.e. by e.	K	$\begin{vmatrix} -4 & 07 \\ -3 & 03 \end{vmatrix}$	-15 27 $-15 34$			
	$\begin{bmatrix} -56 & 04 \\ -56 & 10 \end{bmatrix}$	211 44	T.	$-12 14 \\ -11 45$	s.e. by s.		$\begin{vmatrix} -3 & 03 \\ -3 & 03 \end{vmatrix}$	$\begin{bmatrix} -15 & 17 \\ -14 & 48 \end{bmatrix}$			
		211 49	SM. R.	$ \begin{array}{r rrrr} -12 & 52 \\ -11 & 57 \end{array} $	s.e. by s.	-72 00		$\begin{bmatrix} -15 & 55 \\ -15 & 00 \end{bmatrix}$	>-1 20	-15 43	
14 P.M.	-56 22	211 56	T. S.	$\begin{bmatrix} -8 & 36 \\ -9 & 02 \end{bmatrix}$	E. 1/4 N. E.N.E.		$\begin{vmatrix} -4 & 35 \\ -4 & 02 \end{vmatrix}$	-13 11 $-13 04$			
			T. T.	-944 -1001	E.N.E.	IJ	$\begin{vmatrix} -4 & 02 \\ -2 & 54 \end{vmatrix}$	$\begin{bmatrix} -13 & 46 \\ -12 & 55 \end{bmatrix}$	j		
			S. S.	$\begin{bmatrix} -9 & 03 \\ -8 & 11 \end{bmatrix}$	N.E. $\frac{1}{2}$ E. E. $\frac{1}{2}$ N.		$ \begin{array}{r rrrr} -3 & 13 \\ -4 & 35 \end{array} $	$\begin{bmatrix} -12 & 16 \\ -12 & 46 \end{bmatrix}$			
	FC 00	211 58	R. W.	$\begin{bmatrix} -851 \\ -851 \end{bmatrix}$	E.N.E. E. by N.	* • • • • • • • • • • • • • • • • • • •	$\begin{vmatrix} -4 & 02 \\ -4 & 27 \end{vmatrix}$	$\begin{bmatrix} -12 & 53 \\ -13 & 18 \end{bmatrix}$			
	-50 23	211 59	R. T.	$\begin{bmatrix} -8 & 37 \\ -9 & 10 \end{bmatrix}$	s.e. by s.		-3 03	$\begin{vmatrix} -11 & 40 \\ -12 & 13 \end{vmatrix}$		-13 50	
	¥0.04		W. T.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s.		$\begin{vmatrix} -3 & 03 \\ -3 & 03 \end{vmatrix}$	-12 05 $-12 34$			
15 A.M.	-56 24 $-56 50$	211 59 212 12	W. T.	$ \begin{array}{r rrrr} -9 & 44 \\ -11 & 01 \end{array} $	s.e. by s. s. by E. $\frac{1}{2}$ E.	H	$\begin{vmatrix} -3 & 03 \\ -1 & 40 \end{vmatrix}$	$\begin{vmatrix} -12 & 47 \\ -12 & 41 \end{vmatrix}$	ń		
			Sм. Y.	$ \begin{array}{r rrrr} -11 & 34 \\ -10 & 29 \end{array} $	s. by E.		$\begin{vmatrix} -1 & 08 \\ -2 & 13 \end{vmatrix}$	$\begin{vmatrix} -12 & 42 \\ -12 & 42 \end{vmatrix}$			
		212 41	S.	$ \begin{array}{r rrrr} -10 & 25 \\ -9 & 31 \end{array} $	S.S.E.	$-72 \ 39$	-2 13	$\begin{bmatrix} -12 & 38 \\ -11 & 44 \end{bmatrix}$	>-1 zu	-13 32	
		212 41	R.	$\begin{bmatrix} -9 & 21 \\ -8 & 24 \\ \hline -8 & 26 \end{bmatrix}$	s.e. by s.		$\begin{bmatrix} -3 & 09 \\ -3 & 09 \end{bmatrix}$	$\begin{vmatrix} -12 & 36 \\ -11 & 33 \end{vmatrix}$			
15 г.м.	$-57 01 \\ -57 13$	212 42 212 45	R. T.	$\begin{vmatrix} -7 & 56 \\ -9 & 41 \end{vmatrix}$	s.e. by s.	K	$\begin{vmatrix} -3 & 09 \\ -2 & 10 \end{vmatrix}$	-11 05 $-11 51$	lή	*	
			S. W.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	S.S.E.		$\begin{vmatrix} -2 & 10 \\ -2 & 10 \end{vmatrix}$	-11 53 $-11 46$			
	-57 14	212 45	R. T.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	S.S.E.	-	$\begin{vmatrix} -2 & 10 \\ -2 & 10 \end{vmatrix}$	$\begin{vmatrix} -11 & 55 \\ -11 & 38 \end{vmatrix}$	3 1		
		212 45	R. Y.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E. S.S.E.	-72 12		$\begin{bmatrix} -12 & 01 \\ -14 & 01 \end{bmatrix}$	}-1 20	-13 54	
	-57 16	212 45	T. T.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E. E.N.E.		$\begin{vmatrix} -2 & 10 \\ -4 & 05 \end{vmatrix}$	$\begin{bmatrix} -12 & 22 \\ -13 & 16 \end{bmatrix}$			
			S. S.	$\begin{bmatrix} -8 & 07 \\ -9 & 29 \end{bmatrix}$	E.S.E.		$\begin{vmatrix} -4 & 05 \\ -4 & 47 \end{vmatrix}$	-12 12 -14 16			
10		212 47	S. R.	-853 -1112	S.E. S.S.E.	l l	$\begin{vmatrix} -3 & 51 \\ -2 & 10 \end{vmatrix}$				
16 A.M.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	213 09 213 08	S. T	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	S.S.E.						
	50 15	213 08	S. T.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	S.S.E.						
	-90 19	213 00	Y. T.	$\begin{array}{c cccc} -10 & 08 \\ -10 & 47 \\ -11 & 56 \end{array}$	S.S.E.	$\left \begin{array}{c} -73 & 55 \end{array} \right $	-2 21	-13 12	-1 20	-14 37	
	-58 21	213 17	R. W.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E.						
	59 05	213 06	R. R.	$ \begin{array}{c cccc} -11 & 17 \\ -12 & 08 \\ -11 & 28 \end{array} $	S.S.E.						
- 17 А.М.		213 45	S.	-11 28 $-11 32$	S.S.E. S.S.E.	$-75 \ 40$	-2 40	-14 12			

1043	Posi	ition.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected Declina-	Correction for index	True	Remarks.
1841.	Lat.	Long.	Init	observed.	ship's head.	inclination.	attraction.	tion.	error.	Declination.	Rem
Dec. 18 A.M.	$-6^{\circ}2 \ 40$	212 49	T. R.	$-1\overset{\circ}{7}$ 18 -19 25	S. $\frac{1}{2}$ E. S. by W.	, ,	$\begin{vmatrix} -0.44 \\ +1.28 \\ +0.22 \end{vmatrix}$	_ 18 62 _ 17 57) ,° ′	· /	
19 n.v.	$-62 ext{ } 45$ $-62 ext{ } 50$	212 44	W. R. Sм. R.	$-19 ext{ } 14$ $-20 ext{ } 47$ $-19 ext{ } 54$	s. $\frac{1}{4}$ w. s. by w. s. $\frac{1}{2}$ w.		$\begin{vmatrix} +0 & 22 \\ +1 & 28 \\ +0 & 44 \end{vmatrix}$	-18 52 $-19 19$ $-19 10$			
10 P.M.	-62 50 $-62 53$ $-62 56$	211 34	R. R. T.	$ \begin{array}{r} -26 & 11 \\ -25 & 40 \\ -23 & 59 \\ -23 & 47 \end{array} $	S.W. $\frac{1}{2}$ W. S.W. $\frac{1}{2}$ W. S.W. $\frac{1}{2}$ W. S.W. $\frac{1}{2}$ W.	├ -76 49	+5 30 $+5 30$ $+5 30$ $+5 30$		}-1 20	-20 14	
10 a m	-62 57 $-63 19$		W. R. R. S.	$ \begin{array}{rrrr} -25 & 11 \\ -21 & 25 \\ -21 & 49 \\ -23 & 12 \end{array} $	s.w. ³ / ₄ w. s.s.w. s.s.w.		$ \begin{array}{r} +5 & 41 \\ +2 & 57 \\ +2 & 57 \\ +5 & 27 \end{array} $	$ \begin{array}{rrr} -19 & 30 \\ -18 & 28 \\ -18 & 52 \\ -17 & 45 \end{array} $			
13 A.M.	$-63 \ 20$		O. W. T.	$ \begin{array}{c cccc} -23 & 26 \\ -23 & 32 \\ -23 & 34 \end{array} $	S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W. S.W. by S.	-77 40	$ \begin{array}{c cccc} +3 & 45 \\ +3 & 45 \\ +4 & 25 \end{array} $	$ \begin{array}{c cccc} -19 & 41 \\ -19 & 47 \\ -19 & 09 \end{array} $	-1 20	-20 39	
(m)	$ \begin{array}{cccc} -63 & 19 \\ -63 & 23 \end{array} $		R. R. R.	$ \begin{array}{c cccc} -22 & 11 \\ -22 & 07 \\ -19 & 19 \\ -20 & 43 \end{array} $	s.s.w. s. by w.		+3 11 +1 33	$ \begin{array}{ccc} -19 & 00 \\ -20 & 34 \\ -19 & 19 \\ -20 & 43 \end{array} $	$\begin{bmatrix} -0 & 06 \\ -0 & 28 \end{bmatrix}$, ,	H 162 H 167
			R. R. R.	$ \begin{array}{c cccc} -22 & 35 \\ -18 & 24 \\ -18 & 44 \end{array} $	Observed on ice.	$\left77\ 36 \right $	•••••	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} +1 & 00 \\ -0 & 06 \\ -0 & 28 \end{array}$	-19 59	
19 р.м.	-63 23	210 05	S. T. T. T.	$ \begin{array}{c cccc} -13 & 00 \\ -13 & 39 \\ -26 & 28 \\ -21 & 32 \end{array} $	E.N.E. E. by N. W.S.W. s. by W. ³ / ₄ W.		$-6 \ 40$	$ \begin{array}{ccc} -19 & 07 \\ -20 & 19 \\ -19 & 42 \\ -18 & 48 \end{array} $			
			S. T. S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. s. w. ¹ / ₄ w. s. 42° w. s. w.	>-77 36	$\begin{array}{c c} +3 & 27 \\ +5 & 10 \end{array}$	-20 04 $-18 48$ $-19 12$	1 20	20.44	
			S. T. T.	$ \begin{array}{c cccc} -21 & 44 \\ -24 & 23 \end{array} $	s.w. by w. $\frac{1}{2}$ w. s. 22° w. s. 42° w.	>-17 30	$ \begin{array}{c c} +6 & 22 \\ +3 & 07 \\ +5 & 10 \end{array} $	$ \begin{array}{c cccc} -20 & 24 \\ -18 & 37 \\ -19 & 13 \\ 10 & 25 \end{array} $	>-1 20	-20 44	
	-63 24	209 39	T. S. T. T.	$ \begin{array}{c cccc} -23 & 43 \\ -23 & 21 \\ -25 & 01 \\ -27 & 10 \end{array} $	s. 33° w. s.w. by s. s. 54° w. w.s.w.		+421	$ \begin{array}{rrr} -19 & 25 \\ -19 & 00 \\ -18 & 41 \\ -20 & 23 \end{array} $			
	$-63 \ 36$ $-63 \ 52$	208 45	S. O. T.	$ \begin{array}{c cccc} -23 & 40 \\ -23 & 49 \\ -23 & 16 \end{array} $	s.w. by s. s.s.w. s. by w. ½ w.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{bmatrix} -19 & 01 \\ -20 & 32 \\ -20 & 47 \end{bmatrix} $			
21 A.M.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	206 55	T. S. T. W.	$ \begin{array}{c cccc} -19 & 00 \\ -18 & 26 \\ -18 & 31 \end{array} $	S. $\frac{1}{2}$ E. S.S.E. S. by E. S. by E. $\frac{1}{2}$ E.	-78 30	$ \begin{array}{c c} -0 & 50 \\ -3 & 17 \end{array} $	$ \begin{array}{rrr} -19 & 50 \\ -21 & 43 \\ -20 & 11 \\ -20 & 37 \end{array} $	├ —1 20	-22 00	
	$-64 ext{ } 49 \\ -64 ext{ } 50$		T. S. R.	$ \begin{array}{c cccc} -20 & 30 \\ -21 & 18 \\ -25 & 18 \\ -20 & 29 \end{array} $	s.		$\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ +4 & 39 \end{bmatrix}$	$ \begin{array}{r} -20 & 30 \\ -21 & 18 \\ -20 & 39 \\ -22 & 09 \end{array} $			
	-64 54	206 06	W. T. R. R.	$ \begin{array}{c cccc} -19 & 35 \\ -21 & 56 \\ -19 & 25 \end{array} $	s. by E. s. ½ E. s. ¾ W. s. ¾ E.		$ \begin{array}{c cccc} -0 & 51 \\ +1 & 16 \\ -1 & 16 \end{array} $	$ \begin{bmatrix} -20 & 26 \\ -20 & 40 \\ -20 & 41 \end{bmatrix}^{2} $			
	-64 56	206 04	R. R. R.	$ \begin{array}{c cccc} -18 & 54 \\ -22 & 38 \\ -20 & 24 \\ -17 & 56 \end{array} $	s. by E. s. 11° E. s. 9° E. s. 8° E.	-78 50	$ \begin{array}{c cccc} -1 & 40 \\ -1 & 36 \\ -1 & 18 \end{array} $	$ \begin{array}{rrrr} -20 & 34 \\ -24 & 14 \\ -21 & 42 \\ -19 & 05 \end{array} $	-1 20	-22 51	
			R. R.	-23 07	s. 11° E.]	$-1 \ 36$	$\begin{bmatrix} -19 & 05 \\ -24 & 43 \end{bmatrix}$			

1841.	Posi	Long.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
Dec. 22 л.м.	_65 13	206 07 205 55 205 47	S. O. T. S. Y. O. T.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	s. 3/4 w. s. by w. 1/2 w. s. by w.	-79 20	$\begin{vmatrix} +1 & 47 \\ +1 & 47 \\ +1 & 47 \end{vmatrix}$	$\begin{array}{c cccc} -20 & 42 \\ -21 & 46 \\ -20 & 27 \\ -20 & 52 \\ -20 & 15 \\ -18 & 57 \\ -20 & 26 \end{array}$	-1 20		
22 P.M	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	206 06 205 50 205 47 205 44 205 46	T. W. W. R. R. S. T. Y. R.	$\begin{array}{c} -22 \ 58 \\ -23 \ 00 \\ -19 \ 56 \\ -22 \ 43 \\ -23 \ 11 \\ -18 \ 11 \\ -21 \ 14 \\ -22 \ 02 \\ -21 \ 18 \end{array}$	s. by w. \frac{1}{4} w s.s.w. s. \frac{1}{2} w. s. \frac{1}{2} w. s.s.e. s. \frac{1}{2} w. s.s.e. s. \frac{1}{2} w. s.	79 20	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-20 44 -19 32 -19 56 -21 50 -22 18 -21 39 -20 48 -22 08 -23 24	-1 20	-22 46	
	-66 01 $-66 16$		T. T. T.	-27 28 -26 45 -14 34 -14 42 -16 17 -30 17 -29 00 -30 56	S.S.W. N.W. by N. S.E. by E. \frac{1}{2} E E.S.E. E. by N. \frac{1}{2} N S.W. by S. S.S.W. \frac{1}{2} W.	$\left. \right\} - 79 \ 45$	$ \begin{vmatrix} +3 & 35 \\ +4 & 20 \\ -7 & 50 \\ -8 & 10 \\ -8 & 02 \\ +5 & 17 \\ +4 & 28 \\ +6 & 39 \end{vmatrix} $	23 5322 2522 2422 5924 1925 0024 3924 17	$\begin{bmatrix} 3 \\ 5 \\ 4 \\ 2 \end{bmatrix} $ $\begin{bmatrix} -1 & 20 \\ 20 \\ 20 \end{bmatrix}$	_24 13	
29 P.M 30 P.M 1842.		203 51 203 06		-30 50 -31 36 -31 41 -30 30 -17 13 -31 25 -30 38	S.W. W.N.W. W.N.W. 1/2 W. E. by N. 1/2 W. S.W. by W. 1/2 W. S.W.		+7 43 +6 18 +8 02 +8 02 +6 39	24 1123 5323 5824 1925 1123 2323 59	$\begin{vmatrix} -1 & 20 \\ 8 & 2 \\ 5 & 3 \end{vmatrix}$	0 -25 36	
Jan. 6 P.M	66 0s	5 203 13	SM. R. SM. R. R. T.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. \frac{1}{4} w. s. \frac{1}{2} w. s. by w. \frac{1}{4} w. s. by w. \frac{1}{2} w. s. by w. \frac{1}{2} w. n. by e. n. by w. \frac{1}{4} w. n. w. \frac{1}{4} n.	$\left -79 \right $	$\begin{vmatrix} -1 & 53 \\ +1 & 54 \\ +2 & 16 \\ +6 & 26 \end{vmatrix}$	-25 50 -25 59 -25 1 -25 39 -24 59 -25 29	$ \begin{vmatrix} 2 & 2 & 3 & 3 \\ 2 & 4 & 4 & 3 \\ 2 & 2 & 3 & 3 \\ 3 & 3 & 4$	0 -26 59	
7 P.M 8 P.M 9 A.M	66 18	204 48 204 50 204 49 204 26	R. R. R. SM O.	_16 49	N.W. ½ W. N.W. ½ W. s.w. by W. E. by s. s.w. by W. s.s.W. ½ W E. s.E. by E. ½ 1			-26 3 -25 0 -24 3 -25 3 -23 5 -23 5 -25 2 -24 4	$\begin{bmatrix} 7 \\ 3 \\ 5 \\ 6 \\ 3 \\ 4 \end{bmatrix} -1 \ 2$	0 -26 36	
		5 204 26 204 23 6 204 24	T. O. S. T. Y. W.	$\begin{array}{c} -16 & 50 \\ -31 & 46 \\ -30 & 14 \\ -17 & 09 \\ -15 & 31 \\ -15 & 38 \\ -14 & 22 \\ -16 & 12 \\ \end{array}$	E. by s. $\frac{1}{2}$ s. s. w. s. w. $\frac{1}{2}$ s. E. $\frac{1}{2}$ s. E. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s.		$ \begin{array}{c cccc} -8 & 24 \\ +6 & 33 \\ +5 & 54 \\ -8 & 26 \\ -8 & 24 \\ -8 & 24 \end{array} $	$ \begin{array}{c cccc} -25 & 1 \\ -24 & 2 \\ -25 & 3 \\ -23 & 5 \\ -24 & 0 \\ -22 & 4 \end{array} $	$ \begin{vmatrix} 3 & & \\ 5 & & \\ 5 & & \\ 4 & & \\ 6 & & \\ \end{vmatrix} $	0 —25 55	

1842.		tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina-	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.	<u> </u>				attraction.	cion.	CHOI.		Rei
T 0	_66 65	204 60	T.	$-\mathring{3}0\mathring{3}5$	1 .	2 0 /	$+\overset{\circ}{5}\overset{\prime}{54}$	-24 42	/	0 /	
Jan. 9 P.M.	-00 05	204 22	R.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.W. $\frac{1}{2}$ S. W.S.W.		$+5 54 \\ +8 15$	$-24 42 \\ -23 57$)		
			T.	$-31 \ 41$	S.W. $\frac{1}{2}$ W.		+704	$-23 \ 37$ $-24 \ 37$			
			T.	$-33 \ 36$	w. by s. $\frac{1}{4}$ s.		+8 28	-25 08			
			T.	-31 17	s.w. $\frac{1}{4}$ w.		+6 48	-24 29			
			S.	-30 16	s.w.	{	+6 33	$-23 \ 43$			
	-66 03	204 25		-15 20	s.E. by E. $\frac{1}{2}$ E.	.]]	-755	-23 15			-
			T.	-1604	E. by s. $\frac{1}{2}$ s.	├ _79 52	0 01	-24 28			
	-6604	204 17		-17 33	S.E. 1/4 S.	79 32	-0 14	-23 47	-1 20	$-25\ 48$	
		204 14		-32 25	s.w.byw. $\frac{3}{4}$ w.		+8 05	-24 20			
			T.	$-32\ 10$	s.w. by w.		+7 35	-24 35			
	00 00	204 27	R.	-1655	s.e. by E. $\frac{3}{4}$ E.	·	-805	-25 00			
	-66 06	204 11		-1702	s.e. by E.		-735	-24 37			
			R. Sm.	-33 07	s.w. by $w \cdot \frac{1}{2} w$.		+7 55	-25 12			
			R.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w.s.w. E. by N.		$ +8 \ 15 $ $ -8 \ 15 $	-2455 -2452			
10 4.84	-66 00	204 08		$-10^{\circ} 37$ $-17^{\circ} 38$	S.E.	K	-6 28	-24 06	K		
10 11.51	00 00	~0.	ő.	-17 28	S.E. 1/4 E.		-6 44	-24 12			
			S.	-17 30	S.E. 4 E.		-6 44	-24 14			
	-65 58	204 11		-15 30	E. by s.		$-8 \ 31$	-24 01			
			Y.	-15 21	E. by s.		$-8 \ 31$	-23 52			
			W.	-17 02	s.E. by E. 1/2 E.	-79 48		-24 52		-25 26	
			T.	-1603	s.e. by E. $\frac{1}{2}$ E.		-750	-23 53			
			T.	-31 55	w. by s. $\frac{1}{2}$ s.		+8 18	$-23 \ 37$			
			W.	-32 25	w.s.w.		+8 09	-24 16			
			Y.	-3149	w.s.w.		+8 09	-23 40			
		204 18		-31 50	s.w. by w.	Ŋ	+7 31	-24 19			
10 P.M.	-65 58	204 14		-16 36	s.E. by E.		-731	-24 07			
			T. T.	-15 49	s.E.by E. \frac{3}{4} E.	11	-800	-23 49			
	65 50	204 16		$\begin{vmatrix} -32 & 23 \\ -27 & 46 \end{vmatrix}$	w. by s.	11	$+8 \ 31 \\ +3 \ 37$	-23 52			
	-00 00	204 10	o.	-32 16	s.w. by w.		+731	-24 09 $-24 45$			
	-65 57		R.	-16 26	E. by s. $\frac{1}{4}$ s.		-8 25	-24 51	4		
	00 01		T.	$-16 \ 15$	E. by s.	\\ \-79 48		-24 46	1 20	-25 24	
			T.	-31 12	s.w. by w.	13 10	+7 31	$-23 \ 41$	1 70	-20 24	
			w.	-32 18	s.w.		+628	-25 50			1
	4		R.	-30.27	s.w. ½ s.		+6 10	-24 17			
•		204 13	R.	$-29 \ 31$	s.w. \frac{3}{4} s.		+5 30	-24 01			
			R.	-30 14	$S.W. \frac{1}{2} S.$		+5 50	-24 24			
	-6558	204 10	R.	-32 13	\mathbf{w} by \mathbf{s} $\frac{3}{4}$ \mathbf{s}	را.	+8 18	-23 55	J		l
11 A.M.	-6601	203 51	SM.	-21 04	s. by E.		-152	-22 56			
	-65 56	203 44		-1951	s.E. by s.		-5 12	-25 03			
			T.	-26 27	s. by w. 1 w.	11	+2 16	_24 43		E-Particular Particular Particula	
			Y. T.	-27 21	N.N.W. $\frac{1}{2}$ W.		+3 40	-23 41		Para de la companya d	
12 A.M.	-65 52	203 45		$\begin{vmatrix} -31 & 34 \\ -31 & 42 \end{vmatrix}$	N.w.byw. $\frac{1}{2}$ w. s.w. by w.	1 [+7 07 +7 31	-24 27 $-24 11$	1.		
AN AM	00 02	700 TO	R.	$-31 \ 42 \ -31 \ 52$	s.w. by w.		17 21	-24 11 $-24 21$	- 2		
	1970		w.	-31 58	w. by s. $\frac{3}{4}$ s.	├ -79 48	+8 18	$-23 \ 40$			
12 P.M.	-65 56	203 24		-26 53	S.S.W.		$+3 \ 37$	-23 16		-24 58	
			T.	-27 00	s.s.w.	11	+3 37	-23 23	1 ~0	- 2 UQ	
			Т.	-2349	s.	1	0 0	-23 49			
			S.	-2248	s.		0 0	-22 48			
	1	203 29	T.	$-22\ 36$	S. $\frac{3}{4}$ E.		_1 24	-24 00			
		203 26		-20 23	s. by E.	J	-152	-22 15			
14 A.M.	$-66\ 10$	202 50		-24 36	s. by w.]	+152	-22 44			
			SM.	-22 06	S. \(\frac{3}{4}\) E.	-7943	-1 24	-23 30			
	1	1	T.	-15 17	E. by N. 3 N.	. 1	-740	-22 57		1	1

1842.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
Jan. 16 р.м.	_65 47	202 13	R. R. R. R.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Observed on ice.	· · · · · · ·	·	$ \begin{array}{c cccc} -22 & 19 \\ -26 & 36 \\ -24 & 45 \\ -24 & 00 \\ -23 & 16 \end{array} $	$\begin{array}{c c} -0 & 05 \\ -0 & 28 \\ -1 & 20 \\ -1 & 20 \end{array}$	-25 15 c c	R H 162 H 167 CCL
	$\begin{bmatrix} -67 & 39 \\ -67 & 40 \\ -67 & 34 \end{bmatrix}$	204 28 204 27	R. T. T. R. T. R. R. R.	-22 58 -29 56 -19 02 -36 04 -17 30 -17 42 -16 49 -35 09 -27 58	$\begin{array}{c} J \\ \text{N. by W.} \frac{1}{2} \text{ W.} \\ \text{S.S.E.} \frac{1}{3} \text{ E.} \\ \text{W. by N.} \frac{1}{4} \text{ N.} \\ \text{E.N.E.} \\ \text{E.} \frac{1}{2} \text{ S.} \\ \text{E.} \frac{1}{2} \text{ S.} \\ \text{S.W.} \frac{1}{4} \text{ W.} \\ \text{S.} \frac{1}{2} \text{ W.} \end{array}$	\right\{ -80 34	$ \begin{array}{r} +2 & 25 \\ -4 & 44 \\ +8 & 44 \\ -8 & 13 \\ -9 & 12 \\ -9 & 12 \\ +7 & 20 \\ +1 & 00 \end{array} $	-22 58 -27 31 -23 46 -27 20 -25 43 -26 54 -26 01 -27 49 -26 58	-1 20		CCH
31 A.M. Feb. 1 P.M.	-67 20 -67 21	202 20 202 02	T. T. R. T. R. T. W.	-16 57 -28 40 -28 20 -25 59 -26 30 -22 51 -24 19 -20 23	E. $\frac{3}{4}$ N. S. by W. $\frac{1}{2}$ W. S. $\frac{1}{2}$ E. S. by E. $\frac{3}{4}$ E. S. by E. $\frac{1}{2}$ E.	\right\}-80 44	-8 57 +3 00 +1 01 -1 01 0 0 -3 28 -3 00 -4 45 -5 42	-25 54 -25 40 -27 19 -27 00 -26 30 -26 19 -27 19 -25 08 -24 50	-1 20	-27 36	
		201 55	T. R. O. T. W. R. R. R.	-19 08 -34 20 -37 09 -34 45 -28 10 -29 43 -29 29 -25 12 -36 14	s.e. by s. N.w. by w. w. $\frac{3}{4}$ N. N.w. by w. s. by w. s. by w. N.N.w. $\frac{1}{4}$ W. N. $\frac{1}{2}$ E. s.w. $\frac{1}{2}$ s.	-80 44	$ \begin{array}{r} -3 & 42 \\ +7 & 27 \\ +9 & 09 \\ +7 & 27 \\ +2 & 02 \\ +2 & 02 \\ +3 & 26 \\ -0 & 50 \\ +6 & 26 \end{array} $	-26 53 -26 00 -26 18 -26 08 -27 41 -26 03 -26 02 -29 48	-1 20	-28 12	
2 A.M.	-68 18 -68 17 -68 04 -68 03 -68 37	200 00 202 24 202 32 199 45	T. R. T. W. T. S. R. R. W. T. S. O.	-31 31 -39 16 -39 48 -21 19 -21 36 -21 34 -22 08 -23 06 -39 53 -38 58 -40 19 -40 25	S.S.W. N.W.by W. $\frac{3}{4}$ W. W.S.W. S. by E. $\frac{1}{4}$ E. S.S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{3}$ S. S.E. by S. S.E. $\frac{3}{4}$ S. W. $\frac{1}{2}$ S.	-81 00	+4 04 +7 55 +9 19 -2 34 -4 57 -6 36 -5 51 -6 13 +9 42 +9 42 +9 42 +9 42 +9 42	-27 27 -31 21 -30 29 -23 53 -26 33 -28 10 -27 59 -29 19 -30 11 -29 16 -30 37 -30 43 -29 52	-1 20	30 25	
4 A.M.	-68 49 -68 50 -68 51 -68 46 -68 45		R. SM. T. O. W. R. T. R. R. T. R. R.	-39 34 -40 56 -24 47 -29 49 -29 42 -37 01 -35 15 -35 57 -35 54 -34 23 -32 17 -33 05 -38 42 -38 31 -35 32	w. by s. $\frac{1}{2}$ s. s. by E. $\frac{1}{2}$ E. s. $\frac{1}{2}$ W. s. by E. N.N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N. N.W. $\frac{3}{4}$ W. N. by W. N. by W. N. by W. $\frac{1}{4}$ S. s. S.W. $\frac{1}{4}$ S. s. S.W. $\frac{1}{4}$ W.	\ -81 38	+9 30 -3 20 +1 08 -2 16 +4 35 +6 15 +6 15 +5 03 +2 16 +2 22 +7 31 +4 52	-31 26 -28 07 -28 41 -31 58 -32 26 -29 00 -29 42 -29 39 -29 20 -30 01 -30 43 -31 35 -31 00 -30 40	-1 20	-32 33	-

1040	Position.	Declination observed.		Inclination.		Corrected Declina-	Correction for index	True	Remarks.
1842.	Lat. Long.	observed.	ship's head.	2370333441011	attraction.	tion.	error.	Declination.	Ren
Feb. 8. A.M.	_70 07 186 36 _70 08 186 28	T. -26 51 O. -30 31 S. -33 41 W. -30 23 T. -29 56	s.s.e. s.s.e. $\frac{1}{2}$ e. s. by e. $\frac{1}{4}$ e. s. by e. $\frac{1}{4}$ e. s. by e. $\frac{1}{2}$ e.	\ -83 39	- 4 12	_33 29 _33 42 _34 02 _33 41 _33 54 _34 08	$\left \right\rangle_{-1}$ 20	-35 42	
9 л.м.	-70 34 185 33 -70 30 185 23	7 R32 55 T33 18 B T52 48 W50 28 5 R50 00	s. $\frac{1}{4}$ E. s. by E. s. by E. w. $\frac{1}{2}$ N. w. by N. w. $\frac{1}{2}$ N.		$ +14 \ 15 \ +14 \ 29 $	_35 31			
	-70 38 185 26 -70 33 185 20 -70 31 185 18	0 R51 21 T51 05 W52 05 T50 17	W. $\frac{1}{2}$ S. W. $\frac{1}{4}$ S. W. $\frac{1}{4}$ S. W. $\frac{1}{4}$ N. W. $\frac{1}{4}$ N. W. $\frac{1}{4}$ S.	-84 00	$+14 \ 41 \ +14 \ 36$	36 20 36 24 37 29 35 41 37 17 38 00	-1 20	-38 21	
10 а.м.	-70 26 185 08 -70 25 185 00 -70 22 184 17	R52 35 R53 52 T51 49 R51 12 O S54 00	W. $\frac{3}{4}$ N. W. $\frac{1}{4}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ S.	$\left.\begin{array}{c} \\ \\ \\ \\ \end{array}\right\}$ -83 52	+14 22 +14 18 +14 11 +14 11 +14 25 +14 22	_38 13 _39 34	$\begin{cases} -1 & 20 \end{cases}$	—37 35	,
*	-70 20 184 10 -70 16 183 54	T49 48 SM49 51 T47 56 O46 47 S47 11 T47 05	$\frac{1}{2}$ N. $\frac{1}{4}$ S. $\frac{3}{4}$ S. $\frac{3}{4}$ S. $\frac{3}{4}$ S. S.w.byw. $\frac{1}{2}$ w. W.S.W. S.w.byw. $\frac{1}{2}$ w.		+14 11 +14 20 +13 50 +12 59 +13 34 +12 57	_35 37 _35 31 _34 06 _33 48 _33 37 _34 08			
10 р.м.	-70 11 183 59 -70 13 183 51 -70 12 183 50	l R. 26 53	w. by s. ½ s. s.e. by s. s.e. w. by s. w. by s. w. ½ s. w. ½ s. w. ½ s.	-83 50	_10 37	_35 34 _37 30 _35 59 _34 39 _34 11	>-1 20	-36 28	. (- 4
16 а.м.	-70 14 183 54 -72 10 180 58 -75 08 173 20 -75 03 173 03	W47 54 T49 53 S30 58 T55 14 R56 11 T56 01	W. $\frac{1}{2}$ N. W. $\frac{1}{4}$ N. S.E. $\frac{5}{4}$ S. S.E. $\frac{1}{2}$ S. S.E. $\frac{1}{2}$ S.		$\begin{array}{r} +14 & 05 \\ +14 & 12 \\ -13 & 19 \\ -19 & 18 \\ -20 & 33 \\ -20 & 33 \end{array}$	_33 49 _35 41 _44 17 _74 32 _76 44 _76 34)	-45 37 $-77 17$	
	-76 48 182 33 -76 47 182 33 -76 21 194 43	R84 09 S88 09 T84 23 W90 46 R80 25	N. N. $\frac{1}{2}$ E. N. N. by W. $\frac{1}{2}$ W. N. $\frac{1}{2}$ E. S. E. $\frac{3}{4}$ S.	$\left.\right \right\} - 86 50$	$\begin{bmatrix} -2 & 39 \\ 0 & 0 \end{bmatrix}$	_85 00 _86 48 _88 09 _84 23 _82 53 _83 04 _76 23	_1 20	-86 23	
	-76 29 -76 32 194 35 -76 58 194 35	O. -72 18 S. -70 54 T. -71 09 T. -68 08 W. -72 15 F. -59 41	s.s.e. $\frac{1}{2}$ e. s.s,e. s. by e. $\frac{1}{2}$ e. s.s.e. $\frac{1}{4}$ e. s. by e. e. by s.	-85 26	$ \begin{array}{c cccc} & 9 & 49 \\ & 8 & 03 \\ & 6 & 05 \\ & 9 & 00 \\ & 4 & 05 \\ & & 20 & 00 \end{array} $	-82 07 -78 57 -77 14 -77 08 -76 20 -79 41	-1 20	—79 57	-
	-76 57 194 28		E. by s. E. by s.		$ \begin{array}{c cccc} -20 & 00 \\ -20 & 00 \\ -20 & 00 \end{array} $	-79 00 $-79 18$ $-79 57$			

1040	Posit	ion.	als.	Declination	Direction of	T1:4:			Correction	True	arks.
1842.	Lat.	Long.	Initials.	observed.	ship's head.	Inclination.	for ship's attraction.	Declina- tion.	for index error.	Declina tion.	Remarks
Feb. 23 A.M.	$-\r{7}7 {45}$	198 16	T. O.	$-96\ 30$ $-96\ 31$	s.s.w. s.s.w. ½ w.) ° ′	+ 7 08 + 8 43	-8748		• /	
	-77 42	198 00	S. T. O. T. S. W.	$ \begin{array}{rrrr} -96 & 05 \\ -93 & 06 \\ -93 & 39 \\ -94 & 06 \\ -94 & 02 \\ -98 & 12 \end{array} $	s.s.w. s.w. by s. s.s.w. ½ w. s.w. by s. s.w. by s.	85 00	$\begin{vmatrix} + 7 & 08 \\ + 7 & 08 \\ + 10 & 19 \\ + 8 & 43 \\ + 10 & 19 \\ + 10 & 19 \end{vmatrix}$	-85 58 -83 20 -85 23 -83 43	-1 20	-88 0 8	
23 г.м.	$-77 ext{ } 50 $ $-77 ext{ } 48 $ $-77 ext{ } 56 $ $-78 ext{ } 00$	197 03 197 40	T. W. R. T. R.	-99 25 -98 09 -69 54 -69 07 -70 06	s.w. by s. s.w. $\frac{1}{2}$ s. E. $\frac{1}{2}$ s. E. $\frac{3}{4}$ s. E. by s.		$\begin{vmatrix} +10 & 19 \\ +11 & 41 \\ -17 & 41 \\ -17 & 39 \\ -17 & 37 \end{vmatrix}$	-89 06 -86 28 -87 35 -86 46			
	-78 02 -78 07	197 24	T. S. R. T. S.	$ \begin{array}{rrrr} -68 & 51 \\ -70 & 14 \\ -67 & 13 \\ -66 & 56 \\ -68 & 23 \end{array} $	E. $\frac{1}{4}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	85 00	-17 39	-86 30 -88 00 -84 54 -84 37	_1 20	-87 31	
25 A. M.	-78 10 $-75 13$ $-74 40$	193 50	R. T. T. O. R.	$ \begin{array}{r} -67 & 53 \\ -66 & 26 \\ -82 & 32 \\ -80 & 13 \\ -73 & 01 \end{array} $	E. \frac{1}{2} S. E. by S. W. W. N.W.byW.\frac{1}{2}W.	-85 00	$ \begin{array}{r rrrr} -17 & 41 \\ -17 & 37 \\ +17 & 46 \\ +17 & 46 \\ +15 & 11 \end{array} $	$ \begin{array}{rrrrr} -85 & 34 \\ -84 & 03 \\ -64 & 46 \\ -62 & 27 \\ -57 & 50 \end{array} $. fa 17	
27 p.m.	$ \begin{array}{rrr} -74 & 37 \\ -74 & 25 \\ \hline -71 & 59 \end{array} $	194 04 194 04 193 55 186 42	R. T. R. T.	$ \begin{array}{rrrrr} -73 & 34 \\ -76 & 47 \\ -76 & 45 \\ -57 & 42 \end{array} $	w.n.w. w.n.w. n.w. by w. s.w.byw. 4w.		$\begin{vmatrix} +16 & 05 \\ +16 & 05 \\ +14 & 17 \\ +14 & 00 \end{vmatrix}$	$ \begin{array}{rrrr} -57 & 29 \\ -60 & 42 \\ -62 & 28 \\ -43 & 42 \end{array} $	1 00	-62 17 -45 11	
28 A.M.	$ \begin{bmatrix} -71 & 54 \\ -71 & 11 \\ -71 & 09 \end{bmatrix} $	185 03 184 58	R. T. S. T. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. by w. s.w.byw.½w. w.s.w. s.w.byw.½w. w.½ s.	.	$\begin{vmatrix} +13 & 40 \\ +13 & 51 \\ +14 & 30 \end{vmatrix}$	$ \begin{array}{r rrr} -38 & 15 \\ -36 & 15 \\ -39 & 34 \end{array} $	$\left \right\rangle_{-1}$ 20	-39 20	
Mar. 1 A.M.		180 32	R. O. T. S. T.	$ \begin{array}{rrrrr} -53 & 16 \\ -46 & 44 \\ -45 & 32 \\ -44 & 09 \\ -46 & 02 \end{array} $	w. w. n. w. w. by n. ½ n. w. n. w. w. n. w.	$\left \begin{array}{c} \\ \\ \\ \end{array} \right > -83 \ 46$	$\begin{vmatrix} +15 & 23 \\ +13 & 52 \\ +14 & 22 \end{vmatrix}$	$ \begin{array}{c cccc} -37 & 53 \\ -32 & 52 \\ -31 & 10 \\ -30 & 17 \end{array} $			
1 р.м.	-69 36		W. R. S. T.	$\begin{array}{r rrrr} -45 & 45 \\ -24 & 21 \\ -24 & 00 \\ -24 & 01 \end{array}$	w.n.w. n. by e. n. by e. n. by e. ½ e.	1 1	$ \begin{vmatrix} +13 & 52 \\ - & 2 & 47 \\ - & 2 & 47 \\ - & 4 & 10 \end{vmatrix} $	$ \begin{array}{c cccc} -31 & 53 \\ -27 & 08 \\ -26 & 47 \\ -28 & 11 \end{array} $	-1 20	30 50	
2 A.M.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	180 10182 38	O. S. T. R. W.	$\begin{array}{c cccc} -24 & 05 \\ -22 & 09 \\ -21 & 28 \\ -21 & 20 \\ -22 & 58 \\ \end{array}$	N. by E. $\frac{1}{2}$ E. N.N.E. $\frac{1}{2}$ E. N.N.E. $\frac{1}{2}$ E. N.N.E. $\frac{1}{2}$ E. N.N.E.	$\left \begin{array}{c} -83 & 48 \\ \hline \end{array} \right $	$ \begin{array}{c cccc} - & 6 & 45 \\ - & 6 & 45 \\ - & 6 & 45 \\ - & 4 & 31 \end{array} $	28 54 -28 13 -28 05 -27 29			
2 p.m.	$ \begin{array}{c cccc} -68 & 44 \\ -68 & 40 \\ -67 & 53 \\ -67 & 52 \\ -67 & 49 \end{array} $	182 53 183 44	T. W. T. R. S. T.	$\begin{array}{r rrrr} -22 & 15 \\ -22 & 09 \\ -23 & 34 \\ -22 & 49 \\ -20 & 18 \\ -17 & 56 \end{array}$	N.N.E. N.N.E. N. by E. $\frac{1}{2}$ E. N. by E. $\frac{3}{4}$ E. N.E. by N.	-82 23	- 4 31 - 4 31 - 3 24 - 3 57 - 6 34 - 8 27	$ \begin{array}{r} -26 & 40 \\ -26 & 58 \\ -26 & 46 \\ -26 & 52 \end{array} $	7 00	_27 32	
	-67 47 -67 45	184 25	T. R. W. R.	-18 59 -19 10 -16 49 -18 58 -21 25	N.N.E. \frac{1}{2} E. N. by E. \frac{3}{4} E. N.E. N.E. by N. N.E. by N.		- 5 33 - 3 57 - 8 27 - 6 34 - 6 34	$ \begin{array}{r rrrr} -24 & 32 \\ -23 & 07 \\ -25 & 16 \\ -25 & 32 \\ \end{array} $			

1842.	Posi	tion.	als.	Declination	Direction of	To alimentino	Correction for ship's	Corrected Declina-	Correction for index	True	rks.
1042.	Lat.	Long.	Initials.	observed.	ship's head.	Inclination.	attraction.	tion.	error.	Declination.	Remarks.
March 3 А.м.		185 19 185 39	O. R.	$-\mathring{1}7 \overset{2}{2}\mathring{1}$	N.E. 1/2 E.	$\left.\right _{-82}^{\circ}$	- 8 41 8 41	-26 02		• /	- 3
5 А.М.	-67 20		T. W.	-18 06 $-16 16$	N.E. $\frac{1}{2}$ E. E. by N.	$\left.\right _{2}^{3}$ -81 10	$-10^{\circ} 23^{\circ}$	$\begin{bmatrix} -26 & 47 \\ -26 & 39 \end{bmatrix}$	20 1 – ح	$-27 \ 32$	
6 а.м.		191 35 191 45	уу. Sм. Т.	-14 45 $-19 52$	$\begin{array}{c c} E. \frac{1}{2} N. \\ N. by E. \\ \end{array}$	1	$\begin{bmatrix} -10 & 35 \\ -1 & 34 \\ 0 & 47 \end{bmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7		
6 р.м.	$-65 \ 00$	192 42	Т.	-21 59 $-21 38$	$ \begin{array}{cccc} \mathbf{N} \cdot \frac{1}{2} & \mathbf{E} \cdot \\ \mathbf{N} \cdot \frac{3}{4} & \mathbf{E} \cdot \\ \end{array} $	70.05	$\begin{vmatrix} - & 0 & 47 \\ - & 1 & 10 \end{vmatrix}$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1 20	20. 40	
		192 40	W. T. R.	$ \begin{array}{c cccc} -20 & 48 \\ -20 & 15 \\ 20 & 22 \end{array} $	N. by E.	$\begin{vmatrix} -79 & 25 \end{vmatrix}$	- 1 34	$ \begin{array}{rrr} -22 & 22 \\ -21 & 49 \\ -22 & 07 \end{array} $	\rightarrow 1 20	-23 40	
7 n w		192 44	Т.	$ \begin{array}{c cccc} -20 & 33 \\ -21 & 55 \\ 15 & 05 \end{array} $	N. by E. N. $\frac{3}{4}$ E.	78 17	-134 -110	-23 05	_	01 75	
7 р.м. 8 а.м.			R. W. T.	-15 05 $-17 12$	S.E. $\frac{1}{2}$ S. N. by E.	−78 17 	- 1 17	$ \begin{array}{c cccc} -20 & 37 \\ -18 & 29 \\ 20 & 17 \end{array} $	7 -1 20	-21 57	
8 р.м.	-62 11		T. T.	-19 19 $-11 28$	N. 3/4 E. S.E.	-77 23	-058 -544 -307	$ \begin{array}{rrr} -20 & 17 \\ -17 & 12 \\ -18 & 12 \end{array} $	-1 20	-19 51	
QAR	—61 15	196 29	R. T.	-15 05 $-15 53$ $-14 36$	N.N.E. ½ E. N.N.E. N.E. by N.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-18 12 $-18 25$ $-17 56$	-		
9 P.M.	_		Sм. W.	-13 54 $-12 25$	N.E. by N. N.E. $\frac{3}{4}$ E.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-17 14 $-17 25$			
, J I am	$-60 \ 51$		R. S.	$-12 23 \\ -12 19 \\ -12 12$	N.E. by E. N.E. by E.	}-76 0 9	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$-17 \ 30$ $-17 \ 23$	-1 20	-18 42	(
	-60 50	199 49	W. R.	-14 24 $-11 40$	N.E. by E.		-422 -512	$-18 \ 46$ $-16 \ 52$			
- 10 а.м.	$-60 \ 47$	200 20	R. S	-10 12 $-10 21$	E.N.E.	$\frac{1}{2}$	$-600 \\ -530$	-16 12 $-15 51$	}		
	-60 32		Ö. T.	-10 09 $-11 10$	E.N.E.	-74 15	-530 -530	$-15 39 \\ -16 40$	-1 20	-17 31	
	-60 18 $-60 17$	206 10	T. S.	-10 34 $-10 54$	e. by n. e. by n.	$\left\{ \right.$	-6.00 -534	-16 34 $-16 28$			
			O. T.	-958 -829	E. by N. E. by N. ½ N.	├ ─73 55	-534 -520	-15 30 $-13 49$	-1 20	-17 01	
14 р.м.	$-60 13 \\ -59 15$		S. T.	$-11 19 \\ -8 53$	e. by n.	$\left\{ \begin{array}{c} \cdot \\ \cdot \end{array} \right\}$	- 5 34 - 3 37	-16 53 $-12 30$	$\{ $,	
		219 14	T. T.	- 8 33 - 8 10	n.e. by e.	-73 56	$ \begin{array}{c cccc} - & 4 & 26 \\ - & 4 & 26 \end{array} $	-12 59 $-12 36$	1 00	15 20	
15 А.М.	-58 44	221 51	T. S.	-10 06 $-12 31$	E. by N. 1/4 N. E.N.E.	$\left.\right\}$ -73 30	-510 -450	-15 16 $-17 21$	1 20	-15 30	
16 г.м.	$-58 42 \\ -59 04$	221 59 229 00	T. R.	-923 -1108	E.N.E. E. ½ S.	$\{ $	- 4 50 - 5 26	-14 13 $-16 34$	{		
,	of c		S. O.	-11 15 $-10 47$	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	├-73 00		-16 41 -16 13	-1 20	→17 49	
18 а.м.	-60 14	236 32	T. S.	-11 03 $-13 59$	E. ½ S. E.	J	- 5 26 - 5 24	-16 29 $-19 23$	{	20. **	
00	$-60 \ 13$		O. T.	-15 28 $-13 10$	E. E.	$\left.\right\}$ -73 00	_ 5 24	$ \begin{array}{c cccc} -20 & 52 \\ -18 & 34 \end{array} $		-20 56	
	$-59 17 \\ -58 40$		R. T. W	$-14 40 \\ -15 41 \\ 15 40$	E.N.E. E. by N.	$-71 \ 33$	_ 4 29	$ \begin{array}{rrr} -18 & 54 \\ -20 & 10 \\ -20 & 17 \end{array} $)	-20 14 21 47	
02 4 34	-58 42	954 AG	W. S. T.	-15 48 -16 24 -17 28	E. by N. E. by N.	$\left.\right\}$ -70 51	- 4 29 - 4 29 - 4 26	$ \begin{bmatrix} -20 & 17 \\ -20 & 53 \\ -21 & 54 \end{bmatrix} $	$\begin{cases} -1 & z_0 \\ \\ \end{cases}$	-21 47	
£⊎ A.M.	-58 42 $-58 43$		W. T.	-17 28 $-17 40$ $-18 20$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	}−70 11	- 4 26 - 4 35	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-1 20	-23 28	
23 P.M. 24 A.M.		255 34	R. T.	-18 20 $-17 58$ $-18 40$	N.E. by E. ½ E. E.	$\left\{ \right.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} $	$\left\{ \right $		
,	00 10		O. S.	$-19 \ 41$ $-20 \ 42$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$-69 \ 46$		$ \begin{array}{r} 24 & 02 \\ -25 & 03 \end{array} $		-25 25	
			~-		2	_				*****************	

1842.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected Declina-	Correction for index	irue	Remarks.
1011	Lat.	Long.	liit	observed.	ship's head.		attraction.	tion.	error.	Declination.	Ren
Маг. 26 а.м.	_5°9 0′0	268 07 268 10	T. W. T.	$\begin{array}{c cccc} -20 & 21 \\ -21 & 51 \\ -22 & 06 \end{array}$	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N	. 3	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} -23 & 53 \\ -25 & 23 \\ -25 & 38 \end{array} $		0 /	
26 р.м.	-59 02	268 40	T. R.	$ \begin{array}{c cccc} -22 & 17 \\ -22 & 10 \end{array} $	E. by N. ½ N. E.N.E. E.N.E.	-67 38	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-1 20	-26 17	The second secon
		268 45	T. R. O.	$ \begin{array}{c cccc} -21 & 40 \\ -21 & 31 \\ -20 & 32 \end{array} $	E.N.E. E.N.E.		$ \begin{array}{r rrrr} -3 & 24 \\ -3 & 24 \\ -3 & 24 \end{array} $	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		PORTO PERSONAL PROPERTY PROPER	Note that the state of the stat
	$-59 02 \\ -58 50$		R. SM. S.	$\begin{array}{c cccc} -21 & 02 \\ -22 & 15 \\ -21 & 42 \end{array}$	E.N.E. E.N.E. N.E. by E. ¹ / ₂ E.		_2 50	$ \begin{array}{r rrr} -24 & 26 \\ -25 & 31 \\ -24 & 32 \end{array} $	-1 20	-26 51	
The state of the s	-58 52	276 15	O. W. T.	$\begin{array}{r rrrr} -21 & 37 \\ -24 & 04 \\ -22 & 51 \end{array}$	N.E. by E. $\frac{1}{2}$ E. N.E. by E. N.E. by E.	-65 30	_2 36	$ \begin{array}{r rrrr} -24 & 27 \\ -26 & 40 \\ -25 & 27 \end{array} $	-1 20	-26 18	
	$ \begin{array}{r rrr} -58 & 54 \\ -58 & 24 \\ -58 & 20 \\ \end{array} $	280 05	R. T. R.	$ \begin{array}{c cccc} -21 & 06 \\ -22 & 22 \\ -20 & 55 \end{array} $	N.E. by E. N.E. \frac{1}{2} E. N.E.		$ \begin{array}{ c c c c c c } -2 & 36 \\ -2 & 15 \\ -2 & 02 \end{array} $	$ \begin{array}{r} -23 & 42 \\ -24 & 37 \\ -22 & 57 \end{array} $	Ĭ,		
1	-58 19	280 31	T. W.	$ \begin{array}{c cccc} -22 & 12 \\ -21 & 09 \end{array} $	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	-64 50	$ \begin{array}{r rrrr} -2 & 15 \\ -2 & 15 \end{array} $	$ \begin{array}{r} -24 & 27 \\ -23 & 24 \end{array} $	-1 20	-25 04	and the second s
30 а.м.	-58 30	280 32 282 07	Т. Т. Sм.	$ \begin{array}{c cccc} -21 & 01 \\ -22 & 52 \\ -23 & 19 \end{array} $	N.E. $\frac{1}{2}$ E. E.N.E. N.E. by E. $\frac{1}{2}$ E.		$ \begin{array}{ c c c c c c } -2 & 15 \\ -2 & 47 \\ -2 & 35 \end{array} $	$ \begin{array}{r} -23 & 16 \\ -25 & 39 \\ -25 & 54 \end{array} $	Ĭ.		
			O. S. T.	$ \begin{array}{c cccc} -21 & 57 \\ -21 & 46 \\ -21 & 53 \end{array} $	E.N.E. E.N.E.	-63 40	$ \begin{array}{ c c c c c c } -2 & 47 \\ -2 & 47 \\ -2 & 47 \end{array} $	$ \begin{array}{c cccc} -24 & 44 \\ -24 & 33 \\ -24 & 40 \end{array} $	1 00	-26 14	
	-58 29	282 01	S. W. T.	$\begin{array}{c cccc} -22 & 24 \\ -20 & 46 \\ -22 & 21 \end{array}$	N.E. by E. E. by N. ½ N. E.N.E.		$ \begin{array}{c cccc} -2 & 23 \\ -2 & 58 \\ -2 & 47 \end{array} $				
	water and the second se	282 22	S. T. S.	$ \begin{array}{r rrrr} -22 & 09 \\ -23 & 34 \\ -21 & 39 \end{array} $	N.E. by E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.		$ \begin{array}{c cccc} -2 & 18 \\ -2 & 04 \\ -2 & 04 \end{array} $	$ \begin{array}{r rrr} -24 & 27 \\ -25 & 38 \\ -23 & 43 \end{array} $	Ñ	* 101	
31 л.м.	$ \begin{array}{r rrr} -58 & 28 \\ -58 & 40 \end{array} $		T. W. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ N.	-63 00	$ \begin{array}{r rrrr} -2 & 04 \\ -1 & 36 \end{array} $	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-1 20	-26 18	
April 5 A.M.		285 30 300 18	T. T.	$ \begin{array}{c cccc} -22 & 42 \\ -24 & 02 \\ -15 & 31 \end{array} $	N.E. by N. N.E. $\frac{1}{2}$ N. N.N.E.		$ \begin{array}{c cccc} -1 & 23 \\ -1 & 36 \\ -0 & 33 \end{array} $	$ \begin{array}{r rrr} -24 & 05 \\ -25 & 38 \\ -16 & 04 \\ \end{array} $	1		
5 P.M. 6 A.M.		300 50 301 43		$ \begin{array}{c cccc} -15 & 26 \\ -14 & 33 \\ -12 & 06 \end{array} $	N.N.E. N. by E. E. by s.	\right\}-53 54	$\begin{vmatrix} -0 & 16 \\ -2 & 16 \end{vmatrix}$	-15 59 $-14 49$ $-14 22$	-1 20	-16 29	
	-		T.	$\begin{vmatrix} -12 & 32 \\ -15 & 34 \end{vmatrix}$	E. by s. N.N.W. $\frac{1}{2}$ W.	$-52\ 30$	$\begin{vmatrix} -2 & 16 \\ +0 & 38 \end{vmatrix}$	$-14 48 \\ -14 56$			

Declinations observed on board Her Majesty's Ship Terror, between June 1841 and August 1842.

The Observers are distinguished in the column of Initials as follows:—C. Captain Crozier; P. Lieut. Phillips; Cr. Mr. Cotter, Master.

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1841.	Posit	ion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Decli	Remarks.
]									01.01.		- 12
July 7.	_43 30	147 20	C. C. C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. 53° e. s. 48° e. s. 48° e.	-71 00	- 4 01	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 07	。, —12 35	Card
9.	—42 23	149 31	C. C.	-10 05 $-14 45$ $-15 09$	s. 48° e. n. 22° w. n. 32° w.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c c} -14 & 06 \\ -13 & 21 \\ -13 & 06 \end{array} $			P.
	-42 08	149 30	CR. CR. CR.	$ \begin{array}{r rrr} -14 & 07 \\ -14 & 45 \\ -13 & 37 \end{array} $	N.N.W. N.N.W.	-69 50	+ 1 25	$ \begin{array}{c c} -12 & 42 \\ -13 & 20 \\ -12 & 12 \end{array} $	+1 07	—11 49	
10.	-40 56	149 20	C. C.	$ \begin{array}{rrrr} -11 & 57 \\ -13 & 03 \\ -14 & 35 \end{array} $	N. 12° W. N. 12° W. N. 15° W.	$-68 \ 40$	+ 0 39 + 0 39	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 07	—11 11	
11.	-40 33 -38 15		C. Cr. C.	$ \begin{array}{r rrrr} -12 & 15 \\ -12 & 55 \\ -12 & 58 \end{array} $	N. 12° W. N. ½ W. N.	}	+ 0 39 + 0 19	$ \begin{array}{c c} -11 & 36 \\ -12 & 36 \end{array} $ $ -12 & 58 $			
	-37 47		C. C.	$ \begin{array}{c cccc} -12 & 38 \\ -11 & 23 \\ -12 & 50 \\ -11 & 28 \end{array} $	N. 15° W. N. 8° W. N. 8° W.		+ 0 50 + 0 27	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			
		e	C. C.	$ \begin{array}{c cccc} -11 & 28 \\ -11 & 46 \\ -12 & 35 \\ -12 & 59 \end{array} $	N. 17° W. N. 15° W. N. 12° W.	$-66 \ 40$	+ 0 56 + 0 50	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 07	-10 38	
12.	-37 25	151 25	CR. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. 12 W. N. 30° E. N. 28° E.		$\begin{bmatrix} 0 & 00 \\ - & 1 & 31 \end{bmatrix}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	ý X		
			С. С. С.	$ \begin{array}{c cccc} -9 & 55 \\ -11 & 38 \\ -10 & 27 \\ -12 & 14 \end{array} $	N. 36° E. N. 38° E. N. 32° E.	-66 00	-147 -153	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-		
	× *	181 40	Cr.	$ \begin{array}{c cccc} -11 & 21 \\ -11 & 06 \end{array} $	n.e. by n.	-	-139 -210	$-13 00 \\ -13 16$	+1 07	-11 32	
13.	-37 13 $-36 17$	151 50	CR. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. 20° w. N. 20° w.	$\left. \begin{array}{c} 1 \\ -65 \\ \end{array} \right\}$	+ 100 + 100	-12 23	4,	: *	
Aug. 6.	—33 5 6	151 0	C. C.	$ \begin{array}{rrrrr} -10 & 06 \\ - 9 & 21 \\ - 9 & 03 \end{array} $	n. 82° e. n. 85° e. n. 83° e.	$-62 \ 40$	- 3 05	$egin{array}{c} -13 & 07 \\ -12 & 26 \\ -12 & 05 \end{array} angle$	+1 07	— 11 18	
8.	-33 25	160 45	C. C.	$ \begin{array}{c cccc} & 9 & 42 \\ & -13 & 21 \\ & -12 & 50 \end{array} $	n. 70° e. n. 75° e. n. 70° e.	$-61 \ 30$	-245 -235	$ \begin{bmatrix} -12 & 03 \\ -16 & 06 \\ -15 & 25 \end{bmatrix} $,	·	
9.	-33 39	163 40	C. C.	$ \begin{array}{c cccc} -12 & 41 \\ -12 & 00 \\ -12 & 41 \end{array} $	n. 76° е. е. е.		- 2 56	$ \begin{array}{c cccc} -15 & 28 \\ -14 & 56 \\ -15 & 37 \end{array} $	<u>ተ</u> ነ በ7	—14 26	
			C. C. C. C.	$ \begin{array}{c cccc} -12 & 31 \\ -12 & 35 \\ -12 & 39 \\ -12 & 35 \\ -13 & 14 \end{array} $	e. n. 79° e. e. n. 85° e. e.	$-60 \ 40$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} -15 & 27 \\ -15 & 18 \\ -15 & 35 \\ -15 & 25 \\ -16 & 10 \end{array} $	1-1 01		
10.	-33 44	166 30	C. C. C.	$ \begin{array}{c cccc} -11 & 05 \\ -13 & 11 \\ -12 & 22 \\ -13 & 07 \end{array} $	E.S.E S.E. by E. N. 82° E. E.		$\begin{array}{rrrr} - & 2 & 59 \\ - & 2 & 50 \\ - & 2 & 42 \\ - & 2 & 52 \end{array}$	$ \begin{array}{c cccc} -14 & 04 \\ -16 & 01 \\ -15 & 04 \\ -15 & 59 \end{array} $		97.y	
*		i) ·	C. C. C.	$ \begin{array}{c cccc} -11 & 59 \\ -12 & 23 \\ -13 & 25 \end{array} $	E. by s. ½ s. E.S.E. S.E. ½ E.	}-60 10	-259 -259	-14 58 -15 22	+1 30	-13 40	Card R.

1841.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at-	Corrected Declination.	Correc- tion for index	True Decli- nation.	Remarks.
	Lat.	Long.	Ini	observed.	smp s neau.	inemation.	traction.	Decimation.	error.	nation.	Reı
Aug. 10.	$-3\overset{\circ}{3}\overset{\prime}{44}$	166 30	C. C. C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	n. 70° e. n. 65° e. n. 61° e.	}-60 10	$ \begin{array}{c cccc} & 0.00 & 0.00 \\ & 0.00 & $		+ i 30	-1°3 4′0	
	-34 00	166 26	C. C. Cr. Cr. Cr.	$ \begin{array}{c cccc} -13 & 12 \\ -11 & 15 \\ -13 & 13 \\ -11 & 30 \\ -12 & 04 \\ -11 & 33 \end{array} $	s. 82° e. n. 67° e. e. by n. e. e.s.e.		$ \begin{array}{r rrrr} -2 & 57 \\ -1 & 59 \\ -2 & 39 \\ -2 & 52 \end{array} $				
11.	-33 32	167 35	Cr. C. C.	$ \begin{array}{r rrrr} -12 & 29 \\ -14 & 56 \\ -14 & 34 \\ -14 & 16 \end{array} $	s.e. by e. N. 77° E. E. N. 73° E.		$ \begin{array}{r rrrr} -2 & 50 \\ -2 & 36 \\ -2 & 49 \\ -2 & 27 \end{array} $	$ \begin{vmatrix} -15 & 19 \\ -17 & 32 \\ -17 & 23 \\ -16 & 43 \end{vmatrix} $			
			C. C. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	n. 78° e. e. s. 85° e. n. 72° e. n. 72° e.	-59 40	$ \begin{array}{r rrr} -2 & 36 \\ -2 & 49 \\ -2 & 43 \\ -2 & 25 \\ -2 & 25 \end{array} $	$\begin{bmatrix} -16 & 49 \\ -15 & 24 \end{bmatrix}$	+1 30	-15 02	
12.	-32 53	169 30	CR. C. C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	e. n. 56° e. n. 53° e.		$ \begin{array}{r rrrr} -2 & 49 \\ -1 & 56 \\ -1 & 50 \end{array} $	$ \begin{array}{c cccc} -16 & 20 \\ -15 & 53 \\ -17 & 29 \\ -16 & 43 \end{array} $			
15.	-33 56	171 50	Cr.	-15 09 $-13 22$	N.E. E. ½ S.	Ĭ		$\begin{bmatrix} -16 & 45 \\ -16 & 05 \\ -14 & 14 \end{bmatrix}$			
16.	-34 20	172 45	C. C.	$ \begin{array}{c cccc} -11 & 27 \\ -13 & 53 \end{array} $	E. by s. E.		-2 40	_16 33			
		÷	C. C. C. Cr.	$ \begin{array}{r} -14 & 08 \\ -16 & 20 \\ -14 & 30 \\ -12 & 16 \\ -15 & 30 \end{array} $	E. N. 26° W. N. 38° W. E.S.E. N.W. by N.	-58 10	$\begin{vmatrix} -2 & 47 \\ +1 & 04 \end{vmatrix}$	$ \begin{array}{c cccc} -15 & 34 \\ -13 & 15 \\ -15 & 03 \\ -14 & 26 \end{array} $	+1 30	-13 45	
17.	-34 3 6		CR. C. C. C. C.	$ \begin{array}{r rrrr} -12 & 34 \\ -12 & 11 \\ -12 & 24 \\ -13 & 20 \\ -11 & 38 \end{array} $	E. by s. $s. 83^{\circ}$ E. E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s.	-58 10	$ \begin{array}{r rrrr} -2 & 45 \\ -2 & 47 \\ -2 & 47 \\ -2 & 47 \end{array} $	$ \begin{vmatrix} -15 & 21 \\ -14 & 56 \\ -15 & 11 \\ -16 & 07 \\ -14 & 25 \end{vmatrix} $	+1 30	-13 42	
Nov. 24.	-34 17 $-36 17$	177 12	Cr.	$\begin{vmatrix} -12 & 35 \\ -13 & 51 \end{vmatrix}$	E. by s. E.S.E.	J -59 40	$\begin{vmatrix} -2 & 47 \\ -2 & 45 \end{vmatrix}$	$\begin{bmatrix} -15 & 22 \\ -16 & 36 \end{bmatrix}$			
25.	—38 06	179 40	C. C. C. Cr.	$ \begin{array}{r rrrr} -15 & 02 \\ -14 & 57 \\ -15 & 53 \\ -14 & 50 \end{array} $	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. S.E. by S.		$ \begin{array}{r rrrr} -2 & 30 \\ -2 & 30 \\ -2 & 22 \\ -1 & 56 \end{array} $	$ \begin{bmatrix} -17 & 27 \\ -18 & 15 \end{bmatrix} $. 1 00		
	-38 26	179 54 179 54 179 54	CR. CR. C. C.	$ \begin{array}{r rrrr} -14 & 26 \\ -12 & 07 \\ -13 & 23 \\ -11 & 33 \end{array} $	s.e. by e. s.e. by e. s.e. by e. s.e. by e.	}−60 15	$ \begin{array}{r rrrr} -2 & 39 \\ -2 & 39 \\ -2 & 39 \\ -2 & 39 \end{array} $	$ \begin{vmatrix} -17 & 05 \\ -14 & 46 \\ -16 & 02 \\ -14 & 12 \end{vmatrix} $	+1 20	— 14 5 0	
26.	-39 03	182 33	C. Cr. C. C.	$ \begin{array}{ c c c c c } -13 & 59 \\ -13 & 18 \\ -15 & 57 \end{array} $	s.e. by e. ½ e. e. by s. s.e. by e. ½ e. s.e. s.e. by e. ½ e.		$ \begin{array}{rrrr} -2 & 43 \\ -2 & 54 \\ -2 & 48 \\ -2 & 26 \\ -2 & 48 \end{array} $	$\begin{bmatrix} -16 & 53 \\ -16 & 06 \\ -18 & 23 \end{bmatrix}$	*		
28.	—40 38	183 05	CR. CR. CR. CR. C.	-14 19 -13 43 -12 32 -13 22 -18 06 -15 51 -16 32	s.e. by e. e.s.e. e.s.e. e.s.e. s. by e. s.e.	\right\{ -61 00 \\ \right\{ -62 00 \\ \right\{ -62 00 \\ \right\{ -63	-2 44 -2 53 -2 53 -2 53 -0 45 -2 31 -2 31	$\begin{vmatrix} -17 & 03 \\ -16 & 36 \\ -15 & 25 \\ -16 & 15 \\ -18 & 51 \\ -18 & 22 \end{vmatrix}$	+1 30	—16 55	

	Posit	tion.	Initials.	Declination		Inclination.	Correc- tion for	Corrected		True Decli-	arks.
1841.	Lat.	Long.	Init	observed.	ship's head.		ship's at- traction.	Declination.	index error.	nation.	Remarks.
Nov. 29.	-41 33	183 30	C. C. C. Cr. Cr. Cr. Cr. Cr. Cr. Cr. Cr.	-17 40 $-18 41$ $-18 32$ $-18 51$	s.s.e. s.e. by s. s. by e. s. by e. s. by w. s. by e. s.s.e. s. by e. s.s.e. s. by e. s.s.w. s.w. by w.	-63 20	- 2 08 - 0 47 - 0 47 0 0 + 0 47 - 1 30 - 0 47 + 1 30 + 2 58 + 2 38 + 3 09	$\begin{array}{c} -16 & 22 \\ -15 & 38 \\ -16 & 32 \\ -15 & 40 \\ -16 & 10 \\ -15 & 43 \\ -15 & 54 \\ -15 & 42 \\ \end{array}$	+1 30	-15 13	
30.		183 05	CR. CR. C. CR. CR.	$\begin{array}{rrrr} -14 & 42 \\ -16 & 41 \\ -17 & 56 \\ -15 & 53 \\ -17 & 17 \end{array}$	s.w. by s. s.e. by s. s. ½ E. s. ½ w. s.	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right\}$ -65 00	$ \begin{array}{c cccc} & 2 & 08 \\ & 0 & 25 \\ & 0 & 0 \\ & 0 & 0 \end{array} $	$ \begin{array}{c cccc} -17 & 31 \\ -15 & 53 \\ -17 & 17 \end{array} $		×	
	-45 29 -47 09	184 30	CR. CR. C. C.		s.e. by e. s.e. by e. e.s.e. s.e. by e. ½ e.		- 3 29	$ \begin{array}{c cccc} -19 & 43 \\ -19 & 16 \\ -18 & 23 \end{array} $			
	-47 11	1	C. C. C. Cr.	-12 04 $-13 24$	S.E. $\frac{1}{2}$ E. S.E. $\frac{3}{4}$ E. S.E. by E. $\frac{3}{4}$ E. S.E. by E.	-67 5 5	- 3 22 - 3 36	12 57	+1 30	-15 17	
	-47 33 $-48 57$	186 40	CR. CR. C. C.	-14 20	s.e. by e. s.e. by e. e. by s. ½ s. s.e. ¾ e.		- 4 07 - 3 40	$ \begin{array}{c c} -14 & 50 \\ -17 & 58 \\ -18 & 00 \end{array} $			
	-49 33 40 33	÷	C. C. C. C. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. 34 S. E. 34 S. E. 54 S. E. 52 S. E. 12 S.	$-69 \ 40$	- 4 13 - 4 13	$ \begin{array}{c c} -19 & 19 \\ -17 & 53 \\ -17 & 49 \end{array} $	+1 30	—16 52	
6.	-49 33 -49 57		CR. C. C. C. C. C.	-15 27 -15 09 -14 07 -12 35 -12 44 -13 55 -13 49	E. by s. E. ½ s.	$\left. \begin{array}{c} -69 & 37 \end{array} \right $	- 4 15 - 4 15 - 4 19 - 4 19 - 4 15	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 30	—16 36	
7.	—50 53		CR. CR. C.	$ \begin{array}{cccc} -14 & 21 \\ -15 & 02 \\ -13 & 31 \\ -14 & 35 \\ -15 & 00 \end{array} $	E. by S. S.E. by E. S.E. by E. S.E. by E. S.E. $\frac{1}{2}$ E. S.E. by E.	\right\}-69 50	- 4 18 - 3 56 - 4 06 - 3 56 - 3 41	$ \begin{bmatrix} -18 & 39 \\ -18 & 58 \\ -17 & 37 \\ -18 & 31 \end{bmatrix} $	+1 30	-16 37	
	-51 37 -51 53	194 00 195 17	C. Cr. Cr. C. C.	-14 59 -12 11 -15 47 -12 14 -13 24 -12 57 -12 00 -11 26	S.E. by E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. E. S.E. E. by S. E. by S. E. by S. E. by S. E. S.E.		 4 06 3 41 4 15 4 25 4 25 4 25 	$ \begin{array}{c cccc} -16 & 17 \\ -19 & 28 \\ -16 & 29 \\ -17 & 49 \\ -17 & 22 \\ -16 & 25 \\ \end{array} $	1 1 90	15 14	
			C. C. C.	$ \begin{array}{c cccc} -12 & 15 \\ -11 & 50 \\ -13 & 02 \\ -11 & 59 \end{array} $	E.S.E. E. by s. E. by s.	5-70 11	-419 -419 -425	$ \begin{array}{c c} -16 & 34 \\ -16 & 09 \\ -17 & 27 \\ -16 & 24 \end{array} $	+ 1 90	15 14	

1841.	Posi	ion.	Initials.	Declination	Direction of	Inclination.	Correc- tion for	Corrected		True Decli-	arks.
	Lat.	Long.	Init	observed.	ship's head.		ship's at- traction.	Declination.	index error.	nation.	Remarks
Dec. 9.	-52 27 -53 03	198 14 204 50	CR. C. C. C.	$\begin{array}{c cccc} -1\overset{\circ}{5} & 1\acute{6} \\ -12 & 10 \\ -11 & 33 \\ -10 & 32 \\ -10 & 52 \end{array}$	E.S.E. E.S.E. S.E. by E. $\frac{3}{4}$ E. E. by S. $\frac{3}{4}$ S. E. by S. $\frac{5}{4}$ S.			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0 /	
	-53 18	205 46	C.	$ \begin{vmatrix} -11 & 00 \\ -11 & 32 \\ -12 & 32 \end{vmatrix} $	E.S.E. E.S.E. E.S.E.	-70 15	- 4 20 - 4 20		+1 30	-14 54	
		205 24	CR.	$\begin{vmatrix} -12 & 11 \\ -12 & 31 \end{vmatrix}$	s.e. by e.		- 4 20 - 4 01	$\begin{vmatrix} -16 & 31 \\ -16 & 32 \end{vmatrix}$			The same district of the same same same same same same same sam
14		205 24 211 30		$ \begin{array}{r rrr} -12 & 42 \\ -13 & 27 \\ -12 & 37 \\ -13 & 57 \end{array} $	E.S.E. S.E. $\frac{1}{4}$ E. S.E. $\frac{3}{4}$ E. S.E.		$\begin{bmatrix} -3 & 57 \\ -4 & 13 \end{bmatrix}$	$\begin{bmatrix} -17 & 02 \\ -17 & 24 \\ -16 & 50 \\ -17 & 46 \end{bmatrix}$	10		martine ambient i menima a na company
	_56 24	211 45	C. C. C.	$ \begin{vmatrix} -13 & 54 \\ -12 & 24 \\ -12 & 01 \\ -21 & 03 \end{vmatrix} $	S.E. $\frac{1}{2}$ S. E. E. $\frac{1}{4}$ N. S.W. $\frac{1}{4}$ W.	\\\\>-72 00	- 3 26 - 4 43 - 4 35 + 3 57	$\begin{bmatrix} -17 & 20 \\ -17 & 07 \\ -16 & 36 \\ -17 & 06 \end{bmatrix}$	⊥1 30		
	-56 10	211 37	Cr. Cr. Cr.	-12 34	N.E. ¹ / ₄ N. s.e. by s. s.e. by s.		- 3 03 - 3 03	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$, 10 11	
	-56.29	211 50		-14 50 $-14 52$	s.e. by s. s.e. by s. s.s.e. s.e.		$\begin{bmatrix} -3 & 03 \\ -2 & 03 \end{bmatrix}$	$\begin{bmatrix} -14 & 22 \\ 3 & -17 & 53 \\ -17 & 01 \\ -17 & 04 \end{bmatrix}$			
15	56 51	212 00		$ \begin{array}{c cccc} -14 & 51 \\ -13 & 35 \\ -13 & 48 \end{array} $	S.S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ S. S.E. $\frac{3}{4}$ S.		- 2 40 - 3 3	$\begin{bmatrix} -17 & 31 \\ -17 & 06 \\ -17 & 08 \end{bmatrix}$			
	-57 09	212 26	C. C. C.	$ \begin{array}{c cccc} -13 & 42 \\ -15 & 01 \\ -13 & 59 \\ -13 & 30 \end{array} $	S.E. $\frac{3}{4}$ S. S.S.E. S.S.E. $\frac{1}{4}$ E.	72 30	- 3 20 - 2 19 - 2 19 - 2 28	$\begin{bmatrix} 0 & -17 & 02 \\ 2 & -17 & 13 \\ 2 & -16 & 11 \\ 5 & -15 & 55 \\ 2 & -15 & 51 \end{bmatrix}$	+1 30	-15 14	AND
16	-58 2	213 00	C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by E. $\frac{1}{4}$ E		- 2 19 - 2 19 - 2 00 - 1 3	$egin{array}{cccc} 2 & -16 & 55 \ 2 & -16 & 27 \ 3 & -18 & 38 \ 1 & -19 & 10 \ \end{array}$			9
AMERICA DO CONTOCA ARRESTA CARRESTA AMERICA	•		C. C. C. C.	$ \begin{array}{c cccc} -15 & 52 \\ -16 & 11 \\ -16 & 05 \\ -15 & 42 \\ -15 & 47 \end{array} $	s. by E. $\frac{3}{4}$ E. s.s.E. s.s.E.	-73 55	- 2 2: - 2 0: - 2 2: - 2 2: - 2 2:	$egin{array}{cccccccccccccccccccccccccccccccccccc$	+1 3	0 17 34	
		8 213 40 3 212 48		-19 07	s.s.e. s.s.e. s. by w.	-75 40	$ \begin{vmatrix} -2 & 2 \\ -2 & 2 \\ -2 & 3 \\ +1 & 2 \\ +0 & 4 \end{vmatrix} $	$egin{array}{cccccccccccccccccccccccccccccccccccc$		8	
	-62 5	6 212 00	C.	$ \begin{array}{c cccc} & -20 & 41 \\ & -21 & 10 \\ & -28 & 15 \\ & -27 & 18 \\ & -27 & 54 \end{array} $	s. by E. \(\frac{1}{4}\) E s. \(\frac{1}{2}\) E. s.w. by w. s.w. by w.		$ \begin{array}{c cccc} & 1 & 5 \\ & 0 & 4 \\ & + & 5 & 5 \\ & + & 5 & 5 \\ & + & 5 & 4 \end{array} $	$egin{array}{cccccccccccccccccccccccccccccccccccc$.10	0 -20 03	
			C. C. C.	$ \begin{array}{c cccc} -28 & 15 \\ -27 & 49 \\ -27 & 16 \end{array} $	s.w. by w. s.w. by w. s.w.	7.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccc} 4 & -22 & 21 \\ 1 & -21 & 38 \\ 8 & -22 & 08 \end{array} $	71 3	-20 03	
Canadament	-63 0	1 211 30	C. C. C.	$ \begin{array}{c cccc} -23 & 57 \\ -24 & 06 \\ -24 & 02 \end{array} $	s.s.w.		$\begin{vmatrix} + & 3 & 3 \\ + & 2 & 5 \\ + & 2 & 5 \end{vmatrix}$				
	-62 5	6 212 0				J	+ 5 0	8 _21 40			

1841.	Pos	ition.	Initials.	Declination		Inclination.	Correc- tion for	Corrected		True Decli-	Remarks.
	Lat.	Long.	Imit	observed.	ship's head.		ship's at- traction.	Declination.	index error.	nation.	Rem
Dec. 19.		2°0 00 209 40	C. C. C.	$ \begin{vmatrix} -2\mathring{8}, 2\acute{0} \\ -2\acute{6} & 10 \\ -31 & 10 \\ -25 & 18 \end{vmatrix} $	s.s.w. $\frac{3}{4}$ w. s.s.w. $\frac{1}{4}$ w. w. by s. $\frac{1}{2}$ s. s. by w. $\frac{1}{2}$ w.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} -22 & 43 \\ -24 & 16 \end{bmatrix}$		o /	
			C. C. C. C. C. C.	$ \begin{vmatrix} -23 & 47 \\ -21 & 21 \\ -28 & 21 \\ -29 & 18 \\ -26 & 15 \\ -25 & 04 \\ -27 & 23 \end{vmatrix} $	S. \frac{1}{4} W. S. W.S.W. S.W. S.S.W. \frac{1}{2} W. S.S.W. S.W. \frac{1}{4} W.	\right\}-77 36	+ 0 23 0 0 + 6 47 + 5 25 + 3 46 + 3 08 + 5 38	$ \begin{vmatrix} -23 & 24 \\ -21 & 21 \\ -21 & 34 \\ -23 & 53 \\ -22 & 29 \\ -21 & 56 \\ -21 & 45 \end{vmatrix} $	+1 30	—20 56	
		210 14	CR. CR. CR. CR.	$ \begin{array}{r rrrr} -24 & 51 \\ -25 & 00 \\ -27 & 16 \\ -27 & 06 \\ -28 & 50 \end{array} $	s.w. by s. s. 18° w. s. 40° w. s.s.w. s. 78° w.		+ 4 20 + 2 35 + 4 52 + 3 08 + 7 02	$ \begin{array}{c cccc} -22 & 24 \\ -23 & 58 \end{array} $			
21.	64 4 8	206 10	Cr. C. C. C.	$ \begin{array}{rrrrr} -26 & 45 \\ -22 & 59 \\ -22 & 36 \\ -25 & 09 \end{array} $	s. 78° w. s. by e. ½ e. s.s.e. s. ½ w.		+ 7 02 - 2 04 - 3 17 + 0 25	$ \begin{array}{c cccc} -19 & 43 \\ -25 & 03 \\ -25 & 53 \\ -24 & 44 \end{array} $			
200	Gr ou	205 20	C. C. C. C. C. C.	$\begin{vmatrix} -23 & 09 \\ -20 & 51 \end{vmatrix}$	S. $\frac{3}{4}$ E. S.S.W. S. S. by W. $\frac{1}{2}$ W. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	-78 30	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c cccc} -23 & 49 \\ -24 & 25 \\ -23 & 59 \\ -21 & 41 \end{array} $	+1 30	-22 55	
22.		205 20	C. C. Cr.	$ \begin{vmatrix} -25 & 11 \\ -25 & 56 \\ -27 & 31 \\ -27 & 12 \\ -27 & 32 \end{vmatrix} $	s. s. s. ³ / ₄ w. s. by w.	\right\}-79 20	0 0 + 1 20 + 1 48 0 0	$\begin{vmatrix} -25 & 56 \\ -26 & 11 \\ -25 & 24 \\ -27 & 32 \end{vmatrix}$	+1 30	-24 27	
1842.		204 00 203 37	C. Cr. C.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	s. by w. $\frac{1}{2}$ w. s.s.w. $\frac{1}{2}$ w. n.e. $\frac{1}{4}$ n.	$\left. \begin{array}{c} -79 & 40 \\ 1 & 1 \end{array} \right.$	+ 2 42 + 4 19 - 5 26	$[-27 \ 11]$		Α.	
			C. C. C. C.	$ \begin{vmatrix} -29 & 29 \\ -27 & 27 \\ -27 & 10 \\ -28 & 02 \\ -29 & 38 \end{vmatrix} $	S. \frac{1}{2} E. \frac{1}{2} E. \frac{3}{4} E. \frac{1}{4} E. \fr	-79 56	$ \begin{array}{c cccc} 0 & 0 \\ - & 0 & 57 \\ - & 1 & 25 \\ - & 0 & 28 \\ + & 1 & 54 \\ \vdots & \vdots & \ddots & \ddots \end{array} $	$ \begin{vmatrix} -28 & 24 \\ -28 & 35 \\ -28 & 30 \end{vmatrix} $	+1 07	-27 24	Card P.
9.	66 0%	204 00	C. C. C. C. C. C.	$ \begin{vmatrix} -20 & 09 \\ -34 & 42 \\ -35 & 52 \\ -23 & 47 \\ -20 & 29 \end{vmatrix} $	E.S.E. S.W.byw. $\frac{1}{2}$ W. E. $\frac{1}{2}$ S. S.W. $\frac{1}{2}$ S. W. by S. S.E. by S. S.E. $\frac{3}{4}$ E.		+ 6 14 - 8 14 + 7 58 - 8 32 + 5 54 + 8 32 - 5 13 - 7 18	$ \begin{bmatrix} -27 & 52 \\ -29 & 06 \\ -26 & 48 \end{bmatrix} $			
	And the state of t		C. C. C. C. Cr. Cr. Cr. Cr.	$ \begin{vmatrix} -19 & 20 \\ -34 & 20 \\ -19 & 35 \end{vmatrix} $	S.W. \$\frac{4}{4}\$ W. S.E. \$\frac{3}{4}\$ E. S.W. \$\frac{3}{4}\$ W. S.E. \$\frac{3}{4}\$ E. S.W. E.S.E. S.W. \$\frac{1}{2}\$ W. E. \$\frac{1}{2}\$ S. S.E. by \$E. \$\frac{3}{4}\$ E.	\}-79 52	- 7 18 + 7 18 + 7 18 - 7 18 + 6 34 - 8 14 + 7 03 - 8 32	-28 55 -26 37 -27 01 -27 52 -28 07 -27 34 -27 17 -28 07 -28 58	+1 07	-26 48	

1842.	Pos	sit	ion.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at-	Corrected		True Decli-	Remarks.
	Lat.		Lon	g.		observed.	smp s nead.		traction.	Declination.	index error.	nation.	Ren
Jan. 10.	-6°5 5	8	20°3	54	C. C	-19 32 -34 59 -18 30 -33 40 -34 14 -33 99 -32 30 -30 16 -33 04 -32 47	E. by N. w. by S. E. \(\frac{1}{4}\) S. S.W. \(\frac{3}{4}\) W. S.W. \(\frac{1}{2}\) W. S.W. \(\frac{1}{2}\) S. S.S.W. \(\frac{1}{4}\) W. S.W. by W.	>-79 48	-8 •13 +8 31 -8 31 +7 44 +7 20 +7 35 +7 02 +4 01 +7 34 +8 32	-25 30	+1 07	-25 00	
*	Ÿ				C. C	-31 04 -32 00 -23 04 -34 10 -19 17 -16 56 -19 00 -19 31 -18 33 -21 18 -19 20 -18 52	S.S.W. 3/4 W. S.S.W. 3/4 W. S.E. 1/2 S. W.S.W. S.E. S.E. by E. E.S.E. E. by S. S.E. E. by N. E.S.E.	\right\}-79 48	+4 48 +4 48 -7 02 +8 12 -6 32 -7 34 -8 12 -8 31 -6 32 -8 13 -8 12	-26 16 J -27 12 -30 06 -25 58 -25 49 -24 30 -27 12 -27 43 -27 04 -27 50 -27 33 -27 04 -27 04 -27 50 -27 33 -27 04 -27 04 -2	+1 07		
12.	-66 1	16 10	203 202	22 40	C. C. C. Cr. Cr. Cr. Cr. Cr. Cr. Cr. Cr.	-29 53 -30 13 -26 44 -26 45 -35 16 -38 22 -26 00 -23 36 -25 26	N. \(\frac{3}{4}\) W. w. by s. \(\frac{1}{2}\) s s. \(\frac{1}{4}\) W. s. by W. \(\frac{1}{2}\) W s. s. w. s. w. by W. s. \(\frac{1}{4}\) E. s. by E. \(\frac{1}{2}\) E. s. \(\frac{1}{2}\) W. E.N.E.	} −79 48	+1 09 +8 21 +1 26 +2 44 0 0 0 +6 32 +7 34 -1 26 -1 50 0 -2 44 -0 55 -7 34	-26 20 -28 27 -27 29 -26 44 -26 45 -28 44 -30 48 -27 26 -25 28 -25 26 -28 57 -27 33	+1 02	7—26 24	
28.	-67 4	10	204	10	C. CR. C.	-20 30 -30 54 -29 04 -31 48 -26 53 -33 38 -36 47 -35 19 -34 11	N.E. by E. S. $\frac{1}{2}$ W. S. $\frac{3}{4}$ E. S. $\frac{3}{4}$ W. N. $\frac{1}{2}$ E. N.W. $\frac{1}{4}$ N. S.W. $\frac{1}{4}$ S. S.W. by S.	-80 34	$ \begin{array}{c cccc} -6 & 42 \\ +1 & 01 \\ -1 & 30 \\ +1 & 30 \\ -0 & 50 \\ +5 & 52 \\ +6 & 38 \\ +5 & 36 \\ +3 & 53 \end{array} $	-29 53 -30 34 -30 18 -27 43 -27 46 -30 09 -29 43 -30 22	+1 07	—28 19	45
	-67 3 -67 1				C. C. C. C. C. C.	-19 11 -21 47 -35 06 -32 27 -26 24 -31 53 -31 04 -29 03 -31 39	E. $\frac{3}{4}$ S. E. by S. S.S.W. $\frac{1}{4}$ W. S.S.W. S. by E. $\frac{1}{2}$ E. S. $\frac{1}{2}$ W. S. $\frac{3}{4}$ W. S. $\frac{1}{2}$ W. S. by W.	-80 40	$\begin{array}{c} -9 & 14 \\ -9 & 20 \\ +4 & 20 \\ +3 & 57 \\ -2 & 58 \\ +1 & 02 \\ +1 & 33 \\ +1 & 02 \\ +2 & 01 \end{array}$	-31 07 -30 46 -28 30 -29 22 -30 51 -29 31 -28 01 -29 38	+1 07	-28 37	
-	-67 1	3	202	35	C. Cr. Cr.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. $\frac{3}{4}$ w. s.s.w. $\frac{1}{4}$ w. s.s.w.		$\begin{vmatrix} +1 & 33 \\ +4 & 20 \\ +3 & 57 \end{vmatrix}$	$\begin{bmatrix} -30 & 46 \\ -29 & 44 \end{bmatrix}$			

1842.	Posi	tion.	Initials.	Declination		Inclination.	Correc- tion for	Corrected		True Decli-	Remarks.
	Lat.	Long.	Im	observed.	ship's head.		ship's at- traction.	Declination.	index error.	nation.	Rem
Feb. 1.	−67 ź0	201 40	C. C. C.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.e. N. 72° w. s. 27° e. N. 25° w.		+ 8 45 - 4 51 + 3 46	$ \begin{array}{c cccc} -25 & 38 \\ -30 & 53 \\ -27 & 52 \end{array} $	o /	0 /	
		÷	C. C. C. C. C.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. 50° W. S. 5° E. S. 5° E. N. 15° E. N. 14° W. W.	-80 45	+ 2 11 + 9 25	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 07	-28 33	,
2. 3.	-67 46 -68 06 -68 40	199 40	CR. CR. C. C. C.	$\begin{array}{r} -28 & 37 \\ -37 & 55 \\ -28 & 02 \\ -29 & 23 \\ -31 & 03 \\ -28 & 10 \end{array}$	S.S.E. S.S.W. S.S.E. $\frac{1}{2}$ E. S.E. $\frac{3}{4}$ E. S.E. $\frac{1}{4}$ S.		$\begin{array}{rrrrr} + & 4 & 04 \\ - & 4 & 57 \\ - & 7 & 22 \\ - & 7 & 39 \\ - & 6 & 36 \end{array}$	$ \begin{array}{c cccc} -33 & 51 \\ -32 & 59 \\ -36 & 45 \\ -38 & 42 \\ -34 & 46 \end{array} $			
	-67 58	199 50	C. C. C. C. C.	$\begin{array}{r} -44 & 56 \\ -44 & 26 \\ -43 & 50 \\ -42 & 51 \\ -42 & 07 \\ -41 & 14 \end{array}$	w. by s. w.s.w. w.s.w. w. by s. ½ s. w. by s. w. by s.	-81 00	+ 9 19 + 9 19 + 9 30 + 9 42 + 9 42	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 30	-32 43	Card R.
4.	68 52	199 40	CR. CR. C. C. C.	-26 59 -30 29 -40 55 -38 40 -38 46 -34 27	S.S.E. S.S.E. N.W. $\frac{1}{4}$ W. N.W. $\frac{3}{4}$ N. N.W. $\frac{1}{4}$ N.	-81 38	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 30	-30 47	
8.	-70 06	186 20	C. C. C. C. C.	$ \begin{vmatrix} -36 & 02 \\ -40 & 17 \\ -38 & 50 \\ -37 & 51 \\ -37 & 00 \\ -37 & 30 \end{vmatrix} $	N.N.w. ³ / ₄ W. s.w. by s. s.s.w. ¹ / ₄ W. s. ³ / ₄ E. s. by E. ³ / ₄ E. s. ¹ / ₂ E.	-83 30	+ 6 19 + 4 51 - 2 08 - 4 53 - 1 25	$ \begin{array}{c cccc} -39 & 59 \\ -41 & 53 \\ -38 & 55 \end{array} $			
9.		185 40 185 10	CR. C. C. C. C. C.	-37 06 -53 35 -57 49 -55 20 -54 51 -55 48 -54 57	S. $\frac{3}{4}$ E. W. W. $\frac{3}{4}$ S. W. $\frac{1}{2}$ S. W. S. 85° W. S. 85° W.		$\begin{vmatrix} +14 & 38 \\ +14 & 40 \\ +14 & 43 \\ +14 & 41 \end{vmatrix}$	$\begin{array}{c c} -39 & 14 \\ -38 & 52 \\ -43 & 11 \\ -40 & 40 \\ -40 & 08 \\ -41 & 07 \\ -40 & 17 \\ \end{array}$	+1 30	—38 5 5	
	—70 22	185 00	C. C. C. C. C.	-54 57 -55 05 -54 54 -56 07 -53 58 -55 06 -53 56	w. 3/4 s. w. 3/4 s. w. 3/4 s. w. 100° w. s. 78° w.	-84 00	+14 38 +14 38 +14 43 +13 31 +14 15	$ \begin{array}{c cccc} -40 & 27 \\ -40 & 16 \\ -41 & 24 \\ -40 & 27 \end{array} $	·		
		185 40	Cr. Cr. Cr. Cr.	$ \begin{array}{r} -53 & 02 \\ -51 & 03 \\ -52 & 21 \\ -49 & 34 \end{array} $	w. by n. w.n.w. w. by n. w.		$+14 15 \\ +13 16$	$ \begin{array}{c c} -38 & 47 \\ -37 & 47 \\ -38 & 06 \end{array} $	+1 30	—38 17	
	-10 00	200 10	CR. CR. CR.	-56 21 -56 14 -53 30	w. W. W. ½ N. W.N.W.		$+14 43 \\ +14 30$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-	

1842.	Posi		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at-	Corrected Declination.	Correction for index	True Decli- nation.	Remarks.
	Lat.	Long.	-				traction.		error.		- Be
Feb. 10.	−7°0 1′4	184 0Ó	C. C. C.	- 53 45 - 51 09 - 28 40 - 28 57	s.w.byw. <u>3</u> w. s.e. <u>1</u> e.		$+13 \cdot 03$ $-10 \cdot 54$	$\begin{bmatrix} -39 & 38 \\ -38 & 06 \\ -39 & 34 \\ -41 & 02 \end{bmatrix}$	0 /	• /	
		-30	C. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by e. w. by s. $\frac{1}{2}$ s. w. $\frac{3}{4}$ s. w. by s.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{bmatrix} -41 & 17 \\ -40 & 25 \\ -38 & 37 \\ -38 & 42 \end{bmatrix}$			
Vergan-rander/Coronical and		*	C. C. C.	- 51 25 - 50 32 - 50 33 - 37 01	w. by s. w.n.w. n. ½ E.	}−83 45 	$\begin{vmatrix} +14 & 02 \\ +12 & 43 \\ -1 & 17 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 30	-37 19	
AND THE REAL PROPERTY OF THE P		- 1	Cr. Cr. Cr. Cr.	- 28 15 - 53 43	s.e. by s. s.e. $\frac{1}{2}$ e.		$\begin{bmatrix} -8 & 17 \\ -11 & 17 \\ +14 & 05 \end{bmatrix}$	$\begin{bmatrix} -35 & 38 \\ -37 & 45 \\ -39 & 32 \\ -39 & 38 \\ -40 & 03 \end{bmatrix}$			
- 12.	71 04	180 46	C. C. C.	- 30 39 - 29 45 - 31 59 - 32 18	s.e. ½ s. s.e. s.e. by s.		$ \begin{array}{c cccc} -11 & 16 \\ -11 & 53 \\ -9 & 24 \\ -10 & 00 \end{array} $	$ \begin{vmatrix} -41 & 55 \\ -41 & 38 \\ -41 & 23 \\ -42 & 18 \end{vmatrix} $	+1 30	-40 45	
14.	-73 14	181 08	CR. C. CR.	- 37 39		$\left.\right _{-86.00}$	-15 24	$\begin{bmatrix} -44 & 02 \ -53 & 03 \ -53 & 33 \end{bmatrix}$	+1 30	-51 48	
1	-75 04		C.	$\begin{bmatrix} -59 & 26 \\ -40 & 57 \end{bmatrix}$	s.e. by s. s.e. by e.	$\left \begin{cases} -87 & 00 \end{cases} \right $	$\begin{bmatrix} -18 & 03 \\ -27 & 15 \end{bmatrix}$	$\begin{bmatrix} -77 & 29 \\ -68 & 12 \end{bmatrix}$		FC 00	
	-76 04		C.	$ \begin{vmatrix} -56 & 12 \\ -56 & 34 \\ -58 & 13 \end{vmatrix} $		$\left \right -87 00$	-24 47	$ \begin{vmatrix} -86 & 15 \\ -81 & 21 \\ -82 & 00 \end{vmatrix} $	+1 30	-76 03	
18.	-76 54	182 17		$ \begin{array}{r rrrr} - & 80 & 43 \\ - & 75 & 23 \\ - & 74 & 51 \end{array} $	N. \(\frac{1}{4}\) E. N. \(\frac{1}{4}\) W.		$\begin{vmatrix} + & 1 & 19 \\ -13 & 23 \end{vmatrix}$	$\begin{bmatrix} -82 & 02 \\ -74 & 04* \\ -88 & 14 \\ -81 & 37 \end{bmatrix}$	+1 30	-82 28	
	-76 12	*	C.	- 58 32 - 51 19	N.E. N.E.by E. ½ E.	05 55	$\begin{vmatrix} -15 & 00 \\ -18 & 53 \end{vmatrix}$	$\begin{bmatrix} -73 & 32 \\ -70 & 12 \end{bmatrix}$	+1 30	-70 22	
22.	-76 32	194 40	C. C.	$ \begin{array}{r rrrr} - & 72 & 15 \\ - & 74 & 30 \\ - & 72 & 24 \end{array} $	S.S.E. ¹ / ₄ E. S.S.E.			$\begin{bmatrix} -81 & 02 \\ -82 & 24 \\ -83 & 50 \end{bmatrix}$			
ET	-77 00	,	C. C. C.	$ \begin{array}{r rrrr} - & 60 & 26 \\ - & 72 & 10 \\ - & 65 & 19 \end{array} $	E.S.E. E.S.E.	85 30	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+1 30	-81 23	
23				$\begin{vmatrix} -70 & 48 \\ -69 & 19 \end{vmatrix}$	w. by N. $\frac{3}{4}$ N E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{bmatrix} -92 & 06 \\ -90 & 30 \\ -88 & 54 \end{bmatrix}$			
	70.04	* -	C. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. W. $\frac{1}{2}$ N. W.N.W.	85 30	+17 59	$\begin{bmatrix} -90 & 07 \\ -89 & 23 \\ -85 & 23 \end{bmatrix}$	+1 30	-88 01	
24 25	-75 22	200 00	C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. W. $\frac{1}{2}$ N. N. 75° W.	-85 00	$\begin{vmatrix} +12 & 05 \\ +17 & 30 \\ +16 & 57 \end{vmatrix}$	$\begin{bmatrix} -89 & 55 \\ -83 & 30 \\ -67 & 24 \\ -62 & 14 \\ -58 & 55 \end{bmatrix}$	+1 30	-64 33	
28	_71 00	184 10	CR.	-5639 -5604	$N \cdot \frac{1}{2} E \cdot W$	04.00	$\begin{vmatrix} -1 & 38 \\ +14 & 43 \end{vmatrix}$	$\begin{bmatrix} -58 & 10 \end{bmatrix}$ $\begin{bmatrix} -41 & 21 \end{bmatrix}$		20.00	- *-
	-70 54	183 50	Cr.	$\begin{bmatrix} -55 & 15 \\ -52 & 17 \end{bmatrix}$		$\left \right\} - 84 00$		$\begin{pmatrix} -40 & 46 \\ -37 & 40 \end{pmatrix}$	+1 30	38 26	

^{*} Doubtful; omitted in the mean.

1842.	P	osit	ion.		Initials.	Declination		Inclination.	Correction for ship's at-	Corrected Declination.		True Decli-	Remarks.
	Lat.		Long	g.	Ini	observed.	ship's head.		traction.	Decimation.	error.	nation.	Ren
Mar. 1.	−7° 0 1	ιΌ	180	20	C.	-48 05	w. by N. ½ N. w. N. w.	$\left. \begin{array}{c} \cdot \\ -83 \ 45 \end{array} \right.$	$+14 23 \\ +13 52 \\ +14 52$	$ -34 \ 13 >$	+1 30	。, —31 26	
2.	-67 E	54	183	40	Cr. C. C. C.	-47 46 -26 18 -24 31 -25 00	w. by n. n.n.e. n.e. by n. n. by e. ½ e.	$\left. \begin{array}{c} -82 & 20 \end{array} \right.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{bmatrix} -32 & 54 \\ -30 & 45 \\ -31 & 02 \\ -28 & 21 \end{bmatrix} $	+1 30	-28 50	
3.	-688 -673				Cr. C. C.	-26 47 -22 20 -19 15	N.N.E. N.E. $\frac{3}{4}$ E. N.E. $\frac{1}{4}$ N.] }		$\begin{bmatrix} -31 & 14 \\ -31 & 26 \end{bmatrix}$			
					C. C.	-24 24 $-23 27$ $-24 07$	N.E. ½ N. E.N.E. N.E.	$-82\ 00$		$\begin{vmatrix} -34 & 04 \\ -32 & 03 \end{vmatrix}$	+1 30	-29 46	
5.	_67 I	19	187	25	Cr. Cr. C. Cr.	$ \begin{array}{rrr} -25 & 40 \\ -22 & 50 \\ -25 & 52 \\ -26 & 54 \end{array} $	N.N.E. $\frac{1}{2}$ E. N.E. by E. N. $\frac{1}{2}$ W. N. by W.	$\left.\begin{array}{c} \\ \\ \end{array}\right\}$ -81 10	$\begin{vmatrix} - & 9 & 26 \\ + & 0 & 57 \end{vmatrix}$				
6.	65 I				C. C. Cr.	-24 59 $-24 14 $ $-25 43$	N. by E. N. by E. ½ E. N.N.E.	79 30	$\begin{bmatrix} - & 2 & 21 \\ - & 3 & 08 \end{bmatrix}$	-28 51	+1 30	-25 02	
8.	-64 4 -62 9	56 26	192 195	24 40	Cr. C. Cr.	$\begin{array}{r} -27 & 15 \\ -20 & 31 \\ -22 & 33 \\ -18 & 16 \end{array}$	N. N. $\frac{3}{4}$ E. N. N. by E.		- 0 58 0 0 - 1 18	$ -19 \ 34 \rangle$	+1 30	-19 41	-
9.	<u>-61</u>	00	199	00	CR. C. C. CR.	$ \begin{array}{rrrr} -22 & 28 \\ -17 & 27 \\ -14 & 35 \\ -17 & 46 \end{array} $	N. by w. N.E. E.N.E. N.E.	$\left.\right $ -76 10	$\begin{vmatrix} + & 1 & 18 \\ - & 4 & 20 \\ - & 5 & 55 \\ - & 4 & 20 \end{vmatrix}$	$\begin{bmatrix} -21 & 47 \\ -20 & 30 \end{bmatrix}$	+1 30	-19 49	4
10.	—60	20	205	36	Cr. C. C. C.	$ \begin{array}{c cccc} -15 & 00 \\ -15 & 04 \\ -14 & 25 \\ -13 & 58 \end{array} $	E.N.E. E. by N. ½ N. E.N.E.	$\left.\right \right> -75 \ 15$			+1 30	-18 20	
12.	60	18	204 212		CR. C. C.	$ \begin{array}{c cccc} -13 & 39 \\ -12 & 51 \\ -12 & 57 \end{array} $	E.N.E. E. by N. E. by N.		- 5 30 - 5 34 - 5 34	$\begin{bmatrix} -19 & 09 \\ -18 & 25 \\ -18 & 31 \end{bmatrix}$			
	_60 _59				C. C. Cr. Cr.	$ \begin{array}{r rrrr} -12 & 59 \\ -11 & 39 \\ -16 & 30 \\ -16 & 01 \end{array} $	E. by N. E.N.E. N.E. N.E. by E.	} —74 15	- 5 06 - 3 43	$ \begin{array}{c cccc} -18 & 33 \\ -16 & 45 \\ -20 & 13 \\ -20 & 30 \end{array} $	+1 30	-17 19	
	-58				C. C. C.	$ \begin{array}{c cccc} -12 & 10 \\ -13 & 06 \\ -10 & 27 \end{array} $	E. by N. E. by N.		- 4 59 - 5 26	$\begin{bmatrix} -17 & 36 \\ -18 & 05 \\ -15 & 53 \\ -18 & 38 \end{bmatrix}$	+1 30	_16 03	
16. 18.	$-58 \\ -60$	58 18	227 236	00 30	C. Cr. C.	$ \begin{array}{r rrrr} -13 & 12 \\ -13 & 00 \\ -18 & 40 \\ -15 & 26 \end{array} $	E. by N. E. by s. E.		- 5 31 - 5 24	-18 31		$\begin{vmatrix} -17 & 01 \\ -20 & 57 \end{vmatrix}$	
19 22	$-60 \\ -58$	02 28	240 251	31 40		$ \begin{vmatrix} -17 & 03 \\ -17 & 53 \\ -18 & 33 \end{vmatrix} $	E. by N.	$\begin{bmatrix} J \\ -72 & 15 \end{bmatrix}$	- 5 24 - 4 25 - 4 25 - 4 45	$\begin{bmatrix} -22 & 18 \\ -23 & 02 \end{bmatrix}$		-20 48	-
23	_58	36	255	20	CR. CR. CR.	$ \begin{vmatrix} -19 & 58 \\ -20 & 22 \\ -20 & 41 \end{vmatrix} $	E. by N.		- 4 29 - 4 29 - 4 18	$\begin{bmatrix} -24 & 27 \\ -24 & 51 \end{bmatrix}$ $\begin{bmatrix} -24 & 51 \end{bmatrix}$ $\begin{bmatrix} -24 & 59 \end{bmatrix}$	+1 30	22 46	
Market Control of the					C. C. C.	$ \begin{array}{r rrrr} -24 & 18 \\ -23 & 57 \\ -24 & 13 \\ -21 & 04 \end{array} $	E. by N.	-70 11			+1 3	0 -24 46	
				-	C. C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by N. $\frac{1}{4}$ N		- 4 0	$\begin{bmatrix} -26 & 16 \\ 8 & -25 & 01 \end{bmatrix}$			

1842.	Po	siti	on.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's at-	Corrected Declination.		True Declination.	Remarks.
	Lat.		Lon	g.	II I	obscivcu.	sinp s nead.		traction.	Decimation	error.	nation.	Rer
Mar. 24.	$-\mathring{58}$ $\overset{\circ}{4}$	6	2Š7	50	C. C. Cr.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	E. $\frac{3}{4}$ N. E. by N.	$\left.\right\}$ -69 45	- 4 15 - 4 11 - 4 11	$ \begin{vmatrix} -26 & 07 \\ -29 & 10 \\ -27 & 52 \end{vmatrix} $	。 / +1 30	° ' -26 13	
25. 26.					Cr. C. C.	$ \begin{array}{rrr} -27 & 53 \\ -23 & 47 \\ -24 & 43 \end{array} $	E. by n. E.N.E. E.N.E. E. by n. 3/4 n.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{bmatrix} -31 & 31 \\ -27 & 11 \\ -28 & 12 \end{bmatrix}$			
					C. Cr. Cr.		E. by N. $\frac{1}{2}$ N. N.E. by E. $\frac{3}{4}$ E. E.N.E. N.E.		$ \begin{vmatrix} -3 & 34 \\ -3 & 17 \\ -3 & 24 \\ -2 & 24 \end{vmatrix} $	$egin{array}{c c} -27 & 04 \\ -28 & 48 \\ -25 & 46 \\ -28 & 15 \\ \hline \end{array}$	+1 30	-26 25	
27.	59 0	4	272	20	Cr. C. C. Cr.	$ \begin{array}{rrrr} -22 & 29 \\ -25 & 45 \\ -26 & 39 \\ -25 & 53 \end{array} $	E. E.N.E. E.N.E.	$\left\{ -67.00 \right\}$	- 4 01 - 3 16 - 3 16 - 3 16	$\begin{bmatrix} -26 & 30 \\ -29 & 01 \end{bmatrix}$	+1 30	-27 08	
28.	-58 5				Cr. C. C.	$ \begin{array}{r} -23 & 12 \\ -26 & 15 \\ -27 & 37 \end{array} $	E.N.E. N.E. by E. N.E. by E.		$\begin{vmatrix} - & 3 & 16 \\ - & 2 & 35 \\ - & 2 & 35 \end{vmatrix}$	$\begin{bmatrix} -26 & 28 \ -28 & 50 \ -30 & 12 \end{bmatrix}$			
	-58 5	4	z/0	40	00000	$ \begin{array}{rrr} -30 & 22 \\ -29 & 25 \\ -27 & 06 \\ -27 & 54 \end{array} $	N. by E. N.E. by E. N.E. by E.	-65 30	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{vmatrix} -29 & 58 \\ -29 & 41 \\ -30 & 29 \end{vmatrix}$	+1 30	-28 25	
29.	-58 2 $-58 2$				CR. C. C. C.	$ \begin{array}{r} -26 & 44 \\ -24 & 53 \\ -25 & 19 \\ -31 & 06 \end{array} $	N.E. by E. N.E. by E. N.E. by E. N. by W.		$ \begin{vmatrix} -2 & 35 \\ -2 & 30 \\ -2 & 30 \\ +0 & 31 \end{vmatrix} $	$\begin{bmatrix} -27 & 23 \\ -27 & 49 \\ -30 & 35 \end{bmatrix}$	-		
					C. C. C. C.	$ \begin{array}{rrr} -29 & 30 \\ -24 & 59 \\ 27 & 46 \\ -25 & 09 \end{array} $	N. by E. E. N.E. \frac{1}{2} E. E.N.E.	-64 50	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{bmatrix} -30 & 01 \\ -28 & 04 \end{bmatrix}$	+1 30	-27 13	
30.	-58 2 $-58 3$				Cr. Cr. Cr.	$ \begin{array}{rrrr} -25 & 27 \\ -27 & 45 \\ -25 & 08 \\ -24 & 51 \end{array} $	E.N.E. N. E. N.E. by E. ½ E.		$ \begin{array}{c cccc} & 2 & 55 \\ & 0 & 0 \\ & 3 & 30 \\ & 2 & 35 \end{array} $	$\begin{bmatrix} -27 & 45 \\ -28 & 38 \end{bmatrix}$ $\begin{bmatrix} -27 & 26 \end{bmatrix}$		70	
,					C. C. C.	$ \begin{array}{r} -24 & 19 \\ -25 & 46 \\ -25 & 46 \\ -25 & 16 \end{array} $	E.N.E. $\frac{1}{2}$ E. N.E. by E. N.E. by E.	 -63 40	$ \begin{vmatrix} - & 2 & 47 \\ - & 2 & 08 \\ - & 2 & 23 \\ - & 2 & 23 \end{vmatrix} $	$\begin{bmatrix} -28 & 09 \\ -27 & 39 \end{bmatrix}$. 1 90	-26 49	
					C. C. C.	$ \begin{array}{r} -25 & 49 \\ -27 & 18 \\ -25 & 46 \\ -26 & 05 \end{array} $	n.e. by e. n.e. by e. n.e. by e. n.e. by e. ½ e.	-05 40	- 2 23 - 2 23 - 2 23 - 2 35	$ \begin{bmatrix} -29 & 41 \\ -28 & 09 \\ -28 & 40 \end{bmatrix} $	+1 90	-20 4g	
	-58 3	0 8	282	30	C. C. Cr. Cr.	$ \begin{array}{rrrr} -27 & 48 \\ -25 & 46 \\ -25 & 43 \\ -25 & 04 \\ -25 & 25 \end{array} $	e. by n. E. by n. E. hy n.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} -30 & 11 \\ -28 & 48 \\ -28 & 45 \\ -27 & 45 \\ -28 & 27 \end{array} $			
31.	-58 2				CR. C. C.	-23 46 -26 49 -25 59	e. by n. n.e. by n. n.e. by n.	}−63 00	$ \begin{array}{r rrrr} & 2 & 41 \\ & 1 & 23 \\ & 1 & 23 \end{array} $	$ \begin{array}{c c} -26 & 27 \\ -28 & 12 \\ -27 & 22 \end{array} $	-1 30	-26 13	
April 1.	-583 -573				CR.	$-24 06 \\ -25 30$	N.E. by N.	$-61 \ 13$	$\begin{bmatrix} - & 1 & 50 \\ - & 1 & 16 \end{bmatrix}$		+1 30	-25 16	
3.	$-56\ 4$ $-52\ 2$	6 9	294	30	C. Cr. C.	$ \begin{array}{rrr} -21 & 46 \\ -19 & 07 \\ -21 & 21 \end{array} $	N.E. N.E. N. by E.	$\left. \begin{array}{c} -59 & 00 \\ \end{array} \right.$	- 1 30 - 1 30	$ \begin{bmatrix} -23 & 16 \\ -20 & 37 \end{bmatrix} $ $ \begin{bmatrix} -21 & 38 \end{bmatrix} $		-20 26	
	-51 5				C. C.	-18 20 $-20 32$ $-19 07$	n. by E. n. by E. n.n.w.		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c c} -18 & 38 \\ -20 & 49 \\ -18 & 37 \end{array} $	+1 30	-18 25	

Observations of the Inclination made on board Her Majesty's Ship Erebus, with Needle R. F. 5, between April 1841 and August 1842.

Observers Captain Sir James Clark Ross and Lieutenant Alexander Smith, R.N.

				Observed	7	Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
April 19.		n, Magne- ervatory.	Direct. S. N.	$-70 18.4 \\ -70 38.2 \\ 50 80.0$,	,	0 / 0 /	R. F. 4, used as de- flector.
20.	-4z 5z	14/ 24	N.S. Direct.* N.S. at 24° 44'.	$ \begin{array}{rrrr} -70 & 30.9 \\ -70 & 22.1 \\ -70 & 26.3 \\ -70 & 30.6 \end{array} $				F0.00 F0.00	
24.		1,	S. at 56° 20′. N. at 53° 02′. Direct.	$ \begin{array}{rrrr} -70 & 02.7 \\ -70 & 12.5 \\ -70 & 24.3 \end{array} $	Observed on shore.	••	-6	$-70 \ 32 \ -70 \ 32$	R. F. 3, used as de- flector.
			S. N. S. at 38° 11′.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		*			icetor.
June 29.	At a	nchor.	N. at 43° 54′. Direct. S. Direct.	-70 29·9 -71 38·9 -71 50·7 -71 40·5	N. N.	+81 +81	$\begin{vmatrix} -7 \\ -7 \\ -7 \end{vmatrix}$	} -/0 31	R. F. 4, used as deflector.
			S. Direct. S.	-71 40.3 $-71 52.5$ $-71 38.0$ $-71 57.3$	N.N.E. N.N.E. N.E. N.E.	+78 +78 +67 +67	$ \begin{bmatrix} -7 \\ -7 \\ -7 \\ -7 \\ -6 \\ -6 \\ -6 \end{bmatrix} $. 12
			Direct. S. Direct.	-71 31.4 $-71 31.8$ $-70 55.5$	E.N.E. E.N.E.	$+47 \\ +47 \\ +20$	$\begin{vmatrix} -6 \\ -7 \\ -6 \end{vmatrix}$	$\left. \begin{array}{c} -70 & 42 \\ 70 & 45 \end{array} \right $	
			S. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. E.S.E. E.S.E.	+20 -12 -12	$\begin{vmatrix} -6 \\ -6 \end{vmatrix}$		
			Direct. S. Direct.	-69 53.6 $-69 55.1$ $-69 17.0$	S.E. S.E. S.S.E.	$-43 \\ -43 \\ -67$		$\left. \begin{array}{c c} -70 & 43 \\ -70 & 44 \end{array} \right $	
			S. Direct. S. Direct.	$-69 ext{ } 46.4$ $-69 ext{ } 03.3$ $-69 ext{ } 14.9$	S.S.E. S. S.	-67 -80 -80	$ \begin{array}{r} -6 \\ -5 \\ -5 \end{array} $	$\left. \left. \left. \left. \right. \right\} -70 \right. 34 \right\} -70 \left. 39 \right \right. $	
	-		S. Direct. S.	-69 26.5 $-69 40.3$ $-69 41.0$ $-69 51.4$	S.S.W. S.S.W. S.W.	-67 -67 -43 -43	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \end{array} $	$\begin{cases} -70 & 46 \\ -70 & 35 \end{cases}$	
			Direct. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w.s.w. w.s.w. w.	-12 -12 $+20$	$ \begin{array}{c c} -6 \\ -6 \\ -6 \end{array} $	\begin{cases} -70 & 39 \\ 70 & 80 \end{cases}	
		*	S. Direct. S.	$\begin{array}{c cccc} -70 & 49.1 \\ -71 & 10.4 \\ -71 & 19.3 \end{array}$	W. W.N.W. W.N.W.	$+20 \\ +47 \\ +47$	$ \begin{array}{r} -6 \\ -6 \\ -7 \end{array} $	$ \begin{cases} -70 & 32 \\ -70 & 34 \end{cases} $	
			Direct. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.W. N.W. N.N.W.	+67 + 67 + 78	-7 -7 -7 -7	$ \begin{cases} -70 & 35 \\ -70 & 39 \end{cases} $	
			S. Direct. S.†	$ \begin{array}{c cccc} -71 & 58.3 \\ -71 & 42.5 \\ -72 & 03.3 \end{array} $	N•N•W• N• N•	+78 +81 +81		$\begin{cases} -70 & 39 \\ -70 & 39 \end{cases}$	

* Observed on shore;
$$\begin{cases} \text{Direct.} - \mathring{71} & 40.6 \\ \text{S.} & -71 & 09.6 \\ \text{N.} & -71 & 20.1 \\ \text{N.S.} & -71 & 10.8 \end{cases}$$

[†] Face west. $\begin{cases} \text{Direct.} - \mathring{73} \ \mathring{07} \cdot 8 \\ \text{S.} \quad -72 \ 34 \cdot 9 \end{cases}$ Head north.

				Observed	D:	Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination. Remarks.	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,									
July 7.	0 /	• /	Direct.	-70 16.1	S.E. 1/2 E.	-37	-6	h ° ′ ° ′	
, and			S.	-70 03.4	S.E. ½ E.	-37	-6		
-			N.	-70 05.4	S.F. \(\frac{1}{2}\) E.	-37	-6	> -70 54 -70 54 Running out Storm Bay.	of
			N.S.	-70 12.0	S.E. 1/2 E.	-37	-6	Storm Bay.	
8.	49.00	140 00	Direct.	$-70 \ 18.9$	S.E. \(\frac{1}{2}\) E.	-37	$-\frac{6}{7}$	K	
8.	-43 00	148 28	S.	$-71 27.3 \\ -71 43.2$	N.N.E.	$ +78 \\ +78$	$-7 \\ -7$		
			N.	$-71 \ 36.7$	N.N.E.	+78	-7	>-70 25 -70 25 A heavy head sea	a.
			N.S.	-71 39.1	N.N.E.	+78	-7		
			Direct.	-71 32.2	N.N.E.	+78	-7		
9.	-42 13	149 25	Direct.	$-70 \ 46.5$	N.N.W.	+77	6	<u> </u>	
			S.	-70 56.3	N.N.W.	+77	-6	0. 25	
			N.	-71 126	N.N.W.	+77	$\begin{vmatrix} -7 \\ -6 \end{vmatrix}$	-69 37 -69 37 A head sea.	
			N.S. Direct.	$-70 \ 30.2$	N.N.W.	+77	-6		
10	-40 55	140 10	Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.W. N. by W.	$+77 \\ +76$	-6	R	
10.	- 10 00	119 12	S.	$-69 \ 53.7$	N. by w.	+76	-6	00 10	
			Ñ.	$-69 \ 47.1$	N. by w.	+76	-6	├ -68 41	
			N.S.	-69 49.2	N. by w.	+76	-6		
11.	-3750	150 22	Direct.	-67 47.8	N₀ by w.	+72	-5	<u> </u>	
			N.	-67 53.9	N. by w.	+72	-5	>−66 36 −66 36	
			N.S.	-67 28.9	N. by w.	+72	-5	00 00 -00 00	
10	or o:	151 00	Direct.	-67 40.4	N. by w.	+72	-5	Į l	ı
12.	-37 21	151 33	Direct.	$\begin{vmatrix} -67 & 01.6 \\ -66 & 58.0 \end{vmatrix}$	N.E.	+62	-4	-	
			S. N.	-67 03.3	N.E.	$+62 \\ +62$	$-4 \\ -4$	> -66 01 -66 01	
			N.S.	$-66\ 49.4$	N.E.	+62	_4	00 01	
			Direct.	-67 04.8	N.E.	+62	-4		
13.	-3601	151 48	Direct.	-66 19.0	n.w. by n.	+64	_4	ň l	
A Committee of the Comm			N.	-65 57.0	n.w. by n.	+64	_4	-65 04 -65 04 Much motion.	
			N.S.	-6559	n.w. by n.	+64	_4	do of the motion.	
			Direct.	$-66\ 08.5$	n.w. by n.	+64	_4	Ž .	
14.	-3352	151 21	Direct.	-64 05.9	N.	+67	_3		
			S. N.	-64 20.3 $-64 05.4$	N. N.	$+67 \\ +67$	$-3 \\ -3$	>-63 15) Running along t	ha
			N.S.	-64 00.8	N.	+67	-3	land into Po	rt
			Direct.	-65 03.8	N.	+67	_3	Jackson.	
14.	-33 51	151 20	Direct.	-63 49.0	n. by w.	+66	3	$-62 \ 46$	
			Direct.	$-63\ 37.9$	N.W.	+58	_3	$-62 \ 43$	
0			Direct.	-62 05.5	s.w. by w.	-17	_2	-62 25	i
			Direct.	-62 03.1	S.E.	-35	_2	$-62 \ 40$	
31.			Direct.	-61 52.5 $-63 11.9$	S.S.W. ½ W.	-51	_2	$\begin{vmatrix} -62 & 46 \\ 62 & 56 \\ \end{vmatrix} -62 & 47 \end{vmatrix}$	
91.	Ator	chor.	Direct. S.	$-63 \ 24.0$	w. w.	$+25 \\ +25$	$-2 \\ -3$	$\left. \left\{ -62\ 56 \right\} ^{-62\ 47} \right $	
1	-33 51		Direct.	-62 19.1	w.s.w.	_ 2	_2	-62 23	
	33 31		Direct.	-61 12.6	s.	-63	_2	} -62 24	
			S.	-61 26.1	s.	-63	_2	} -0z z4	
-	***************************************		Direct.	$-61 \ 31.5$	s.s.w.	-53		34	
			S.	$-61 \ 47.5$	s.s.w.	-53	-2	{	
Aug. 3.	and the same of th		Direct.	$-63 \ 30.1$	N.E.	+58	$ \begin{array}{c c} -3 \\ -3 \end{array} $	$-62 \ 40$	
			S.	-63 40.9	N.E.	+58	-0	J	

				Observed		Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
July 15.	Syd	lsland, lney. 151 17	Direct. S. N.	$ \begin{vmatrix} -62 & 40.8* \\ -62 & 50.1 \\ -62 & 49.9 \end{vmatrix} $	Ì		-2 -2 -2	· · · · · · · · · · · · · · · · · · ·	
Aug. 4.	,		N.S. Direct. S. N.	$\begin{array}{c cccc} -62 & 42.9 \\ -62 & 45.9 \\ -62 & 50.1 \\ -62 & 50.2 \\ \end{array}$	Observed on shore.	-	$ \begin{array}{r} -2 \\ -2 \\ -2 \\ -2 \end{array} $	} −62 48 −62 48	
5.			N.S. Direct. Direct. Direct.	$\begin{array}{c cccc} -62 & 40 & 3 \\ -63 & 40 \cdot 6 \\ -63 & 03 \cdot 4 \\ -63 & 06 \cdot 5 \end{array}$	N.N.E. E. by N. E. by N.	$+64 \\ +35 \\ +35$		-62 40	
c	99. 50	154.08	S. N. N.S. Direct.	$ \begin{array}{r} -63 & 22.6 \\ -63 & 26.1 \\ -63 & 23.0 \\ -63 & 09.8 \end{array} $	E. by N.E. by N.E. by N.	$+35 \\ +35 \\ +35 \\ +35$	$ \begin{array}{r} -3 \\ -3 \\ -3 \\ -2 \\ \end{array} $		Running out of har- bour.
6.	—33 52	154 07	Direct. S. N. N.S. Direct.	$ \begin{vmatrix} -63 & 09.3 \\ -63 & 38.9 \\ -63 & 11.4 \\ -63 & 30.2 \\ -63 & 03.3 \end{vmatrix} $	E. by N. E. by N. E. by N. E. by N.	$+35 \\ +35 \\ +35 \\ +35 \\ +35$		$\left. \begin{array}{c} -62 \ 47 \end{array} \right62 \ 47$	Much motion.
7.	-33 51	157 18	Direct. Direct. S. N. N.S.	$ \begin{array}{c cccc} -03 & 03 & 3 \\ -62 & 47 & 0 \\ -62 & 43 & 3 \\ -62 & 35 & 7 \\ -62 & 31 & 5 \end{array} $	E. by N.	+35 +35 +35 +35 +35		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Much motion.
8.	-33 27	160 43	Direct. Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by N. E. by N. E. by N.	+35 +35 +35 +35		$ \begin{vmatrix} 1 \\ -61 & 30 & -61 & 30 \end{vmatrix} $	
9.	-33 38	163 42	N.S. Direct. Direct. S. N.	$ \begin{array}{c cccc} -62 & 13.7 \\ -62 & 02.0 \\ -61 & 02.5 \\ -61 & 31.5 \\ 61 & 14.6 \end{array} $	E. by N. E. by N. E.	$\begin{vmatrix} +35 \\ +35 \\ +26 \\ +26 \\ +26 \end{vmatrix}$		$ \begin{vmatrix} $	
10.	-33 38	166 28	N.S. Direct. Direct. S.	$ \begin{array}{c cccc} -61 & 14.6 \\ -61 & 18.4 \\ -61 & 04.0 \\ -61 & 11.7 \\ -61 & 06.7 \end{array} $	E. E. by N. N.E.	$\begin{vmatrix} +26 \\ +26 \\ +35 \\ +56 \\ +56 \end{vmatrix}$			
11.	-33 22	167 40	N. N.S. Direct. Direct.	$ \begin{vmatrix} -60 & 45.7 \\ -61 & 03.9 \\ -60 & 33.2 \\ -60 & 12.3 \end{vmatrix} $	N.E. N.E. E. E. by N.	$ \begin{array}{r} +56 \\ +56 \\ +26 \\ +35 \end{array} $	-1 -1 -1 -1	$\left.\begin{array}{c} -60 & 06 \\ -60 & 08 \end{array}\right\} -60 & 07$	
		,	S. N. N.S. Direct.	$ \begin{vmatrix} -60 & 22 & 3 \\ -60 & 06 & 9 \\ -60 & 15 & 0 \\ -60 & 11 & 0 \end{vmatrix} $	E. by N. E. by N. E. by N.	$+35 \\ +35 \\ +35 \\ +35$	$ \begin{array}{c c} -1 \\ -1 \\ -1 \\ -1 \end{array} $		
12.	-32 58	169 20	Direct. S. N. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E. E.N.E. E.N.E.	$ \begin{array}{r} +43 \\ +43 \\ +43 \\ +43 \end{array} $	$ \begin{array}{r} -1 \\ -1 \\ -1 \\ -1 \end{array} $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
		Table 1	Direct.	$-59 \ 49.1$	E.N.E.	+43	-1	J	

^{*} Observed on shore; $\begin{cases} \text{Direct.} - \mathring{6}3 \ \, \acute{5}3 \cdot 3 \\ \text{S.} \quad -63 \ \, 44 \cdot 8 \\ \text{N.} \quad -63 \ \, 33 \cdot 1 \\ \text{N.S.} \quad -63 \ \, 38 \cdot 5 \end{cases}$

[†] Observed on shore; $\left. \right\}$ Direct. -63° 51 7 face west.

				Observed		Correc	tions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Ang 13	_3°2 1′2	170 97	Direct.	-58 47·3	s.e. by e.	_1 ₂		٠, ، ، ،	
145. 10.	02 12	1,0 ~,	S.	-58 30.2	s.E. by E.	-12	Ö		•
			Ň.	-58 09.7	s.E. by E.	-12	0	>-58 33 -58 33 Much	h motion.
			N.S.	-57 55.2	s.E. by E.	-12	0		
14.	-33 27	171 21	Direct.	-57 30.0	s.e. by E.	-12	. +1	i i	
	-33 55		Direct.	-5849.5	E. 1 S.	+20	. 0	1	
			S.	-59 03.7	$E \cdot \frac{1}{2} S \cdot$	+20	0		
			N.	-59 02.9	E. 1 S.	+20	0	-58 24 -58 24 A he	nd awall
	1.		N.S.	-5859.8	E. $\frac{1}{2}$ S.	+20	0	5-38 24 -38 24 A ne	au swen.
			Direct.	-5842.5	E. 1 S.	+20	0		
`16	-34 00		Direct.	$-57 ext{ } 46.5$	s.e. by E. $\frac{1}{2}$ E.		+1		
16.			Direct.	-58 49.3	E.S.E.	+ 4	0	IJ	
17.	-34 29	173 36	Direct.	-58 26.0	E.S.E.	+ 4	0)	
	-		S.	-58 42.5	E.S.E.	+ 4	0		
			N.	-58 02.7	E.S.E.	+ 4	0	-58 26 -58 26 Muc	h motion.
			N.S.	-58 42.0	E.S.E.	+ 4	0		
			Direct.	-58 17.0	E.S.E.	+ 4	0		
20	D .		Direct.	-58 50.8	E.S.E.	+ 4	0	IJ l	
23		Islands.	Direct.	-59 26.4		1			
	-35 16	174 00	S.	-59 34.5					
			N.	-59 29.1	111			*	
			N.S.	-59 22.6	Observed		,	-59 29 -59 29	
Oct. 27			Direct.	-59 28.2*		•••••	— 1	-59 29 -59 29	
Oct. 27	1	- ×	Direct. S.	-59 2801 $-59 432$					
			N.	$-59 \ 31.9$					
		- 1	N.S.	-59 26.2					
			Direct.	-59 28.3	. [2				
20	Ata	nchor.	Direct.	$-60 \ 17.1$	N.W. $\frac{1}{2}$ N.	+54	-1		
,]	1	S.	-61 03.1	$N \cdot W \cdot \frac{1}{2} N \cdot$	+54		50.40	
			Direct.	-58 31.7	s.	-57	0	>−59 49	
			S.	-59 05.6	s.	-57	0		
Nov. 23	-35 15	174 39	Direct.	-59 25.0	E.S.E.	+1	-1	-59 25 >-59 28 Nov	. 23, running
			Direct.	$-59 \ 37.7$	E. by s.	+15	-1	al	ong the land.
			Direct.	-59 30.7	E. by s.	+15	-1		
			S.	-59 23.8	E. by s.	+15	-1	>-59 11	
			N.	-59 11.7	E. by s.	+15	-1		
			N.S.	-59 22.3	E. by s.	+15	-1		
24	-36 27	177 34	Direct.	-59 50.0	E.S.E.	0			
			Direct.	-59 562	E.S.E.	0	-		
			S.	-59 48.2	E.S.E.	0	-1	> -59 54 -59 54	
			N.	$-59 \ 48.2$	E.S.E.	0	-1		
	90.7	150	N.S.	$-60\ 03.2$	E.S.E.	0		K /	
25	-38 17	179 51	Direct.	-59 55.3	s.E. by s.	-34	-1		
			S.	-59 34.4	s.e. by s.	-34	-1		
			N.	-60 02.2	s.E. by s.	-34			
	*	-	N.S.	-60 14.7	s.E. by s.	-34			
		-1-	Direct.	-59 57.2	s.E. by s.	-34			
	1		Direct.	$-60\ 19.5$	S.E.	-23	-1	$-60 \ 43$	

					1	Corre	ctions.		
7047			Method	Observed Inclination.	Direction of			True Inclination.	D 1
1841.	Lat.	Long.	employed.	Face east.	ship's head.	Ship's attraction.	Index.	True Incimation.	Remarks.
N 05	-3854	181 12	Direct.	-61 13·0	T C T	ó	_ź	-61 157 ° '	*
Nov. 25. 26.	-38 34 $-39 01$		Direct.	-61 27.8	E.S.E. E. by s.	+14	$-\frac{z}{-2}$	7 -01 13	
~0.	0,01	10% 1%	S.	-61 04.7	E. by s.	+14	-1		
			N.	-61 43.4	E. by s.	+14	-2	02 20 1	A heavy sea and very much motion.
			N.S.	-61 29.7	E. by s.	+14	-2	>-61 34	much monon,
2	00 10	100 10	Direct.	-61 30.4	E. by s.	$+14 \\ -50$	-2	7	
27.	-39 18	182 58	Direct. S.	$ \begin{array}{r rrrr} -61 & 02.9 \\ -61 & 01.5 \end{array} $	S. S.	$-50 \\ -50$	$-1 \\ -1$		*
			N.	$-61 \ 16.4$	s.	-50	-2	>-61 57	
		0,0	N.S.	-61 11.1	s.	-50	-1	1	
			Direct.	-60 59.6	s.	-50	1	J	
28.	-40 47	183 03	Direct.	-62 03.3	s.e. by e.	-10	-2	· .	
			S.	$-62\ 35.5$	s.E. by E.	10	-2	>-62 21)	
	7		N.	-61 59.9	s.e. by e.	-10	$-2 \\ -2$	$ \left\{ -62 \ 21 \right $	
			N.S. Direct.	$\begin{vmatrix} -61 & 59.8 \\ -61 & 29.8 \end{vmatrix}$	s.e. by e.	$\begin{vmatrix} -10 \\ -49 \end{vmatrix}$	$-\frac{2}{-2}$	$\begin{bmatrix} 1 & -62 & 21 \end{bmatrix}$	2-
29.	-41 49	183 41	Direct.	-62 29.9	s. by E.	-49	-2	7	N.
29.	71 73	100 41	S.	$-62 \ 34.4$	s. by E.	-49	_2		V
			N.	-62 43.2	s. by E.	-49	_2	$> -63 \ 28 \ -63 \ 28$	
		(2)	N.S.	-62 47.0	s. by E.	-49	_2	. .	
			Direct.	-62 32.0	s. by E.	-49	-2	Ų	
30.	-43 32	183 03	Direct.	-63 38.3	S. ½ W.	$ -52 \\ -52$	$-3 \\ -3$	9 =	
			S. N.	-64 16.6 $-63 48.1$	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W.	$-52 \\ -52$	-3	-64 44 -64 44	
	100		N.S.	$-63 \ 43.9$	$S \cdot \frac{1}{2} W \cdot$ $S \cdot \frac{1}{2} W \cdot$	-52		-01 11 -01 11	
	- 1		Direct.	-63 38.9	$s.\frac{1}{2}w.$	_52	_3		
Dec. 1.	-45 40	183 20	Direct.	-66 08.5	s.E. by E.	-15	_4	ň	
			S.	-66 34.2	s.e. by E.	_15	_4		
	<		N.	$-66\ 03.2$	s.e. by e.	-15	_4	> -66 35 -66 35	A head sea.
	-22-		N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by e.	-15 -15	$\begin{vmatrix} -4 \\ -4 \end{vmatrix}$		
2.	_47 19	184 40	Direct.	$-67 \ 41.2$	s.e. by $E \cdot \frac{1}{2}E$		-5	K	
2.	-4/ 13	104 40	S.	-67 34.0	s.E. by E. $\frac{1}{2}$ E		_5		rd.
			N.	-67 34.0	s.e. by $E \cdot \frac{1}{2}E$	-11	_5	>-67 56 -67 56	A head swell.
		÷	N.S.	-67 32.5	s.e. by $E \cdot \frac{1}{2} E$	_11	_5		Maria de la compania del compania del compania de la compania del la compania de la compania del la compania de la compania del la comp
l			Direct.	-67 56.0	s.e. by $E \cdot \frac{1}{2}E$		-5	J Co. 013	
3.	-48 43	186 30	Direct.	-6851.5	E.S.E.	$\begin{vmatrix} -5 \\ -20 \end{vmatrix}$		$-69 \ 01$	
			Direct. S.	-68 46.1 $-68 38.6$	s.e. by e.	-20		-69 08 60 05	7
			N.	$-68 \ 43.6$	s.e. by E.	1		$\left.\right\}^{-09} \left.\right)^{08} \left.\right\}^{-69} \left.\right)^{05}$	
			N.S.	-68 41.6	E.S.E.	- 5	-5	-68 52	ALCOHOL:
			Direct.	-68 49.7	s.e. by E.	-20	-5		
4.	-49 20	187 41	Direct.	-69 32.4	E. by s.	+ 6	-6		
			S.	$-70\ 10.2$	E. by s.	+ 6 + 6			
			N.	-69 48·6	E. by s.	+ 6 + 6		1	
l		-	N.S. Direct.	-69 50.0 $-69 24.4$	E. by s.	+ 6		$>-69 \ 41 \ -69 \ 41$	
5.	-49 2	189 13	Direct.	-69 36.0	E. by s.	+ 6		03 .2	
1	13 2	103 10	S.	$-69 \ 47.2$	E. by s.	+ 6 + 6 + 6 + 6 + 6 + 6 + 6 + 6	-6		
1			N.	-69 32.9	E. by s.	+ 6		4	
			N.S.	-69 28.2	E. by s.	+ 6		7	
6.	-500	0 191 00	Direct.	-69 17.5	E. by s.	+ 6 + 6			
1		*	S. N.	-69 51.7 $-69 37.0$	E. by s. E. by s.	+ 6		>-69 34)	
1			N. N.S.	-69 38.2	E. by s.	+ 6			* 4
1.	-50 4	8 192 20	Direct.	-69 28.5		+6		} −69 43	8
	00 1	1 - 3 ~ ~ 0	1 2	1	1	1			!

THE RESIDENCE OF THE PARTY OF T				Observed		Correct	tions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 7.	$-\mathring{50}$ 48	192 20	Direct. S. N.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by e. s.e. by e. s.e. by e.		$-6 \\ -6 \\ -6$	$\left. \right\} = -69 58 \left. \right\} = -69 4$	43
8.	-51 34	194 29	N.S. Direct. Direct. S. N.	$ \begin{vmatrix} -69 & 04.5 \\ -69 & 17.0 \\ -70 & 04.1 \\ -70 & 33.6 \\ -70 & 12.3 \end{vmatrix} $	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. E. by s. E. by s. E. by s.		$ \begin{array}{r} -5 \\ -6 \\ -6 \\ -6 \\ -6 \end{array} $	$ \begin{cases} -69 & 42 \\ -70 & 10 \\ \end{array} $	*
9.	-52 02	197 53	N.S. Direct. Direct. S. N.	$ \begin{vmatrix} -69 & 53.8 \\ -70 & 06.0 \\ -70 & 19.0 \\ -70 & 49.0 \\ -70 & 29.1 \end{vmatrix} $	E. by s.	+ 6 + 6 + 6 + 6 + 6	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \\ -6 \end{array} $	$ \begin{vmatrix} \\ \\ \\ \\ -70 & 32 \end{vmatrix} -70 & 9 $	21
10.	53 01	202 11	N.S. Direct. Direct. Direct. S.	$\begin{array}{c cccc} -70 & 11.2 \\ -70 & 17.0 \\ -70 & 18.0 \\ -71 & 08.0 \\ -71 & 26.2 \end{array}$	E. by s. E. by s. E. by s. E. ½ N. E. ½ N.	$\begin{vmatrix} + & 6 \\ + & 6 \\ + & 6 \\ + & 25 \\ + & 25 \end{vmatrix}$	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \\ -7 \end{array} $		
11.	-52 48	203 50	N. N.S. Direct. S. N.	-71 13·0 -71 09·7 -71 05·0 -70 35·9 -70 53·5 -70 54·6	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E.	$ \begin{array}{r} +25 \\ +25 \\ +25 \\ +19 \\ +19 \\ +19 \\ \end{array} $	$ \begin{array}{r} -7 \\ -6 \\ -6 \\ -6 \\ -6 \\ \end{array} $	$ \begin{vmatrix} -70 & 53 \\ -70 & 35 \end{vmatrix} - 70 $	44 Ship unsteady; much motion.
12.	-53 01	205 08	N.S. Direct. Direct. S. N.	-70 340 -71 11·2 -70 30·4 -69 56·8 -70 11·6 -70 00·7	E. E. E.S.E. E.S.E.	+19 +19 - 6 - 6 - 6	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ \end{array} $		Y
13.	—54 55	209 30	N.S. Direct. Direct. S.	$\begin{array}{c cccc} -69 & 42.3 \\ -69 & 56.5 \\ -70 & 01.5 \\ -70 & 21.0 \\ -70 & 55.7 \end{array}$	E.S.E. E.S.E. S.E. by E. \frac{1}{2} E. S.E. by E. \frac{1}{2} E.	$ \begin{vmatrix} -6 \\ -6 \\ -14 \\ -14 \end{vmatrix} $	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \end{array} $	\rightarrow -70 10 -70 1	0
	55 08	210 04	N. N.S. Direct. Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by $E.\frac{1}{2}E.$ s.e. by $E.\frac{1}{2}E.$ s.e. by $E.\frac{1}{2}E.$ s.e. by $E.\frac{1}{2}E.$ s.e. by $E.\frac{1}{2}E.$ s.e. by $E.\frac{1}{2}E.$	$ \begin{vmatrix} -14 \\ -14 \\ -14 \\ -14 $	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ -6 \\ \end{array} $	$\begin{vmatrix} -70 & 54 \\ -71 & 13 \end{vmatrix} -70 & 8$	58
	-55 20	210 28	N.S. Direct. Direct. S. N.	$ \begin{vmatrix} -71 & 03.0 \\ -70 & 27.5 \\ -70 & 35.5 \\ -71 & 13.5 \\ -70 & 48.7 \end{vmatrix} $	s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$	-14 -14 -15 -15 -15	$ \begin{array}{r} -6 \\ -6 \\ -6 \\ -7 \\ -6 \end{array} $	} } }-71 11]	
14.	-56 20	211 52	N.S. Direct. Direct. S N. N.S.	$ \begin{vmatrix} -70 & 53.0 \\ -70 & 39.0 \\ -70 & 38.0 \\ -71 & 23.9 \\ -71 & 01.3 \\ -70 & 36.2 \end{vmatrix} $	s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$ s.e. by s. s.e. by s. s.e. by s.		$ \begin{array}{r} -6 \\ -6 \\ -7 \\ -6 \\ -6 \\ -6 \end{array} $	$\left\{\begin{array}{c} \\ \\ \\ \end{array}\right\} = 71 46 $	28
			Direct.	$\begin{vmatrix} -70 & 30.2 \\ -70 & 43.0 \end{vmatrix}$	s.E. by s. s.E. by s.	-47 -47	$-6 \\ -6$		

	×			Observed		Correc	ctions.		OPENIER I VINCENTE ENTRE DE LA COMPANIE DE LA COMP
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 14.	$-\overset{\circ}{55} \overset{\circ}{55}$	2 [°] 11 3 [′] 8	Direct. S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s. s.e. by s.	-48 -48	- 6 - 7) , , , , , , , , , , , , , , , , , , ,	-
	,		N. N.S. Direct.	$ \begin{array}{c cccc} -71 & 00.7 \\ -71 & 04.0 \\ -70 & 50.3 \end{array} $	s.e. by s. s.e. by s. s.e. by s.	-48 -48 -48	- 6 - 6 - 6	$-72 ext{ 03}$	
15.	— 56 55	212 34	Direct. S. N.	$\begin{array}{r rrrr} -71 & 09.5 \\ -72 & 36.0 \\ -71 & 18.2 \end{array}$	S.S.E. S.S.E. S.S.E.	$-58 \\ -58 \\ -58$	- 7	$ \begin{array}{c} -72 & 18 \\ -72 & 33 \end{array} $	
	—56 06	212 20	N.S. Direct. Direct.	$ \begin{array}{c cccc} -71 & 14.5 \\ -71 & 07.5 \\ -71 & 37.1 \end{array} $	s.s.e. s.s.e. s.e. by s.	-58 -58 -48	-7 -6 -7		
			Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E. E.S.E.	- 9 - 9 - 9	- 7 - 7 - 7		
16.	-58 29	213 11	N.S. Direct. Direct.	$ \begin{array}{r rrrr} -71 & 31.0 \\ -71 & 50.0 \\ -72 & 41.5 \end{array} $	E.S.E. E.S.E. S.S.E.	$\begin{bmatrix} -9 \\ -9 \\ -60 \end{bmatrix}$	$ \begin{array}{r} -7 \\ -7 \\ -7 \end{array} $		
			S. N. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.S.E. S.S.E. S.S.E.		- 7	$\left.\begin{array}{c} -73 & 40 \end{array}\right]$	
	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.S.E. S.S.E. S.S.E.	$ \begin{array}{r} -60 \\ -60 \\ -61 \end{array} $	$-7 \\ -7$	$\left.\begin{array}{c} -73 \ 45 \end{array}\right $	
	÷		S. N. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.S.E. S.S.E. S.S.E.		$\begin{bmatrix} -7 \\ -7 \\ -7 \end{bmatrix}$	$\left \begin{array}{c} -73 & 52 \end{array} \right $	
17.	—61 03	213 57	Direct. Direct. S.	$ \begin{array}{c cccc} -72 & 47.7 \\ -74 & 02.5 \\ -74 & 27.7 \end{array} $	S.S.E. S.S.E.		$\begin{vmatrix} -7 \\ -8 \\ -8 \\ -8 \end{vmatrix}$		
			N. N.S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.S.E. S.S.E.		- 8 - 8 - 8	75 15	
	-61 37	213 57	Direct. Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.e. s. by e. s. by e. s. by e.		- 8 - 8	$\begin{bmatrix} \\ \\ \\ \\ \\ \end{bmatrix} = 75 47 \end{bmatrix} = 75 32$	
19	60 40	212 53	N.S. Direct. Direct.	$ \begin{array}{rrrrr} -74 & 070 \\ -74 & 25 \cdot 0 \\ -74 & 33 \cdot 0 \\ -75 & 01 \cdot 5 \end{array} $	s. by E. s. by E.	$\begin{vmatrix} -69 \\ -69 \\ -72 \end{vmatrix}$	- 8 - 8		
, 10.	-02 40	212 00	S. N. N.S.	$ \begin{bmatrix} -75 & 20 \cdot 3 \\ -75 & 10 \cdot 5 \\ -75 & 47 \cdot 0 \end{bmatrix} $	S. S.	$\begin{vmatrix} -72 \\ -72 \\ -72 \\ -72 \end{vmatrix}$	$\begin{bmatrix} - & 9 \\ - & 8 \end{bmatrix}$	\\ \-76 38\\\	,
×	*		Direct. Direct. Direct.	$ \begin{vmatrix} -75 & 07.8 \\ -75 & 10.0 \\ -75 & 18 & 0 \end{vmatrix} $	s. by w. s. by w.	$\begin{vmatrix} -72 \\ -70 \\ -70 \end{vmatrix}$	- 8 - 8 - 9	$\left \begin{array}{c} \\ \\ \\ \end{array} \right = 76 \ 32 \right\rangle = 76 \ 36$	×
19.	-63 23	210 02	Direct. S. N.	$ \begin{vmatrix} -76 & 17.0 \\ -76 & 23.3 \\ -75 & 54.0 \end{vmatrix} $	s.s.w. s.s.w.		- 9 - 9 - 9	$ \begin{vmatrix} -77 & 26 & -77 & 26 \end{vmatrix} $	
	_63 23	210 02	N.S. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.w.	$\begin{vmatrix} -63 \\ -63 \end{vmatrix}$	$\begin{vmatrix} -9 \\ -9 \\ -9 \end{vmatrix}$		· *
		*	S. N. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Observed on Ice.		$\begin{vmatrix} -10 \\ -9 \\ -9 \end{vmatrix}$		

^{*} Observed on ice; face west. Direct. -78° 20'-3.

			35.3	Observed		Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Dec. 19.	-63 23	210 Ó2	Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. by w. w.s.w.			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
20.	-63 47	208 26	Direct. Direct. S.	$ \begin{array}{r rrr} -76 & 31.2 \\ -76 & 26.6 \\ -77 & 23.7 \end{array} $	s.w. by s. s. by w. s. by w.		$\begin{vmatrix} -9 \\ -9 \\ -10 \end{vmatrix}$	$\begin{bmatrix} -77 & 35 \end{bmatrix}$	
21.	-64 38	206 53	N. N.S. Direct. Direct. S. N.	$\begin{array}{r} -76 & 03.0 \\ -76 & 36.6 \\ -76 & 33.7 \\ -76 & 42.5 \\ -77 & 34.8 \\ -76 & 39.4 \end{array}$	s. by w. s. by w. s.s.w. s. s. s.		- 9 - 9 - 9 - 10 - 9	$ \begin{vmatrix} -77 & 58 \\ -77 & 46 \end{vmatrix} -77 & 57 \\ -78 & 32 \end{vmatrix} $	
	-64 50	206 37	N.S. Direct. Direct. Direct. Direct.	$\begin{array}{rrrr} -76 & 49.5 \\ -76 & 54.0 \\ -77 & 02.0 \\ -76 & 58.0 \\ -77 & 13.3 \end{array}$	s. by w. s. by w. s. by E. s. s.		- 9 - 9 - 9 - 9	$ \begin{vmatrix} -78 & 09 \\ -78 & 23 \\ -78 & 21 \\ -78 & 27 \end{vmatrix} -78 & 20$	*
	-64 53	206 30	Direct. S. N. N.S.	$ \begin{array}{rrrrr} $	s. by w. s. by w. s. by w. s. by w.		$ \begin{array}{r} -10 \\ -10 \\ -10 \\ -10 \end{array} $	78 55	
22.	-65 30	205 41	Direct. Direct. Direct. S.	-77 13·1 -77 37·4 -77 37·4 -78 00·3	s. s. s. s. s.			$\begin{bmatrix} -78 & 37 \\ -79 & 06 \end{bmatrix} -78 & 57$	
23.	65 59	204 16	N. N.S. Direct. S. Direct.	$\begin{array}{c cccc} -77 & 47.2 \\ -77 & 27.6 \\ -77 & 38.0 \\ -79 & 50.3 \\ -80 & 53.5 \\ -78 & 04.0 \end{array}$	s. s. s. E.N.E. E.N.E. s. by w.			$igg\} - 79 \ 53 igg]$	
24.	65 57	203 53	S. N. Direct. S. N. N.S. Direct. Direct.	-79 32·3 -78 11·2 -77 53·0 -78 44·7 -78 06·5 -77 51·8 -78 30·4 -80 25·6	s. by w. s. by w. s.	$egin{array}{c} -73 \\ -73 \\ -75 \\ -75 \\ -75 \\ -75 \\ -30 \\ +74 \\ \end{array}$	$ \begin{vmatrix} -11 \\ -10 \\ -10 \\ -10 \\ -10 \\ -10 \\ -11 \\ -11 \\ -11 \\ -11 \\ -11 \\ -11 \\ -11 $	$\begin{bmatrix} -79 & 10 \\ -79 & 10 \\ -79 & 23 \end{bmatrix}$	Fast to a piece of ice.
		×	Direct. Direct. Direct. Direct. Direct.	-80 11·7 -79 49·2 -80 27·2 -80 01·6 -79 16·6	N.E. by N. N.W. ½ W. N. N.W. w. by N.	+67 +57 +76 +60 +28		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	On the 24th lying becalmed along- side pieces of ice.
	-65 58	203 51	Direct. Direct. S. N. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. by s. s.w. by s. s.w. by s.	$\begin{vmatrix} +40 \\ -65 \\ -57 \\ -57 \\ -57 \end{vmatrix}$	-10	$ \begin{vmatrix} -79 & 04 \\ -79 & 29 \\ \\ -79 & 47 \end{vmatrix} $	
25.	-66 00	203 46	Direct. Direct. S. N. Direct.	$\begin{array}{c cccc} -78 & 20 \cdot 1 \\ -79 & 38 \cdot 5 \\ -80 & 52 \cdot 7 \\ -79 & 46 \cdot 8 \\ -79 & 39 \cdot 7 \end{array}$	S.W. E. E. E.	$\begin{vmatrix} -45 \\ +14 \\ +14 \\ +14 \end{vmatrix}$	$-11 \\ -11$		
			Direct. Direct.	$ \begin{vmatrix} -80 & 29.6 \\ -79 & 45.6 \end{vmatrix} $	N.W. E. by N.	$+60 \\ +28$		$\begin{bmatrix} -79 & 54 \\ -79 & 41 \\ -79 & 53 \end{bmatrix}$	

			35.43	Observed	D: :: :	Corre	ctions.	·	
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 26.	-66 íí	203 36	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by e.	$-30 \\ -30$	_10 _11]	
			N.	-79 16·2	s.e. by E.	-30	-11	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
			Direct. Direct.	$\begin{bmatrix} -79 & 02 \cdot 1 \\ -79 & 59 \cdot 2 \end{bmatrix}$	s.e. by e.	$-30 \\ +60$	$-10 \\ -11$	1	
			S.	-79 39.2 $-81 36.5$	N.W.	+60	-12	$ -80 \ 11 $	
27.	-66 16	203 31	Direct.	-79 51.5	E.	+14	-11	$-79 \ 48$	
90	CC 20	202 22	Direct.	-79 48.5	E. 1/2 N.	$+21 \\ +76$	-11_{10}	$\begin{bmatrix} -79 & 39 \end{bmatrix}$	
28.	-66 20	203 22	Direct. Direct.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	N. N.	$+76 \\ +76$	$-12 \\ -11$	$ -80 \ 05 $	4.5
29.	-6624	203 51	Direct.	$-80 \ 43.5$	N.E.	+60	-11	$\left \frac{1}{2} - 80 14 \right $	
			S.	-81 22.4	N.E.	+60	-12		
30	-66 31	203 07	Direct. Direct.	-79 55.6	Е.	+14	-11	$\begin{bmatrix} -79 & 53 \\ -79 & 38 \end{bmatrix}$	
50.	-00 31	203 07	Direct.	$ \begin{array}{r rrr} -80 & 39.2 \\ -80 & 57.8 \end{array} $	N.N.E. N.	$^{+72}_{+76}$	-11	$\begin{bmatrix} -79 & 58 \\ -79 & 53 \end{bmatrix}$	
			Direct.	-79 05.4	s.w.	-45	-10	-80 00	
0.5	20		Direct.	$-80\ 39.1$	n.w. by w.	+55	-11	-79 55	
31.	$-66 \ 32$	203 33	Direct. Direct.	-78 51.6	s.w. by s.	$-57 \\ -69$	$-10 \\ -10$	-79 59 70 40	
1842.			Direct.	-78 30·1	s. by w. $\frac{1}{2}$ w.	-09	-10	$\begin{bmatrix} -79 & 49 \end{bmatrix}$	
Jan. 1.	-66 32	203 32	Direct.	-78 23.9	S.S.E.	-65	-10		
			S. N.	-78 47·5	S.S.E.	-65	$-10 \\ -10$	 -79 48 	
			N.S.	$\begin{vmatrix} -78 & 39 \cdot 1 \\ -78 & 29 \cdot 0 \end{vmatrix}$	S.S.E.	$-65 \\ -65$	-10	79 40	
			Direct.	-78 24·8	S.S.E.	-65	-10^{-10}) (Fr	st to the same
3.	-66 35	203 29	Direct.	-80 56.0	N. by w. $\frac{1}{2}$ w.	+73	-11		piece of ice as Terror, distant
			S.	$-81 \ 30.1$	N. by w. $\frac{1}{2}$ w.		-12		25 fathoms from her.
			N. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by w. $\frac{1}{2}$ w. n. by w. $\frac{1}{2}$ w.	+73 + 73	-11 -11	}−80 07	ner.
			Direct.	-81 05.3	N. by w. $\frac{1}{2}$ w.		-11		
4.	-66 34	203 51	Direct.	$-79 \ 01.8$	s.e. by E.	-30		-79 42	
6	CC AC	204.04	Direct.	-78 25.4	s. by E.	-73		$\begin{bmatrix} -79 & 48 \end{bmatrix}$	
0.	-66 06	204 24	Direct. S.	$\begin{vmatrix} -78 & 07.2 \\ -78 & 45.8 \end{vmatrix}$	s. s.	$-75 \\ -75$	$-10 \\ -10$		
			Ň.	-78 16·1	s.	-75	-10	70.00	
			N.S.	-77 58·2	S.	-75	-10	├ ─79 39	
,,	CC 10	204 10	Direct.	-78 06.1	s.	-75			
7.	-66 13	204 19	Direct. Direct.	$\begin{vmatrix} -78 & 11.3 \\ -80 & 04.6 \end{vmatrix}$	S. N.W.	-75 +60	$-10 \\ -10$	$\begin{bmatrix} \end{bmatrix}_{-80} \begin{bmatrix} 15 \\ -79 \end{bmatrix}$	ng amongst ose ice.
		204 25	Direct.	$-78 \ 13.7$	s. by w.	-73	-10	$\begin{bmatrix} -79 & 37 \\ \end{bmatrix}$	
			S.	-78 48.3	s.		-10		
			N.	-78 26.9	s.		-10		
			N.S. Direct.	$ \begin{array}{r rrr} -78 & 02.6 \\ -80 & 11.0 \end{array} $	S. N.W.	-75 + 60	$-10 \\ -10$	$\begin{bmatrix} -79 & 21 \end{bmatrix}$	
8.	-66 14	204 33	Direct.	$-80 \ 35.1$	N.	+76	11	$-79\ 30$	
			Direct.	$-80\ 09.6$	N.E.	+60	-11	-79 21	
			Direct. Direct	-79 31·2	E.	+14		$\begin{bmatrix} -79 & 28 \\ 70 & 48 \end{bmatrix}$	
			Direct.	$\begin{vmatrix} -78 & 47.1 \\ -78 & 13.7 \end{vmatrix}$	S.E.	$-45 \\ -75$	$-10 \\ -10$	$\begin{bmatrix} -79 & 42 \\ -79 & 39 \end{bmatrix}$	
			Direct.	-78 09.7	S.S.E.	-65	-10	-79 25	
*	-66 12	204 33	Direct.	$-80\ 19.2$	N.W.	+60	-11	>-79 34	
			S.	-80 44.6	N.W.	+60	- 11	$-79 \ 41 \left[-79 \ 41 \right]$	
			N. N.S.	$ \begin{vmatrix} -80 & 35.3 \\ -80 & 20.0 \end{vmatrix} $	N.W.	$+60 \\ +60$		-	
			Direct.	-78 09.7	S.S.E.		-10	K	
			S.	-78 21.6	S.S.E.	-65	10	├ -79 34	
			Direct.	-79 35·7	W.	+14	-11	70.24	
			Direct.	-78 53.6	s.w. by w.	-30	-10	$\begin{bmatrix} -79 & 34 \end{bmatrix}$	

				Observed		Correct	tions.			
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True	Inclination.	Remarks.
Jan. 9.	-66 04	204 1'9	Direct. Direct. Direct.	$ \begin{vmatrix} -\mathring{7}8 & 48.7 \\ -79 & 24.0 \\ -78 & 39.5 \end{vmatrix} $	s.w. $\frac{1}{2}$ w. E. by s. s.w.	- 1	$-10 \\ -11 \\ -10$	$-79 \\ -79 \\ -79 \\ -79$	36	
10.	—65 59	204 12	Direct. S. N. N.S. Direct. S.	-78 50·8 -79 41·0 -78 40·9 -78 47·0 -79 32·0 -79 45·4	s.w. by w.	$ \begin{array}{r} -30 \\ -30 \\ -30 \\ -30 \\ +14 \end{array} $	-10 -11 -10 -10 -11 -11		41 \\ \> -79 38	
		203 44	Direct. Direct.	$ \begin{array}{r rrr} -80 & 18.8 \\ -78 & 19.8 \end{array} $	n.e. by e.	+55	$-11 \\ -10$	$\begin{bmatrix} -79 \\ -79 \end{bmatrix}$		
		203 32	Direct. Direct.	-78 25·0 -79 00·8 -78 26·9	S.W. S.W. S.W. $\frac{1}{2}$ S.	-45 -51	$ \begin{array}{r} -10 \\ -10 \\ -10 \end{array} $	$\left. \begin{array}{c} -79 \\ -79 \end{array} \right.$	38 28	
13.	-66 11 66 10	203 03 203 05	Direct. Direct. Direct.		s.w. $\frac{3}{4}$ w. s.w. by w. s.s.e.	-30	$-10 \\ -10 \\ -10$	$\begin{bmatrix} -79 \\ -79 \end{bmatrix}$		
	-00 12	203 03	S. N. N.S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.S.E. S.S.E. S.S.E. N.N.E.		-10 -10 -10 -10	$\left.\right\}$ -79		~
	·		S. N. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.E. N.N.E. N.N.E.	+72 +72 +72 +72	$ \begin{array}{r} -10 \\ -11 \\ -11 \\ -11 \end{array} $		4	
14.	-66 14	203 09	Direct. Direct. Direct. Direct. Direct.	$ \begin{vmatrix} -80 & 34.2 \\ -78 & 00.9 \\ -80 & 28.4 \end{vmatrix} $	N.N.E. N.E. by E. s. by W.	+55 -73 +60	-11 -10 -11 -10	$\begin{bmatrix} -79 \\ -79 \\ -79 \\ -79 \end{bmatrix}$	$\begin{array}{c c} 24 & -79 & 33 \\ 39 & \end{array}$	•
15. 16.	$-66 02 \\ -65 49$	202 30 202 02	Direct. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. s.w. E.	-45	-10 -11 -11	$ \begin{array}{c c} -79 \\ -79 \\ -79 \end{array} $	23	
			N. N.S. Direct.	$ \begin{vmatrix} -79 & 33.2 \\ -79 & 58.8 \\ -79 & 22.4* \end{vmatrix} $			-11 -11 -11	$\left ight> -79$	47 -79 47	7
19. 21.		201 22 202 40	Direct. Direct. Direct.	$ \begin{vmatrix} -79 & 08.3 \\ -81 & 06.4 \\ -78 & 33.0 \end{vmatrix} $	s.w. by w. n. by e. s. by e.	+74	$-10 \\ -11 \\ -10$	-79 -80	03	
,			S. N. N.S.	-79 08·5 -78 35·4 -78 29·5	s. by E. s. by E. s. by E.	$\begin{vmatrix} -73 \\ -73 \\ -73 \end{vmatrix}$	$-10 \\ -10 \\ -10$	IJ	05	
, zs.	-67 38	204 01	Direct. N. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. N. N. S.	+76 +76 -75	-12 -12 -12 -10	-80	19	
29.	-67 32	203 59	Direct. Direct. S. N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. ½ w. s.s.w. s.s.w. s.s.w.	$ \begin{vmatrix} -65 \\ -65 \\ -65 \end{vmatrix} $	-10 -10 -10 -10	20	$20 > -80 \ 2$	e
			N.S.	-79 01.9	s.s.w.		-10		J	

^{*} Observed on ice, face west Direct. $-80^{\circ} 39' \cdot 2$.

				011	Ŷ	Corre	ctions.		
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Jan. 30.	-67 18	203 39	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.W. $\frac{1}{2}$ S. S.W. $\frac{1}{2}$ S.	$-51 \\ -51$	_ <u>í</u> 1 _11) ° ′ ° ′	
			». N.	$-80 \ 28.3$ $-79 \ 38.7$	$\begin{array}{c} \text{S.w.} \ \frac{1}{2} \ \text{S.} \\ \text{S.w.} \ \frac{1}{2} \ \text{S.} \end{array}$	-51	-11	$-80 \ 47$	
			N.S.	-79 25.5	$s.w. \frac{1}{2} s.$	-51	-11	91.00	- 3
31	-67 21	202 15	Direct. Direct.	$\begin{vmatrix} -79 & 59.3 \\ -79 & 04.4 \end{vmatrix}$	s. by w.	-73 - 45	$-10 \\ -10$	-81 22	
01.	0, 21	202 10	S.	-79 19.5	s.w.	-45	-11	$\left \begin{array}{c} -80 & 02 \\ -80 & 02 \end{array}\right -80 & 26$	
The state of the s	0.00		N.	-79 04.2	s.w.	-45	-10	$\rangle -80 0z$	
and the same of th			N.S.	$-79\ 00.3$	s.w.	-45	-10	1	
Fob 1	-67 11	202 07	Direct. Direct.	$\begin{vmatrix} -79 & 39 \cdot 1 \\ -79 & 48 \cdot 5 \end{vmatrix}$	w.s.w.	-15 $ -15 $	-11	-80 09	
2.		202 07 200 00	Direct.	-79 22.4	S.E.	-45	1	-80 187	
	0, 0,	200 00	Direct.	-79 59·5	s. by w.	-73	i	-81 24	-
			Direct.	-79 32.0	s.s.e. $\frac{1}{2}$ E.	-61	-11	>-80 46	
			S.	-79 49·7	S.S.E. $\frac{1}{2}$ E.	$\begin{vmatrix} -61 \\ -61 \end{vmatrix}$	$-11 \\ -11$	-80 44	
			N N.S.	$\begin{bmatrix} -79 & 30.2 \\ -79 & 23.0 \end{bmatrix}$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	-61	-11	 - 80 44	
			Direct.	$-79 \ 27.3$	S.S.E. ½ E.	-61	-11		
3.	-68 21	200 03	Direct.	-80 01.0	s.e. by s.	-57	-11	1	The state of the s
	,		s.	-79 53.0	s.e. by s.	-57			
			N.	-7950.4	s.e. by s.	-57		$ -81 \ 04 $	Much motion.
			N.S. Direct.	$\begin{vmatrix} -79 & 57 \cdot 1 \\ -79 & 56 \cdot 8 \end{vmatrix}$	s.e. by s.	$\begin{vmatrix} -57 \\ -57 \end{vmatrix}$			
4.	-68 42	199 44	Direct.	-79 58.7	S. $\frac{1}{2}$ E.	-74		K I	
		133 11	S.	-80 17.9	S. ½ E.	-74	-11	}−81 14	a catalogora
			N.	-79 57.9	S. 1/2 E.	-74		├ -81 24	
			N.S.	-79 41·9	S. ½ E.	$\begin{vmatrix} -74 \\ -74 \end{vmatrix}$			
	_68 40	199 41	Direct. Direct.	$\begin{vmatrix} -79 & 59.2 \\ -82 & 12.8 \end{vmatrix}$	S. $\frac{1}{2}$ E. N. by W.	+74		-81 09 J	
5.		196 07	Direct.	-80 53.5	s.w.	-45		-81 00 j	
		195 51	Direct.	$-80 \ 49.0$	s.w. by s.	-57		h l	
			S.	-81 02.2	s.w. by s.	-57	-11	>-81 57>-81 54	
			N. N.S.	$ \begin{vmatrix} -80 & 46.0 \\ -80 & 39.6 \end{vmatrix} $	s.w. by s. s.w. by s.	$\begin{vmatrix} -57 \\ -57 \end{vmatrix}$	-11		
			Direct.	$-80 \ 59.0$ $-81 \ 52.8$	$W. \frac{1}{2} N.$	+22		$\begin{bmatrix} -81 & 43 \end{bmatrix}$	
6.	-6948	192 25	Direct.	-81 08.5	s. by w.	-74	-11	h ,	
			S.	-81 28.9	s. by w.	-74			
4			N.	-81 11·0	s. by w.	-74 - 74		$-82 \ 35 \ -82 \ 35$	1
			N.S. Direct.	$ \begin{vmatrix} -80 & 47.4 \\ -81 & 12.3 \end{vmatrix} $	s. by w.	-74	-12		
7.	-70 05	191 10	Direct.	-81 45.1	s.w.		-12	$-82\ 43$	
,			S.	-81 50.1	s.s.w.	-66			Much motion.
			N.	-81 38.8	s.s.w.	-66			
			N.S. Direct.	$\begin{vmatrix} -81 & 13.2 \\ -81 & 29.8 \end{vmatrix}$	S.S.W.	$\begin{vmatrix} -66 \\ -66 \end{vmatrix}$	$\begin{vmatrix} -12 \\ -12 \end{vmatrix}$		
	-70 17	190 15	Direct.	-81 298 $-81 43.0$	s.s.w.	-66			
		189 00	Direct.	-82 07.0	s.s.w.	-66	-12		
		-	S.	-81 39.2	s.s.w.	-66		1 1	1 D. T
			N.	-81 44.5	s.s.w.	-66 -66		1 (Much motion.
			N.S. Direct.	$ \begin{vmatrix} -81 & 27.0 \\ -82 & 10.2 \end{vmatrix} $	s.s.w.	-66		1 1	
g.	-70 18	186 01	Direct.	$-82 \cdot 10^{\circ}2$ $-81 \cdot 50^{\circ}6$	S.S.W.	-77	-12		
٥.	, , ,		S.	-81 59.7	s.	-77	-12	(2)	
			N.	-81 49.3	S.	-77	-12		3
			N.S.	-81 37·1	s.	$\begin{vmatrix} -77 \\ -77 \end{vmatrix}$	$\begin{vmatrix} -12 \\ -12 \end{vmatrix}$		-
			Direct.	-81 50.0	s.	1-11	-12	ر	

				Observed		Correct	tions.			-
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True	Inclination.	Remarks.
Feb. 9.	$-70\ 39$	185 31	Direct. Direct. S.	$ \begin{vmatrix} -82 & 06 & 3 \\ -82 & 24 & 5 \\ -82 & 50 & 4 \end{vmatrix} $	s. by E. s.E. by s. s.E. by s.	-58	-12 -12 -12	$-\mathring{83}$	$\left.\begin{array}{c} 33\\-83\end{array}\right\}$	35
10.	_70 11	183 50	N. N.S. Direct. Direct. S.	$ \begin{array}{c ccccc} -82 & 14.6 \\ -82 & 17.0 \\ -82 & 23.2 \\ -83 & 23.9 \\ -83 & 21.9 \end{array} $	s.e. by s. s.e. by s. s.e. by s. w. by s. w. by s.	$\begin{bmatrix} -58 \\ -58 \\ 0 \end{bmatrix}$	-12 -12 -13 -13		36)	,
	F 0.04	100.00	N. N.S. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	w. by s. w. by s. w. by s.	0 0 0	-13 -13 -13	J		33 A head swell.
11.		181 50	Direct. Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. s.w. by s. s.w.	$\begin{bmatrix} -58 \\ -47 \end{bmatrix}$	-13 -12 -12	$\begin{bmatrix} -84 \\ -83 \end{bmatrix}$	57	A head swell.
12.	-71 00	180 44	N. N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. s.w. s.e. by s.	$\begin{vmatrix} -47 \\ -58 \end{vmatrix}$	-12 -12 -12	-83		06 A heavy cross sea.
			S. N. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s. s.e. by s.	$\begin{vmatrix} -58 \\ -58 \end{vmatrix}$	-12 -13 -13	-84	18	
13.	-72 46	181 46	Direct. Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by s. s.e. by s. s.e. by s.	$\begin{vmatrix} -59 \\ -59 \end{vmatrix}$	-12 -13 -13	Ĭ	017	
			N.S. Direct. Direct.	$ \begin{array}{r rrrr} -83 & 46.0 \\ -83 & 45.2 \\ -83 & 36.7 \\ -84 & 04.8 \end{array} $	s.e. by s. s.e. by s. s.e. by s.	$\begin{vmatrix} -59 \\ -59 \end{vmatrix}$	-13 -13 -13	-85	-85	04
15.	-73 23 $-74 24$ $-74 56$	177 09	Direct. Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.E. $\frac{1}{2}$ S. S.S.E. $\frac{1}{2}$ E. S.S.E.	$\begin{vmatrix} -53 \\ -63 \end{vmatrix}$	-13 -13 -13 -14	$ \begin{array}{r} -85 \\ -85 \\ -86 \end{array} $	42 06	02 Very much motion.
10.	-71 50	170 00	S. N. N.S.	$ \begin{vmatrix} -85 & 51 \cdot 8 \\ -85 & 20 \cdot 5 \\ -85 & 10 \cdot 0 \end{vmatrix} $	S.S.E. S.S.E. S.S.E.	$\begin{vmatrix} -69 \\ -69 \end{vmatrix}$	-14 -14 -13	-86		52 Very unsteady.
	-75 10	173 08	Direct. Direct. Direct.		s. by E. ½ E. S.E. E.	$\begin{vmatrix} -74 \\ -48 \end{vmatrix}$	-14 -14 -14	$\begin{bmatrix} -86 \\ -87 \end{bmatrix}$	49	J. S. J. Massoury.
	Control of the Contro		N. N. N.S.	$ \begin{array}{r rrr} -87 & 28.5 \\ -87 & 06.9 \\ -86 & 56.4 \end{array} $	E. E. E.	+16 $ +16 $ $ +16 $	$ \begin{array}{r r} -15 \\ -14 \\ -14 \end{array} $	-86	59 —86	59
17.	$-75 53 \\ -76 00$	175 05 175 15	Direct. Direct. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. E.N.E. E.N.E.	$ \begin{array}{r} +16 \\ +42 \\ +42 \\ +42 \end{array} $	-14	Ĭ		
	,		N.S. Direct.	$ \begin{vmatrix} -87 & 26.9 \\ -87 & 06.3 \\ -87 & 07.0 \end{vmatrix} $	E.N.E. E.N.E.	+42 +42	_15	-86	44 —86	44
18.	-76 58	181 03	Direct. S. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.N.E. E.N.E.	+42 + 42	-15	$\left.\right\rangle$ -86	46 —86	46
			N.S. Direct.	$\begin{bmatrix} -87 & 18.8 \\ -86 & 57.8 \end{bmatrix}$	E.N.E. E.N.E.	$\begin{vmatrix} +42 \\ +42 \end{vmatrix}$	$-15 \\ -14$			

^{*} This observation differs so widely from the others made on the same day, that, considering the unfavourable state of the weather, I have omitted it in the mean results: possibly the ship's head may have been W. by S. instead of S. by W., in which case the observation would agree well with the others.—E. S.

			Method	Observed	Dimention of	Correc	ctions.				
1842.	Lat.	. Long.	employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True	Inclination.		Remarks.
Feb. 19.	$-\mathring{7}6 \ \acute{42}$	184 09	Direct.	$-87 \ 24.5$	n. by E.	+78	_1'5	, .	() °	,	
1 000 130		101 00	S.	-86 57.7	N. by E.	+78					
			N.	-87 15.6	N. by E.	+78	-15	>-86	07	Δ#	Chin with him or
			N.S.	$-86\ 56.5$	n. by E.	+78	-14		>-80	07	Ship pitching.
			Direct.	-87 21.2	N. by E.	+78	-15	J			
	-7646		Direct.	-87 08 0	N.N.E.	+75	-14	-86			
20.			Direct.	-85 58.3	N.E. ½ E.	+60	-14	-85		18	A head sea and much
21.	-7553		Direct.	-84 24 3	s.w.	-47	-13	-85	24]		motion.
22.	-76 42	194 48	Direct.	-84 03·9	s.e. by s.	-60	-13		1		**
			S. N.	-84 19·6	s.E. by s.	$\begin{bmatrix} -60 \\ -60 \end{bmatrix}$	-13	05	0.5		-
			N.S.	-84 24.0 $-84 10.5$	s.e. by s.	-60	$-13 \\ -13$	-85	>-85	25	A swell from the southward.
			Direct.	-84 040	s.E. by s.	_60	-13		1		South ward.
	-7642	194 10	Direct.	_84 56·5	E.S.E.	-17	-13	-85	26		
	-77 05		Direct.	-84 53.0	E. by s.	0	-13	7	ر ٥٠٠		
-		101 00	S.	—85 36·6	E. by s.	0	-14				
			N.	-85 16·0	E. by s.	0	-14	-85	24 - 85	24	
l			N.S.	-85 13.0	E. by s.	0	-14				
			Direct.	84 55·0	E. by s.	0	-13	j			
23.	-7749	197 24	Direct.	-84 26·5	E. by s.	0	13	-84	40)		
			Direct.	-84 05.3	s.w. by w.	33		-84			
	-78 07		Direct.	-84 40.3	E. $\frac{1}{2}$ S.	+ 8	-13	-84		49	
	-78 07	197 46	Direct.	-84 51.9	w. by n.	+30	-13	-84			
24.	-7655		Direct.	-84 12.0	s.w.	-47		-85	12		
25.	-7450	193 45	Direct.	-84 41.0	. w.	+15	-13				
			S.	-84 57·7	w.	+15	-13	>-84	53		
			N.	-85 13·0	w.	+15	-14		-84	49	
			N.S.	-84 50.0 $-84 50.3$	W.	+15 + 30		J -84	22		
			Direct. Direct.	$-83 \ 27.2$	w. by n. s.s.w.	-68	-13	-84 -84			
26.	-72 46	189 59	Direct.	$-85 \ 15.7$	n.w. by w.	+57	-14	7	4 0)		
20.	12 10	109 09	S.	-85 38·0	N.w. by w.	+57	-14	1 .			
			N.	_85 14.5	n.w. by w.	+57	-14	-84	38 -84	38	
			N.S.	_85 25.5	n.w. by w.	+57	-14				
			Direct.	_85 11.3	n.w. by w.	+57	-13	J			
27.	-7201	187 35	Direct.	-83 38.0	w.s.w.	-16	-13	ň			
			S.	$-83\ 48.2$	w.s.w.	-16	-13				
			N.	_83 44.1	w.s.w.	-16	-13	>-84	10 -84	10	
			N.S.	-83 44·2	w.s.w.	-16	-13				
		704 70	Direct.	-83 40.8	w.s.w.	-16	-13	Ŋ			
28.	-71 08	184 59	Direct.	-84 05.5	w.	+15					and the same of th
			S.	_84 18·4	w.	+15	-13				
.			N.	-84 06·5	w.	$ +15 \\ +15$	-13 -13	>-84	04 - 84	04	
			N.S.	$\begin{vmatrix} -84 & 10.4 \\ -84 & 04.5 \end{vmatrix}$	w.	$+15 \\ +15$					
			Direct. Direct.	_83 48·6	w. w.	+15 + 15	-13				
Mar. 1.	-69 52	180 04	Direct.	$-84 \ 35.5$	w. by N.	+33	i .	K			
man. 1.	03 02	100 01	S.	-83 59.2	w. by N.	+33		 			
		1	N.	-83 45.0	w. by N.	+33	-13	 	34 - 83	34	
and the second			N.S.	-83 39.7	w. by N.	+33	-13				
		*	Direct.	-83 32.0	w. by N.	+33					
	-6944	179 53	Direct.	-84 59.1	n. by E.	+93	_13	ń			
			S.	-84 36·6	n. by E.	+93	-13	l Í			
- 8			N.	-84 54.2	n. by E.	+93	-13	>-83	31 - 83	31	A northerly swell.
			N.S.	-84 52.0	n. by E.	+ 93	-13				10
			Direct.	-84 54.0	n. by E.	+93	_13	IJ			

						Correc	ctions.		***************************************	
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True	e Inclination.	Remarks.
M	80.4	100 07	D: /	$-83 \ 43.3$			1/0	_ 。	/_ 0 /	-
Mar. 2.	-68 04	183 25	Direct. S.	$-83 \ 43.3$ $-83 \ 54.0$	N.N.E.	+90 +90	$\begin{vmatrix} -13 \\ -13 \end{vmatrix}$			
	0		Ň.	$-83\ 50.2$	N.N.E.	+90	-13	-82	2 28	'
			N.S.	$-83\ 38.2$	N.N.E.	+90	-13			
			Direct.	$-83\ 37.5$	N.N.E.	+90	-13]]	>-82 1	9
			Direct.	$-83\ 03.2$	n.e. by n.	+82	-12	ñ	7-8z 1	0
			S.	$-83 \ 14.4$	n.e. by n.	+82	-13	1 1		
			N.	-83 12.7	N.E. by N.	+82		>-81	57	-
			N.S. Direct.	-83 04.7	N.E. by N.	+82 + 82	$\begin{vmatrix} -12 \\ -12 \end{vmatrix}$		ı	
3.	-67 32	185 09	Direct.	$ \begin{array}{r rrrr} -82 & 59.0 \\ -82 & 31.0 \end{array} $	n.e. by n.	+51	$-12 \\ -12$	K	\exists	
Ŭ.	0, 02	100 05	S.	$-82\ 41.5$	E.N.E.	+51	-12		-0	
			N.	$-82\ 44.3$	E.N.E.	+51	-12	>-81	56	,
			N.S.	$-82\ 23.6$	E.N.E.	+51	-12	IJ	\rangle -81 5	1
			Direct.	$-82\ 48.7$	n.e. by n.	+81	-12	-81	•	
	-67 28		Direct.	$-82\ 34.8$	N.E.	+74			33	
4. 5.	-67 29 -67 16	188 11 188 10	Direct. Direct.	$ \begin{array}{r rrr} -80 & 39.5 \\ -82 & 05.6 \end{array} $	w.s.w.	-20	-11	1_	1117	A very heavy sea and much motion.
٠.	-07 10	188 10	N.	$-82 \ 03.0$ $-82 \ 37.2$	N. by E.	+91 + 91	$\begin{vmatrix} -12 \\ -12 \end{vmatrix}$	11	91.0	2 A very heavy swell
			N.S.	$-82 \ 29 \ 0$	n. by e.	+91	-12	>-80) 59 $\}$ – 81 0.	from the westward.
			Direct.	-81 59.0	N. by E.	+91	-12			
6.	-65 25	191 48	Direct.	-80 28.3	N. by E.	+89	-11	Ħ		
			N.	$-80 \ 41.9$	N. by E.	+89	-11			
			N.S.	-80 54.6	n. by E.	+89		>-79	9 19 -79 1	9 Much motion.
	0- 00		Direct.	-80 31·8	N. by E.	+89				
7		192 21	Direct.	-80 24.0	N. by E.	+89	-11	K		
1.	-03 30	194 22	Direct.	$\begin{vmatrix} -79 & 37.0 \\ -79 & 31.3 \end{vmatrix}$	N. by E.	+88 +88	-11 $ -11$			
1			S.	$-79 \ 44.5$	n. by E.	+88	-11			_
1		The state of the s	N.	-79 08.1	N. by E.	+88	-10		3 11 -78 1	1
			N.S.	-79 20.2	N. by E.	+88	-11	1 1		
			Direct.	-79 27.4	n. by E.	+88				
8.	-62 16	196 10	Direct.	$-78 \ 35.1$	N. by E.	+87	-10			
	•		S.	-78 40·4	N. by E.	+87			7 1 7 7 7 7 7 1	-
			N. N.S.	$\begin{vmatrix} -78 & 30.5 \\ -78 & 34.0 \end{vmatrix}$	N. by E.	+87		>-7	7 17 -77 1	7
			Direct.	-78 31.9	n. by E.	+87 + 87 + 87	$\begin{vmatrix} -10 \\ -10 \end{vmatrix}$			
9.	-61 14	198 38	Direct.	-77 33.0	N. by E.	+76	-10			
	Automotive		S.	—78 15.5	N.E. by N.	+76	-10			
	* Colombia		N.	-77 36.7	n.e. by n.	+76	-10	7	$6 \ 34 \ -76 \ 3$	4
	0.0		N.S.	-77 24.7	N.E. by N.	+76	_10			
1		199 11	Direct.	-77 23.8	N.E. by N.	+76	-10			
	-00 50	200 11	Direct. S.	$-76 36.5 \\ -77 19.5$	N.E. by N.	+75 +75	$\begin{vmatrix} -9 \\ -10 \end{vmatrix}$			
		36	N.	$-76 \ 31.7$	N.E. by N.	+75 + 75			$5 \ 33 \ -75 \ 3$	3
			N.S.	-76 09.5	N.E. by N.	+75	$\begin{bmatrix} - & 9 \\ - & 9 \end{bmatrix}$			
			Direct.	-76 34.0	N.E. by N.	+75	$\begin{vmatrix} -9 \\ -9 \\ -9 \\ -9 \\ -9 \end{vmatrix}$			1 1 8
10.		203 55	Direct.	-75 33·0	E.N.E.	+48	-9	-7	4 54	
1	-60 18	204 11	Direct.	-75 23.0	E. by N.	+33	- 9			
I			S.	-76 07.5	E. by N.	+33	- 9		>-75 0	8'A cross sea, ship pitching.
			N. N.S.	-76 18.0 $-75 48.2$	E. by N.	+33	- 9 - 9 - 9		5 11	
			Direct.	-75 48.2 $-75 24.4$	E. by N.	$\begin{vmatrix} +33 \\ +33 \end{vmatrix}$	-9	1 1	٠)	
11.	_60 18	208 29	Direct.	-73 244 $-74 27.0$	E. by N.	+33				Very much motion.
	1	1	1	1	1 25 by IN.	1,00	1 3	1		1,

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	tions.	True Inclina	ation.	Remarks.
Mar. 12.	$-60^{\circ}13^{\circ}$	211 34	Direct.	$-\mathring{7}4 \ \acute{0}6.5$	E. by N.	+33	-8	n ° ′	0 /	
	00 20	, , , , , , , , , , , , , , , , , , ,	S.	-74 23.3	E. by N.	+33	-8			
			N. N.S.	-74 57.0 $-74 57.5$	e. by n. e. by n.	+33 +33	8 8	├ -74 21	-7421	A heavy swell, ship
1			Direct.	-74 18·0	E. by N.	+33	-8			very unsteady.
		212 32	Direct.	-74 02.5	E. by N.	+33	-8	J		
	-60 00		Direct.	$\begin{vmatrix} -73 & 56.0 \\ -73 & 26.6 \end{vmatrix}$	N.E.	+67	-8	-7257		
14.	-59 24	218 28	Direct. S.	$\begin{vmatrix} -73 & 20.0 \\ -74 & 20.7 \end{vmatrix}$	n.e. by e.	+59 +59	$-8 \\ -8$			0
1			N.	-73 57·5	N.E. by E.	+59	-8	72.12		
			N.S.	-73 47.2	N.E. by E.	+59	-8	$-73 \ 13$	-73 30	Very unsteady.
-			Direct.	$-73 \ 35.3$	N.E. by E.	+59	-8			
	50 16	219 30	Direct. Direct.	$\begin{vmatrix} -75 & 17.5 \\ -75 & 10.5 \end{vmatrix}$	n.e. by e.	+59 +59	$-9 \\ -8$	K I		
	-09 10	219 00	S.	-74 54.1	N.E. by E.	+59	-8	$\begin{bmatrix} -74 & 03 \end{bmatrix}$		
1			N.	-74 42.7	n.e. by e.	+ 59	-8	>-/4 03)		
		222 04	N.S.	-74 49·5	n.e. by e.	+59	$-8 \\ -8$	Ŋ		
15.	-5854	222 04	Direct. S.	$\begin{vmatrix} -74 & 32 \cdot 1 \\ -74 & 07 \cdot 2 \end{vmatrix}$	E.N.E.	+48 +48	-8			
		e	N.	-74 26·1	E.N.E.	+48	8	>−73 41		
1			N.S.	-74 11·7	E.N.E.	+48	-8		-73 38	-
	FO FO	000 04	Direct.	$\begin{vmatrix} -74 & 28.8 \\ -73 & 57.5 \end{vmatrix}$	E.N.E. E. by N.	$ +48 \\ +33$	-8 -8	K	-/5 56	
	-58 50	223 24	Direct. Direct.	-73 55.0	E. by N.	+33	-8	$ \} -73 \ 31 $		-
16	-59 00	227 32	Direct.	-73 11.8	E.	+19	-7	Н		
			Direct.	-73 11·0	E.	+19	-7			
	-59 04	228 57	S. N.	$\begin{vmatrix} -72 & 20.2 \\ -73 & 06.0 \end{vmatrix}$	E. E.	+19 + 19	$\begin{vmatrix} -7 \\ -7 \end{vmatrix}$	-72 57	—72 57	-
			N.S.	$-73 \ 54.2$	E.	+19	-8	>-12 31	-12 01	
			Direct.	-73 14.5	E.	+19	-8			
			Direct.	-73 07.3	E.	+19	-7	Ų		-
17	$-59 \ 39$	232 48	Direct. S.	$\begin{vmatrix} -72 & 45.0 \\ -72 & 57.6 \end{vmatrix}$	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	$\begin{vmatrix} +12 \\ +12 \end{vmatrix}$	$\begin{vmatrix} -7 \\ -7 \end{vmatrix}$			
			N.	-73 23.0	E. ½ S.	+12	-7	-72 54	-7254	A great deal of mo-
1			N.S.	$-73\ 10.7$	E. $\frac{1}{2}$ S.	+12	-7			tion.
		200 50	Direct.	-72 39.0	E. $\frac{1}{2}$ S.	+12	-7	R	v.	
	-59 48	233 53	Direct. S.	$\begin{vmatrix} -72 & 24.5 \\ -73 & 00.5 \end{vmatrix}$	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	$\begin{vmatrix} +12 \\ +12 \end{vmatrix}$	$\begin{vmatrix} -7 \\ -7 \end{vmatrix}$			A
1			N.	-73 16·7	$E \cdot \frac{1}{2} S \cdot$	+12	-7	$-72\ 51$	-7251	A great deal of mo- tion.
			N.S.	-73 03·0	E. $\frac{1}{2}$ S.	+12		J ·		
18	-60-16	6 236 11		$\begin{vmatrix} -72 & 35.5 \\ -73 & 02.2 \end{vmatrix}$	E. by s.	+ 4				
			S. N.	$\begin{vmatrix} -73 & 02 & 2 \\ -73 & 21.7 \end{vmatrix}$	E. by s.	+ 4 + 4		-73 00	-70 00	Ship unsteady.
4			N.S.	−72 57·0	E. by s.	+ 4	-7		•	
1			S.	-73 04.2	Е.	+19	-7			
	-60 2	1 237 02		$\begin{vmatrix} -72 & 29.8 \\ -73 & 16.5 \end{vmatrix}$	E.	+19 + 19				
1			S. N.	-73 25.6	E. E.	+19		-72 45	-7245	Ship rolling deeply.
			N.S.	$-73 \ 01.3$	Е.	+19	-7			Ŷ
	C0 -	005 50	Direct.	-72 33·0	E.	+19	$\begin{vmatrix} -7 \\ -7 \end{vmatrix}$	Ä		
	-60 2	0 237 50	Direct.	$\begin{vmatrix} -72 & 57.5 \\ -73 & 24.1 \end{vmatrix}$	E. by N.	+33 + 33	-8	1 1	# 0 *	
			N.	$-73 \ 44.0$	E. by N.	+33	-8	\\ \-\1\z 30	-7244	+
			N.S.	-73 19.0	E. by N.	+33	-8	J.		

				Observed		Corre	ctions.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Mar. 18.	_60 20		Direct.	$-\mathring{73} \stackrel{\circ}{15.0}$	E. by N. ½ N.		-8) ° ′ ° ′	У
	-60 19	238 00	Direct. S. N.		E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	$+40 \\ +40 \\ +40$	$\begin{vmatrix} -7 \\ -7 \\ -8 \end{vmatrix}$	$-72 \ 34 \ -72 \ 44$	ý
19.	_60 02	241 03	N.S. Direct.	$\begin{vmatrix} -73 & 30.6 \\ -72 & 52.5 \end{vmatrix}$	E. by N. $\frac{1}{2}$ N. E.N.E.	+40 +47	$\begin{vmatrix} -8 \\ -7 \end{vmatrix}$		×
	-60 01	241 38	Direct. S. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E. E.N.E. E.N.E.	$\begin{vmatrix} +47 \\ +47 \\ +47 \end{vmatrix}$		$\left \begin{array}{cccccccccccccccccccccccccccccccccccc$	Much motion.
20.	-59 17	245 40	N.S. Direct.	$\begin{array}{ c c c c c } -73 & 28.0 \\ -72 & 08.0 \end{array}$	E.N.E.	+47 + 47	$\begin{vmatrix} -8 \\ -7 \end{vmatrix}$		
		120	S. N. N.S.	$ \begin{vmatrix} -72 & 12.0 \\ -72 & 01.0 \\ -72 & 14.0 \end{vmatrix} $	E.N.E. E.N.E.	+47 + 47 + 47	$\begin{vmatrix} -7 \\ -7 \\ -7 \end{vmatrix}$	-71 29 -71 29	-
21.	-59 15	248 12	Direct. Direct. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E. E. by N. E. by N.	$\begin{vmatrix} +47 \\ +33 \\ +33 \end{vmatrix}$	_7		×
			N.S. Direct.	$ \begin{array}{r rrrr} -71 & 55.9 \\ -72 & 11.2 \\ -71 & 35.2 \end{array} $	E. by N. E. by N.	$+33 \\ +33$	$\begin{bmatrix} -7 \\ -7 \\ -7 \end{bmatrix}$	$-71 \ 26 \ -71 \ 26$	' =
	-59 04 $-58 58$		Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by N. N.E. ½ E. N.E. by E.	$+33 \\ +61 \\ +58 \\ +58$	-7	$\begin{bmatrix} -70 & 59 \end{bmatrix}$	
			S. N. N.S.	$ \begin{array}{r rrrr} -72 & 01 \cdot 2 \\ -71 & 53 \cdot 0 \\ -72 & 14 \cdot 7 \end{array} $	N.E. by E. N.E. by E. N.E. by E.	$+58 \\ +58 \\ +58$	-7 -7 -7 -7	$\left \begin{array}{c} -71 & 08 \\ \end{array} \right -71 & 04$	
22.	$-58 28 \\ -58 29$		Direct. Direct. Direct.	$ \begin{array}{c cccc} -71 & 30.6 \\ -71 & 11.0 \\ -71 & 02.4 \end{array} $	E.N.E. E. by N. E. \frac{1}{2} N.	$+47 \\ +33 \\ +26$	$\begin{vmatrix} -7 \\ -6 \\ -6 \end{vmatrix}$	$\begin{bmatrix} -70 & 51 \\ -70 & 44 \end{bmatrix}$	÷
,			S. N. N.S.	$ \begin{array}{rrrr} -71 & 33.5 \\ -71 & 05.8 \\ -71 & 07.4 \end{array} $	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$^{+26}_{+26}$	$\begin{bmatrix} -7 \\ -6 \\ -6 \end{bmatrix}$	$\left \begin{array}{c} -70 & 52 \\ \end{array} \right = -70 & 50$	A head sea.
23.	-58 35	255 10	Direct. S.	$\begin{vmatrix} -70 & 26.0 \\ -70 & 36.9 \end{vmatrix}$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$^{+26}_{+26}$	$\begin{bmatrix} -6 \\ -6 \end{bmatrix}$) 	e
			N. N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$ \begin{array}{r} +26 \\ +26 \\ +26 \end{array} $	$\begin{bmatrix} -6 \\ -6 \\ -6 \end{bmatrix}$	-70 11 -70 11	
24.	-58 44	257 49	Direct. S. N.	$ \begin{array}{c cccc} -70 & 04.5 \\ -70 & 29.6 \\ -70 & 24.7 \end{array} $	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$\begin{vmatrix} +26 \\ +26 \\ +26 \end{vmatrix}$	$\begin{vmatrix} -6 \\ -6 \\ -6 \end{vmatrix}$	$\begin{bmatrix} \\ \\ \\ \end{bmatrix}$ -69 47 -69 47	
ar	-58 51		N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$ +26 \\ +26$	$\begin{bmatrix} -6 \\ -6 \end{bmatrix}$		
25. 26.	-58 56 -59 01		Direct. Direct. S.	$\begin{vmatrix} -67 & 56.0 \\ -68 & 21.7 \end{vmatrix}$	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	$+40 \\ +40 \\ +40$	$\begin{vmatrix} -5 \\ -5 \\ -5 \end{vmatrix}$	$\left. \begin{array}{cccccccccccccccccccccccccccccccccccc$	A heavy swell.
0			N. N.S. Direct.	$ \begin{vmatrix} -68 & 18.7 \\ -67 & 56.8 \\ -67 & 59.5 \end{vmatrix} $	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	$+40 \\ +40 \\ +40$	$ \begin{bmatrix} -5 \\ -5 \\ -5 \end{bmatrix} $		
27.	-59 02	271 58	Direct. S. N.	$ \begin{vmatrix} -67 & 25.5 \\ -68 & 44.6 \\ -67 & 35.7 \end{vmatrix} $	E.N.E. E.N.E.	$+46 \\ +46 \\ +46$	$\begin{vmatrix} -5 \\ -5 \\ -5 \end{vmatrix}$	$\begin{bmatrix} \\ \\ \\ \end{bmatrix}$ -67 01 -67 01	Ship unsteady.
		***	N.S. Direct.	$\begin{bmatrix} -67 & 13.7 \\ -67 & 30.5 \end{bmatrix}$	E.N.E.	$^{+46}_{+46}$	_5		and musicani.

				011		Correc	ctions.				-
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True	Inclination.		Remarks.
_	0 /	9.0 /		00 1	1	/.	_ <u>4</u>	, , ,	· , o	,	
Mar. 28.	-5855 -5850		Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	n.e. by e.	+55 +55	$-4 \\ -4$				**
	- 50 50	211 12	S.	$-66\ 41.4$	N.E. by E.	+55	-4	-65	27 —65	97	
			N.	-66 22.2	n.e. by e.	+55	-4	7-03	21 -00	~1	
			N.S.	$-66\ 14.5$	N.E. by E.	$+55 \\ +55$	-4 -4				
29.	58 23	280 03	Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.E. by E. N.E. \frac{1}{2} E.	+57	-4	\exists			
29.	-00 20	200 00	S.	$-65\ 56.7$	N.E. 1/2 E.	+57	-4				
			N.	$-65 \ 46.0$	N.E. 1/2 E.	+57	-4	>-64	-64	49	
			N.S.	-65 28.5	N.E. 1/2 E.	+57	-4				
	* 0.00	202.04	Direct.	$-65 \ 36.0$	N.E. $\frac{1}{2}$ E.	+57 + 50	$-4 \\ -3$	\exists			
30.	-58 29	282 04	Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.E. by E. $\frac{1}{2}$ E. N.E. by E. $\frac{1}{2}$ E.		-3	0.0			
			s. N.	$-64 \ 39.2$	N.E. by E. $\frac{1}{2}$ E.		_3	}− 63	1		
			N.S.	-64 29.9	N.E. by E. $\frac{1}{2}$ E.	+50	_3]	}−63	41	
	-58 28	282 32	Direct.	-64 22.0	N.E. 1/2 E.	+54	_3	-63			
31.	-58 34	285 44	Direct.	$-63\ 52.3$	N.E. $\frac{1}{2}$ N.	+58	_3	-62	. !		
			Direct.	-63 490	N.E. by N.	$ +60 \\ +60 $	$-3 \\ -3$		ſ	05	A very heavy swell.
	-58 29	286 04	N.	$\begin{vmatrix} -64 & 34.2 \\ -64 & 10.0 \end{vmatrix}$	n.e. by n.	+60	-3	>-63	7.)	-	
			N.S. Direct.	$-63\ 43.0$	N.E. by N.	+60	-3	~			
nril 1	-57 22	289 50	Direct.	-62 24.0	N.E. by N.	+56	-2	П			
pin	0, 22	200 00	S.	$-62\ 16.2$	n.e. by n.	+56	-2				
			N.	-61 50.6	N.E. by N.	+56	-2	>-61	15 - 61	15	
			N.S.	-61 59.0	n.e. by n.	+56	-2				i i
			Direct.	-62 17.0	n.e. by n.	+56	$-2 \\ -1$	K			
2.	-57 10	292 11	Direct.	-59 31.0	E.N.E.	+44 +44	_1				
141			S. N.	$\begin{bmatrix} -59 & 28.3 \\ -59 & 55.5 \end{bmatrix}$	E.N.E.	+44	_1	>-58	45)		
			N.S.	-58 59.0	E.N.E.	+44	0		1	51	A swell from the
			Direct.	-59 25.3	E.N.E.	+44	_1	J	1	91	westward.
	-57 17	292 32	Direct.	-58 35.5	S.S.E.	_46	0	-59	21		
3.	-56 40	294 46	Direct.	-59 44.0	N.E.	+55	-1				
	-		S.	$-60 \ 36.7$	N.E.	+55 +55	-1 -1	>-59	01 -59	۵1	
		· V	N. N.S.	$\begin{bmatrix} -60 & 05.7 \\ -59 & 36.5 \end{bmatrix}$	N.E.	+55	-1		01 03	01	102
			Direct.	-59 30 5 -59 33.5	N.E.	+55	-1				
4.	-54 50	298 08	Direct.	-57 34.0	N. by E.	+54	0	П			
		100	N.	-57 00.3	N. by E.	+54	0	>-56	10 56	10	Too much motion t
			N.S.	-57 10.0	N. by E.	+54	0				use S.
			Direct.	-57 24.0	N. by E.	+54	0	K			
5.	-5254	300 27	Direct.	-54 47.5	N.N.E.	+47 +47	$\begin{vmatrix} +2 \\ +2 \end{vmatrix}$				ž.
			S. N.	$\begin{vmatrix} -54 & 56.6 \\ -54 & 45.7 \end{vmatrix}$	N.N.E.	+47	+2	 -53	52 - 53	52	
			N.S.	-54 30.7	N.N.E.	+47	+2				
			Direct.	-54 26.0	N.N E.	+47	+2	IJ	_		
6.	$-52 \ 36$		Direct.	-54 23.8	N.N.E.	+41	+2	-53			*
	-51 47		Direct.	-53 08.0	n.w. by n.	+42	+3	-52		34	L
2			Direct.	-52 10.0	E. by s.	+18	+3	-51	נפני		
11.		ouis, Falk-	Direct.	$\begin{vmatrix} -52 & 29 \cdot 1 \\ -52 & 42 \cdot 7 \end{vmatrix}$							
		Islands. 2 301 53	N. N.	$-52 \ 37.9$	Observed						
	-01 04	001 00	N.S.	-52 41.2	1 1	1 4	+3	-52	30 - 52	21	0

* Observed on shore;
$$\begin{cases} \text{Direct.} -5\mathring{3} & 48.9 \\ \text{S.} & -53 & 29.2 \\ \text{N.} & -53 & 45.9 \\ \text{N.S.} & -53 & 41.5 \end{cases}$$

				Observed		Correc	tions.		
1842.	Lat.	Long.	Method. employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Aug. 19.	_51 32	301 53	Direct. S. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Observed on shore.	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	+3	$-5\overset{\circ}{2}$ $\overset{\circ}{30}$ $-5\overset{\circ}{2}$ $\overset{\circ}{30}$	
17.	-51 32	301 53	N.S. Direct. S. Direct.	$ \begin{vmatrix} -52 & 31.5* \\ -52 & 46.5 \\ -53 & 00.9 \\ -52 & 38.8 \end{vmatrix} $	w. w. w.	$\begin{vmatrix} +37 \\ +37 \\ +38 \end{vmatrix}$	+3 +3 +3	$\left.\begin{array}{c} -52 & 14 \\ -51 & 58 \end{array}\right $	
	At An	ehor.	S. Direct. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	W.N.W. N.W. N.W.	+38 +42 +42 +41	+3 +3 +3 +3		
		ttraction.	S. Direct. S. Direct.	$ \begin{array}{r} -52 & 46.4 \\ -52 & 54.0 \\ -52 & 52.3 \\ -52 & 37.5 \end{array} $	N.N.W. N. N.	+41 $ +41 $ $ +41 $ $ +41 $	+3 +3 +3 +3	$ \begin{cases} -52 & 09 \\ -51 & 57 \end{cases} $	10
		To obtain corrections for the ship's attraction.	S. Direct. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.E. N.E. N.E. E.N.E.	$\begin{vmatrix} +41 \\ +42 \\ +42 \\ +38 \end{vmatrix}$	+3 +3 +3 +3	$ \begin{vmatrix} 5 & 5 & 7 \\ -51 & 58 \\ -52 & 02 \end{vmatrix} $,
		ons for th	S. Direct. S. Direct.	$ \begin{vmatrix} -52 & 44.7 \\ -52 & 32.0 \\ -52 & 21.5 \\ -52 & 31.0 \end{vmatrix} $	E.N.E. E. E. E.S.E.	$\begin{vmatrix} +38 \\ +37 \\ +37 \\ +9 \end{vmatrix}$	+3 +3 +3 +3	$\begin{vmatrix} 5 & 5 & 5 \\ -51 & 47 \\ -52 & 13 \end{vmatrix} -52 & 05$	
		1 correcti	S. Direct. S. Direct.	$ \begin{vmatrix} -52 & 20 \cdot 1 \\ -52 & 13 \cdot 2 \\ -52 & 22 \cdot 6 \\ -51 & 51 \cdot 7 \end{vmatrix} $	E.S.E. S.E. S.E. S.S.E.	$\begin{vmatrix} + & 9 \\ -14 \\ -14 \\ -32 \end{vmatrix}$	$ \begin{array}{r} +3 \\ +3 \\ +3 \\ +3 \end{array} $	$\left. \begin{array}{c} -52 & 29 \end{array} \right $	
	-	To obtair	S. Direct. S. Direct.	$ \begin{array}{c cccc} -52 & 16.2 \\ -51 & 21.0 \\ -51 & 51.0 \end{array} $	S.S.E. S. S.	$\begin{vmatrix} -32 \\ -40 \\ -40 \\ -32 \end{vmatrix}$	$\begin{vmatrix} +3 \\ +3 \\ +3 \end{vmatrix}$	$igg egin{array}{c c} -52 & 33 \ -52 & 13 \ \end{array}$	
			S. Direct. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.w. s.s.w. s.w. s.w.	$\begin{vmatrix} -32 \\ -14 \\ -14 \end{vmatrix}$	+3 +3 +3 +3	$ \begin{vmatrix} -51 & 58 \\ -51 & 35 \end{vmatrix} $	
			Direct. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	W.S.W. W.S.W.	+ 9 + 9 + 37	$\begin{vmatrix} +3 \\ +3 \\ +3 \end{vmatrix}$	$ \begin{vmatrix} -52 & 05 \\ -52 & 07 \end{vmatrix} $	

* Observed on shore;
$$\begin{cases} \text{Direct.} - \mathring{53} & \mathring{34} \cdot 2 \\ \text{S.} & -53 & 31 \cdot 8 \\ \text{N.} & -53 & 24 \cdot 3 \\ \text{N.S.} & -53 & 21 \cdot 8 \end{cases}$$

Observations of the Inclination made in Her Majesty's Ship Terror, with Needle F. C. B., between April 1841 and August 1842.

Observers Captain Francis Rawdon Crozier, and Mr. Thomas Moore, Mate, R.N.

				Observed		Corre	ctions.	_	
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Apr. 19.	netic Ob	on Mag- servatory. 147 24*	Direct. Direct. Def. N. Def. S. Mag. N.S. Mag. N. Mag. S.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Observed on shore.		-35 -35 -81 -35 -35 -35 -35	-70 52 -70 52	Aspareneedle(marked C.) was used as deflector N. and deflector S.: and the magnets of the apparatus as Mag. N. Mag. S. and Mag. N.S.
July 7.	Storn	ng out of n Bay.	Direct. Def. N. Def. S. Direct.	$ \begin{array}{r} -69 & 46.5 \\ -69 & 29.9 \\ -69 & 38.8 \\ -69 & 51.2 \end{array} $	S.E. 34 E. S.E. 54 E. S.E. 34 E. S.E. 34 E.	$ \begin{array}{r} -32 \\ -32 \\ -32 \\ -32 \end{array} $	$ \begin{array}{r} -35 \\ -81 \\ -35 \\ -35 \end{array} $		Ship steady.
	-43 03 $-42 24$	149 30	Direct. Def. N. Def. S. Direct. Direct. Def. N. Def. S.	-70 58·0 -70 50·4 -71 02·0 -71 04·0 -70 43·3 -70 34·1 -70 36·0	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. N.N.W. N.N.W.	+27 +27 +27 +27 +76 +76 +76	$ \begin{array}{r} -35 \\ -81 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ \end{array} $	$ \begin{cases} -71 & 18 \\ -70 & 10 \end{cases} -70 & 44 $	Ship very steady.
10.	—40 51	149 28	Direct. Direct. Def. N. Def. S. Direct.	$ \begin{array}{rrrrr} -70 & 45.5 \\ -69 & 42.7 \\ -69 & 19.7 \\ -69 & 37.7 \\ -69 & 47.0 \end{array} $	N.N.W. N. by W. N. by W. N. by W. N. by W.	+76 +78 +78 +78 +78	-35 -35 -81 -35 -35		Ship very steady.
11.	—38 17	150 22	Direct. Def. N. Def. S. Direct.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	n. by E. n. by E. n. by E. n. by E.	+73 +73 +73 +73	$-35 \\ -81$		Ship very steady.

^{*} Observations at Hobarton to obtain corrections for the ship's attraction.

	~			Observed		Corre	ctions.			
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True In	clination.	Remarks.
Inly 19	-37 28	1°51 30	Direct.	$-66 \ 45.1$	N.E. $\frac{1}{2}$ N.	+63	-35	· ·	0 /	
July 12.	-07 20	101 00	Def. N.	$-66 \ 40.0$	$N.E. \frac{1}{2} N.$	+63	-81			
			Def. S.	$-66\ 19.1$	N.E. $\frac{1}{2}$ N.	+63	-35	>-66 25	2 —66 22	Ship steering steadily.
			Direct.	$-66\ 49.7$	$\begin{array}{c} N.E. \ \frac{1}{2} \ N. \end{array}$	+63	-35			steadily.
13.	-36 21	151 39	Direct.	-66 24.5	N.N.W. 1/4 W.	+69	-35	Κ -		
			Def. N.	-66 35.9	N.N.W. $\frac{4}{4}$ W.	+69	-81	> −66 1	1 -66 11	Ship unsteady.
		-	Direct.	-66 29.1	N.N.W. 1 W.	+69	-35			,
14.	-34 06	151 19	Direct.	-63 25.9	N.	+67	-35	K		
			Def. N.	$-63\ 08.4$	N.	+67	81	Car		
		-	Def. S.	-63 11.9	N.	+67	-35	>-62 5	5 -62 58	Steering steadily.
			Direct.	-63 29.6	N.	+67	-35			
19.	Garden	Island,	Direct.	-62 29.3*	1		-35	ă —		
	Syd	lney.	Def. N.	-61 36.7			81			
	$-33 \ 51$	151 17	Def. S.	-62 29.8	Observed		-35			
			Mag. N.	$-62\ 15.2$	on shore.		35	>-62 59	-6259	
	ė.		Mag. S.	-62 17.4	on shore.		-35			
		-	Mag. N.S.	-62 14.0			35			
			Direct.	-62 28.8	IJ		-35	J .		
30.	At an	achor.	Direct.	$-62\ 36.6$	w. by s.	+12	-35	-63 00		
Aug. 4.			Direct.	-63 06.1	w.	+25	-35	$-63 \ 16$		
			Direct.	-63 03.3	W. 1/2 S.	+18	-35	-63 20		
5.			Direct.	-62 06.4	s.w. by w.	-16	-35	$-62\ 57$		
	-		Direct.	$-62\ 16.0$	s.w. ½ w.	-25	-35	$-63 \ 16$		
5.		g out of	Direct.	-6252.9	E. by N. $\frac{1}{2}$ N.	+39	-35	-6249		Head swell on the 5th, steering badly.
	hart	oour.	Def. N.	$-62\ 14.1$	E. by $N \cdot \frac{1}{2} N$.	+39	-81	-6256		only steering samy.
			Def. S.	$-62\ 25.4$	E. by N. $\frac{1}{2}$ N.	+39	-35	-62 21		
			Mag. N.	$-62 \ 34.4$	E. by N. $\frac{1}{2}$ N.		-35	$-62 \ 30$	'	
	,		Mag. S.	$-62\ 44.6$	E. by N. $\frac{1}{2}$ N.	+39	-35	-6241		
c	04 07	150 15	Direct.	$-62\ 43.5$	E. by N. ½ N.	+39	-35	-6240	ני	
0.	-34 01	153 17	Direct. Def. N.	$-62 \ 31.3$	E. by N.	+35	-35			
			Def. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by N.	+35	-81	1		
			Direct.		E. by N.	+35	-35			
	-33 54	152 54	Direct.	$ \begin{array}{r rrrr} -62 & 27.2 \\ -62 & 23.7 \end{array} $	E. by N.	+ 35	-35 -35	>-62~30	$-62 \ 30$	Steering badly.
	-00 04	100 04	Def. N.	$-62 \ 02.6$	E. by N. E. by N.	$+35 \\ +35$	-81			
			Def. S.	-62 02.8	E. by N.	+35	-35			
			Direct.	-62 24.1	E. by N.	+35 + 35	-35		and the second	
7.	-33 56	156 38	Direct.	$-61 \ 40.6$	E. by N.	+35	-35	ጎ	Property	•
	55 50		Def. N.	-61 09.9	E. by N.	+35	-81			
			Def. S.	$-61 \ 40.7$	E. by N.	+35	-35	>−61 46	$-61 ext{ } 46$	Steering wildly.
		_	Direct.	$-61 \ 47.6$	E. by N.	+35				
8.	-33 31	160 20	Direct.	-61 17.4	E. by N.	+35	-35	<u>ጎ</u> -		
			Def. N.	-60 38.1	E. by N.	+35	-81	61 04	63.64	a
		-	Def. S.	-60 22.1	E. by N.		-35	-61 04	-01 04	Steering tolerably.
			Direct.	-61 14.2	E. by N.		-35	J		0
9.	-3342	164 05	Direct.	-60 40.6	E.		_35)		
			Def. N.	-60 17.2	Е.	+26	-81	-60 52	60 50	a
			Def. S.	-60 30·8	E.	+26	-35	-00 02	-00 52	Steering badly.
,		1	Direct.	$-60 \ 37.7$	E.	+26	-35	i		

* Observed on shore;
$$\begin{cases} \text{Direct.} & \dots & -6\mathring{2} & 5\mathring{2} \cdot 9 \\ \text{Def. N.} & \dots & -63 & 00 \cdot 7 \\ \text{Def. S.} & \dots & -62 & 52 \cdot 4 \end{cases} \text{ Mag. N.} & \dots & -6\mathring{3} & 00 \cdot 8 \\ \text{Mag. N.} & \dots & -6\mathring{3} & 00 \cdot 7 \\ \text{Def. S.} & \dots & -62 & 52 \cdot 4 \end{cases} \text{ Mag. S.} & \dots & -6\mathring{2} & 57 \cdot 0 \end{cases} \text{ Direct. } \dots & -6\mathring{2} & 52 \cdot 3$$

		-,		Observed		Corre	ctions.			A.
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination	l•	Remarks.
Aug. 10.	99 47	166 39	Direct.	$-5^{\circ}_{9} 5^{\circ}_{9}$	E. by N. ½ N.	+39	$-3\overset{'}{5}$	o /	,	
Aug. 10.	35 4/	100 39	Def. N.	-59 56.7	E. by N. $\frac{1}{2}$ N.	+39	-35 - 81			.40
			Def. S.	-59 38.1	E. by N. $\frac{1}{2}$ N.	+39	1	>-60 027		
			Direct.	$-60\ 02.2$	E. by N. $\frac{1}{2}$ N.	+39	-35			
	-3342	166 36	Direct. Def. N.	$-59 42.3 \\ -59 00.3$	Е.	+26		K I		
			Def. N. Def. S.	$-59 \ 00.3$ $-59 \ 42.7$	E. E.	$\begin{vmatrix} +26 \\ +26 \end{vmatrix}$	$\begin{vmatrix} -81 \\ -35 \end{vmatrix}$	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	9 55	Long swell, motion quick, steering
			Mag. N.	-59 21.1	E.	+26	-35	-59 49		steadily.
			Mag. S.	-59 39.9	E.	+26				
			Direct.	$-60\ 02.2$	E. by N.	+36	-35	Į Į		
11.	-33 34	167 37	Direct.	$-60\ 13.9$	N.E. by E.	+50	-35			
			Def. N. Def. S.	-59 18.4	n.e. by e.	+50	-81			
			Mag. N.	$\begin{vmatrix} -60 & 03.5 \\ -60 & 04.1 \end{vmatrix}$	N.E. by E.	$ +50 \\ +50 $	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	-59 49		
(Mag. S.	$-60 \ 01.4$	N.E. by E.	+50	-35	-5	9 58	Wind light, with a
			Mag. N.S.	-59 54.0	N.E. by E.	+50	-35			heavy swell, mo-
			Direct.	-60 09.5	N.E. by E.	+50	-35	J		1
	—33 31	167 41	Direct.	-59 53.1	E	+26	-35	$\} -60 07$		
10	99 00	160.00	Def. N.	-59 17.2	E.	+26	-81]		
12.	-33 00	169 20	Direct. Def. N.	$\begin{vmatrix} -58 & 59.8 \\ -58 & 22.6 \end{vmatrix}$	E.N.E.	+43 + 43				
			Def. S.	-58 56.9	E.N.E.	+43	-35			
			Mag. N.	-58 36.5	E.N.E.	+43	-35	>-58 43		
			Mag. S.	-58 23.1	E.N.E.	+43		\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-	8 43	Motion quick, steer- ing well.
			Direct.	-58 56.7	E.N.E.	+43				mg went
			Direct.	-59 10.4	N.E.	+52	-35	ļ		
			Mag. N.S. Direct.	-58 40.5	N.E.	+52	$-35 \\ -35$	$-58 \ 43$		Ship unsteady.
13.	-32 12	170 27	Direct.	$\begin{vmatrix} -59 & 09.1 \\ -56 & 21.9 \end{vmatrix}$	s.e. by e.	$ +52 \\ -10$	-35	K		-
10.	02 12	1,0 2,	Def. N.	-56 00.5	s.e. by e.	-10	-81	77.10-		
			Def. S.	_56 18.1	s.E. by E.	-10	-35	-57 13		
			Direct.	-56 24.6	s.e. by e.	-10		Į l		
14.	-32 11	171 20	Direct.	-5658.5	s.e. by e.	-10	-35) -5	7 28	Much motion, steer-
			Def. N. Def. S.	$\begin{bmatrix} -56 & 11.3 \\ -56 & 40.0 \end{bmatrix}$	s.e. by e.	$ -10 \\ -10$				ing well.
			Mag. N.	-56 46.1	s.E. by E.	-10		>-57 36		
			Mag. N.S.	-56 55.9	s.e. by E.	-10				
			Mag. S.	-5649.8	s.E. by E.	-10	-35			
, ,	00	1/71	Direct.	-56 51.0	s.e. by e.	-10				
15.	-33 55	171 59	Direct. Def. N.	-57 39·5	E. by s.	+14	$\begin{vmatrix} -35 \\ -81 \end{vmatrix}$	$-58 17$		
			Dei. N. Direct.	$\begin{bmatrix} -57 & 06.2 \\ -58 & 22.1 \end{bmatrix}$	E. by S. E. ½ N.	+ 14 + 32	$-81 \\ -35$	<u> </u>	8 9.4	A head sea, table
		6	Def. N.	$-57 \ 57.4$	$E. \frac{1}{2} N.$	+32	-81	 }−58 32	- ~·	very unsteady.
			Direct.	-58 20.8	E. $\frac{1}{2}$ N.	+32	-35	J J		
	—33 58	172 06	Direct.	-5757.7	E.S.E.	+ 4	-35			
			Def. N.	-57 32.5	E.S.E.	+ 4	1			
			Def. S. Mag. N.	$\begin{vmatrix} -57 & 22 \cdot 1 \\ -57 & 24 \cdot 9 \end{vmatrix}$	E.S.E.	$\begin{vmatrix} + & 4 \\ + & 4 \end{vmatrix}$	-35 -35	$> -58 \ 14 \ -5$	8 1/	Head sea, steering
			Mag. N.S.	-57 30.0	E.S.E.	+4	-35		J 14	badly, ship un-
40			Mag. S.	-57 22.9	E.S.E.	+4	-35			steady.
			Direct.	-58 00.5	E.S.E.	+ 4	-35	IJ -		
16.	-34 15	172 50	Direct.	-59 25.6	N.W. $\frac{1}{2}$ N.	+51	-35]]		
			Def. N.	-59 00·3	N.W. $\frac{1}{2}$ N.	+51	-81			
			Def. S. Mag. N.	$\begin{vmatrix} -58 & 46.2 \\ -59 & 01.4 \end{vmatrix}$	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N.	+51 + 51	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	>−58 48		Head sea, steering
			Mag. N.S.	-58 55.8	$\begin{array}{c c} N.W. \overline{2} & N. \\ N.W. \frac{1}{2} & N. \end{array}$	+51	-35	1 4	8 48	hadly chin un
				1 55 0	2	'	"	11		swauy.

				Observed	-	Correc	tions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Aug. 16.	-34 1'5	172 50	Mag. S. Direct. Direct. Mag. N.S. Direct.	-58 08·6 -59 24·6 -58 26·9 -58 04·7 -58 23·1	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N. E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s.	$+51 \\ +51 \\ +7 \\ +7 \\ +7$	-35 -35 -35 -35 -35	-58 46	8 Head sea, steering badly, ship unsteady.
17.	—34 24	173 43	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-58 33·2 -58 21·7 -58 23·3 -58 25·9 -58 25·5 -58 21·4	E. by $s. \frac{1}{2} s.$ E. by $s. \frac{1}{2} s.$	+ 7 + 7 + 7 + 7 + 7 + 7	-35 -81 -35 -35 -35		O Strong wind, a good deal of motion.
18.		g into the Islands.	Direct. Direct. Def. N. Direct.	-58 26·8 -58 20·6 -58 08·4 -58 19·2	E. by s. ½ s. s.w. s.w. s.w.	$\begin{vmatrix} +7\\ -30\\ -30\\ -30 \end{vmatrix}$	-35 -35 -81 -35		6 Heavy sea, steering wildly.
Oct. 21.	New 2	Islands, Zealand. 174 00	Direct. Def. N. Def. S. Mag. N.S. Mag. S. Direct. Direct. Def. S. Mag. N. Mag. N.S. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	-58 19.2 -59 00.4 -57 57.5 -59 05.1 -58 41.0 -58 38.4 -59 01.0 -59 00.8 -57 58.4 -58 59.2 -58 38.7 -58 40.3 -58 37.1 -59 02.2*	Observed on shore.		-35 -81 -35 -35 -35 -35 -35 -35 -35 -35 -35	-59 34 -59 18 -59 40 -59 16 -59 19 -59 13 -59 36 -59 36 -59 19 -59 34 -59 14 -59 15 -59 12	5 Magnetic observa- tory.
	Bay of about from Pland.	out of Islands, one mile iercy Is-	Direct. Direct. Def. N. Def. S. Direct.	-57 50·2 -58 34·3 -57 57·1 -58 40·9 -58 34·2	s.e. by e. e. by s. e. by s. e. by s. e. by s.		-35 -35 -81 -35 -35	$ \begin{array}{c cccc} -58 & 58 \\ -59 & 07 \\ -59 & 05 \\ -58 & 58 \end{array} $	Very steady.
24.	-36 20	177 27	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	-59 13·5 -58 23·2 -58 53·7 -58 39·2 -58 37·0 -58 37·3 -59 14·7	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E.	- 5 - 5 - 5 - 5 - 5 - 5	-35 -81 -35 -35 -35 -35 -35	$ \begin{vmatrix} -59 & 49 \\ -59 & 34 \\ -59 & 19 \\ -59 & 17 \\ -59 & 17 \end{vmatrix} $	Ship unsteady.
25 .		179 34	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	-59 147 -59 41·1 -58 31·6 -58 54·4 -58 54·0 -59 02·5 -58 55·4 -59 37·6	s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s.	-40 -40 -40 -40 -40 -40 -40	$ \begin{array}{r} -35 \\ -81 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ \end{array} $	-60 56 -60 33 -60 09 -60 09 -60 17 -60 10	Hand see table
	-38 27	179 59	Direct.	-60 11·8	s.e. by E. ½ E	-12	-35	$\begin{array}{c c} -60 & 53 \\ -60 & 59 \end{array} > -60 & 3 \end{array}$	unsteady.

Direct.... Oct. 21. -59 47.6 Oct. 29. -59° 54.6Oct. 29. -60 10.7 Def. N. . . Oct. 21. -60 13.9 Oct. 29. $-60\ 06.3$ Def. S. .. Oct. 21. $-60\ 00.5$ * Observed on shore;] Oct. 29. -60 13·1 Mag. N... Oct. 21. -60 10.3 face west. Mag. N.S. Oct. 21. -60 13.7 Oct. 29. -60 01.2 Mag. S... Oct. 21. -60 07.4 Oct. 29. -60 12.8 Direct.... Oct. 21. -59 48.6 Oct. 29. -59 58.5

Delinancina elinabera celinabi	<u> </u>					Correc	ctions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Nov. 25.	_3°8 2′7	17̈́9 5́9	Def. N. Def. S. Mag. N.	$-5^{\circ}9 06.2$ $-60 03.3$ $-59 51.3$	s.e. by e. $\frac{1}{2}$ e. s.e. by e. $\frac{1}{2}$ e. s.e. by e. $\frac{1}{2}$ e.	-12	-35	$ \begin{array}{c c} -60 & 39 \\ -60 & 50 \\ -60 & 38 \end{array} $	Head sea, table unsteady.
*	-38 57	181 18	Mag. N.S. Mag. S. Direct. Direct.	$ \begin{array}{ccccc} -59 & 46.0 \\ -60 & 00.6 \\ -60 & 12.9 \\ -60 & 00.6 \end{array} $	s.e. by E. $\frac{1}{2}$ E.	$\begin{vmatrix} -12 \\ -12 \end{vmatrix}$	-35 -35 -35 -35	$ \begin{array}{c c} -60 & 33 \\ -60 & 48 \\ -61 & 00 \\ -60 & 41 \end{array} $	Heavy sea, much
26.			Direct. Def. N. Def. S.	$ \begin{array}{r} -61 & 08.6 \\ -60 & 00.6 \\ -60 & 37.7 \end{array} $	E.S.E. E.S.E. E.S.E.	$ \begin{bmatrix} -5 \\ -5 \\ -5 \\ -31 \end{bmatrix} $	-35 -81 -35 -35	$ \begin{array}{c c} -61 & 49 \\ -61 & 27 \\ -61 & 18 \\ -61 & 18 \end{array} $	motion, observations not satisfactory.
	ĭ		Direct. Def. N. Def. S. Mag. N.	$ \begin{array}{c cccc} -60 & 11.9 \\ -59 & 07.5 \\ -59 & 48.8 \\ -59 & 36.8 \end{array} $	S.E. S.E. S.E.	$ \begin{array}{r r} -31 \\ -31 \\ -31 \end{array} $	-81 -35 -35	$egin{array}{c c} -61 & 00 \\ -60 & 55 \\ -60 & 43 \\ \end{array}$	Tolerably steady.
	-39 02	182 35	Mag. N.S. Mag. S. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. S.E. S.E. E.S.E.	$\begin{bmatrix} -31 \\ -31 \\ -31 \\ -5 \end{bmatrix}$	-35 -35 -35 -35	$\begin{vmatrix} -60 & 54 \\ -60 & 45 \\ -61 & 15 \\ -61 & 54 \end{vmatrix} -61 & 21$	
			Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{vmatrix} -60 & 13.3 \\ -60 & 46.2 \\ -60 & 42.2 \\ -60 & 51.5 \end{vmatrix} $	E.S.E. E.S.E. E.S.E.	- 5 - 5 - 5 - 5	_81 _35 _35 _35	$ \begin{bmatrix} -61 & 39 \\ -61 & 26 \\ -61 & 22 \\ -61 & 31 \end{bmatrix} $	Head swell with considerable motion.
27.	-39 14	182 54	Mag. N. Direct. Direct. Def. N.	$ \begin{vmatrix} -60 & 06.7 \\ -61 & 13.9 \\ -60 & 24.6 \\ -59 & 12.0 \end{vmatrix} $	E.S.E. E.S.E. S.E. by E. S.E. by E.	$ \begin{bmatrix} -5 \\ -5 \\ -20 \\ -20 \\ -20 \end{bmatrix} $	_35 _35 _35 _81	$ \begin{bmatrix} -61 & 47 \\ -61 & 54 \end{bmatrix} $ $ -61 & 20 \\ -60 & 53 \\ -61 & 25 \end{bmatrix} $	
			Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{r rrrr} -60 & 30.1 \\ -59 & 54.5 \\ -59 & 55.1 \\ -60 & 15.2 \end{array} $	s.e. by e. s.e. by e. s.e. by e. s.e. by e.	$\begin{bmatrix} -20 \\ -20 \\ -20 \end{bmatrix}$	_35 _35 _35 _35	$ \begin{array}{c c} -60 & 50 \\ -60 & 50 \\ -61 & 10 \end{array} $	Tolerably steady, steering well.
	-39 15	183 02	Direct. Direct. Direct.	$ \begin{array}{r rrrr} -60 & 31.5 \\ -59 & 41.2 \\ -59 & 41.8 \end{array} $	s.E. by E. s. by E. $\frac{1}{2}$ E. s. $\frac{1}{2}$ E.	$\begin{bmatrix} -20 \\ -56 \\ -61 \end{bmatrix}$	_35 _35 _35	$ \begin{vmatrix} -61 & 27 \\ -61 & 12 \\ -61 & 18 \\ -61 & 15 \end{vmatrix} $	Slight motion.
	-39 31	183 00	Direct. Def. N. Def. S.	$ \begin{array}{r rrrr} -59 & 51.6 \\ -59 & 13.4 \\ -59 & 59.5 \end{array} $	s. by E. s. by E. s. by E.	$\begin{bmatrix} -60 \\ -60 \\ -60 \end{bmatrix}$	$\begin{bmatrix} -35 \\ -81 \\ -35 \end{bmatrix}$	$ \begin{vmatrix} -61 & 27 \\ -61 & 34 \\ -61 & 34 \end{vmatrix} $	Table steady.
			Mag. N. Mag. N.S. Mag. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by E. s. by E. s. by E. s. by E.	$ \begin{bmatrix} -60 \\ -60 \\ -60 \\ -60 $	-35	$ \begin{vmatrix} -60 & 59 \\ -61 & 06 \\ -61 & 20 \\ -61 & 30 \end{vmatrix} $	***
28.	40 35	183 00	Direct. Direct. Def. N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E. S.E. S.E.	- 5 -33 -33 -33	$-35 \\ -81$	$ \begin{array}{c c} -61 & 54 \\ -61 & 56 \\ -61 & 53 \\ -62 & 06 \end{array} $	
,			Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{c cccc} -60 & 57.6 \\ -60 & 28.1 \\ -60 & 29.6 \\ -60 & 46.0 \end{array} $	S.E. S.E. S.E.	-33 -33 -33		$egin{array}{c c} -61 & 36 \\ -61 & 38 \\ -61 & 54 \\ \end{array}$	
-	-40 50	183 11	Direct. Direct. Def. N. Def. S.	$ \begin{array}{c cccc} -60 & 47.3 \\ -60 & 51.2 \\ -59 & 43.5 \\ -60 & 55.4 \end{array} $	S.E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.			$ \begin{vmatrix} -61 & 55 \\ -62 & 14 \\ -61 & 53 \\ -62 & 18 \end{vmatrix} -61 & 56$	
			Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{c cccc} -60 & 13.9 \\ -60 & 30.0 \\ -60 & 30.1 \end{array} $	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	-48 -48 -48	$ \begin{array}{r r} -35 \\ -35 \\ -35 \end{array} $	$egin{array}{c c} -61 & 37 \\ -61 & 53 \\ -61 & 53 \\ \end{array}$	Slight motion,
	1		Direct.	-60 54.0	S.S.E. ½ E.	-48	-35	$\begin{bmatrix} -62 & 17 \end{bmatrix}$	steering well.

				Observed		Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Nov. 29.	-41 34	183 40	Direct. Def. N. Def. S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by E. s. by E. s. by E.	$\begin{vmatrix} -60 \\ -60 \\ -60 \end{vmatrix}$	$-35 \\ -81 \\ -35$	$ \begin{bmatrix} -6\mathring{3} & 0\mathring{3} \\ -6\mathring{2} & 49 \\ -6\mathring{3} & 06 \end{bmatrix} $	Slight motion, steering well.
·	-42 40	183 46	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S.	$ \begin{vmatrix} -61 & 37 \cdot 1 \\ -61 & 03 \cdot 5 \\ -60 & 58 \cdot 9 \\ -61 & 44 \cdot 5 \\ -62 & 23 \cdot 7 \\ -61 & 02 \cdot 1 \\ -62 & 08 \cdot 6 \end{vmatrix} $	s. by E. s. by E. s. by E. s. by E. s. s. s.		$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ \end{array} $	$ \begin{vmatrix} -63 & 12 \\ -62 & 39 \\ -62 & 34 \\ -63 & 19 \end{vmatrix} $ $ \begin{vmatrix} -64 & 03 \\ -63 & 27 \\ -63 & 48 \end{vmatrix} $	
30.	-43 33	183 10	Mag. N. Mag. N.S. Mag. S. Direct. Direct.	$ \begin{array}{r} -61 & 54.9 \\ -62 & 03.6 \\ -62 & 01.2 \\ -62 & 29.6 \\ -63 & 26.2 \end{array} $	S. S. S. S. S. 12 W.		-35 -35 -35 -35 -35	$ \begin{vmatrix} -63 & 34 \\ -63 & 43 \\ -63 & 40 \\ -64 & 09 \\ -65 & 04 \end{vmatrix} $	
	2	*	Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{array}{r} -62 & 29.3 \\ -63 & 58.6 \\ -63 & 16.8 \\ -62 & 58.2 \\ 62 & 46.2 \end{array} $	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W.		-81 -35 -35 -35	-64 53 -65 37 -64 55 -64 36	Table steady, steering well.
	-43 50 -44 15	1	Mag. S. Direct. Direct. Direct. Def. N. Def. S.	$ \begin{vmatrix} -63 & 46 \cdot 3 \\ -63 & 26 \cdot 2 \\ -63 & 43 \cdot 0 \\ -64 & 07 \cdot 3 \\ -63 & 29 \cdot 4 \\ -63 & 59 \cdot 7 \end{vmatrix} $	s. ½ w. s. ½ w. s. by w. s. by w. s. by w.		-35 -35 -35 -81 -35	$ \begin{vmatrix} -65 & 24 \\ -65 & 04 \\ -65 & 20 \\ -65 & 44 \\ -65 & 52 \\ -65 & 37 \end{vmatrix} $	
			Mag. N. Mag. N.S. Mag. S. Direct.	$ \begin{vmatrix} -63 & 51.9 \\ -63 & 52.9 \\ -63 & 58.1 \\ -64 & 11.4 \end{vmatrix} $	s. by w.		-35 -35 -35 -35	$ \begin{array}{c c} -65 & 29 \\ -65 & 30 \\ -65 & 35 \\ -65 & 48 \end{array} $	Cross sea, motion slight.
Dec. 1.	-45 30	183 12	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{array}{r} -65 & 46 \cdot 1 \\ -65 & 01 \cdot 6 \\ -65 & 19 \cdot 5 \\ -65 & 14 \cdot 3 \\ -65 & 31 \cdot 7 \end{array} $	s.e. by e. s.e. by e. s.e. by e. s.e. by e.		-35 -81 -35 -35 -35	-66 45 -66 47 -66 19 -66 13 -66 31	
A Commission of the Commission of Commission	-45 48	183 25	Mag. S. Direct. Direct. Def. N. Def. S.	$ \begin{array}{r} -66 & 00.8 \\ -65 & 40.0 \\ -65 & 43.9 \\ -64 & 55.1 \\ -65 & 36.8 \end{array} $	S.E. by E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.		-35 -35 -35 -81 -35	$ \begin{vmatrix} -67 & 00 \\ -66 & 39 \\ -66 & 50 \\ -66 & 47 \\ -66 & 43 \end{vmatrix} $	Much pitching, steering well.
2.	47 13	3 184 30	Mag. N. Mag. N.S. Mag. S. Direct. Direct.	$\begin{array}{c cccc} -65 & 54 \cdot 2 \\ -65 & 40 \cdot 5 \\ -65 & 49 \cdot 2 \\ -65 & 47 \cdot 4 \\ -66 & 30 \cdot 4 \end{array}$	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. by E. $\frac{1}{2}$ E			$ \begin{bmatrix} -67 & 00 \\ -66 & 47 \\ -66 & 55 \\ -66 & 53 \\ -67 & 23 \end{bmatrix} $	
			Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{r} -65 & 41.8 \\ -66 & 43.2 \\ -66 & 31.4 \\ -66 & 30.3 \\ -66 & 37.0 \end{array} $	s.e. by e. $\frac{1}{2}$ e s.e. by e. $\frac{1}{2}$ e s.e. by e. $\frac{1}{2}$ e s.e. by e. $\frac{1}{2}$ e s.e. by e. $\frac{1}{2}$ e	$ \begin{array}{c c} -18 \\ -18 \\ -18 \end{array} $		$ \begin{vmatrix} -67 & 21 \\ -67 & 36 \\ -67 & 24 \\ -67 & 23 \\ -67 & 30 \end{vmatrix} $	Ship pitching, but steering well.
	-47 39	184 55	Direct. Direct. Def. N. Def. S. Mag. N.	$ \begin{vmatrix} -66 & 34.6 \\ -66 & 54.4 \\ -65 & 36.6 \\ -66 & 40.1 \\ -66 & 21.5 \end{vmatrix} $	s.e. by e. 1/2 c s.e. by e. s.e. by e. s.e. by e. s.e. by e.			$\begin{vmatrix} -67 & 28 \\ -67 & 55 \\ -67 & 24 \\ -67 & 41 \\ -67 & 23 \end{vmatrix} -67 & 32$	Very steady.
			Mag. N.S. Mag. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$			-35 -35 -35	$ \begin{vmatrix} -67 & 36 \\ -67 & 36 \\ -67 & 48 \end{vmatrix} $	

			,	Observed		Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Dec. 3.	-48 18	185 54	Direct. Def. N. Def. S. Mag. N.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by e. s.e. by e. s.e. by e. s.e. by e.	-27 -27 -27 -27	-35 -81 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Mag. N.S. Mag. S. Direct. Direct. Direct.	-67 21·9 -67 17·1 -67 38·6 -67 46·6 -68 01·5	s.e. by e. s.e. by e. s.e. by e. e.s.e. s.e. by e.½ e.	$ \begin{array}{r} -27 \\ -27 \\ -27 \\ -11 \end{array} $	-35 -35 -35 -35 -35		Very steady.
	49 US	100 04	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{r rrrr} -67 & 07.3 \\ -67 & 55.0 \\ -67 & 49.5 \\ -67 & 44.7 \end{array} $	s.e. by E. ½ E. s.e. by E. ½ E. s.e. by E. ½ E s.e. by E. ½ E s.e. by E. ½ E.	-19 -19 -19 -19	_81	-68 47 -68 49 -68 44 -68 39 -68 48	
4.	-49 24	187 23	Direct. Direct. Direct. Direct. Direct.	-68 54·3 -68 53·5 -68 33·0 -68 29·8 -68 42·3	s.e. by e. $\frac{1}{2}$ E. N.E. by E. E. $\frac{1}{2}$ N. E. E.N.E.		$-35 \\ -35$	-69 48 -68 35 -68 42 -68 45 -68 32	
	z i		Direct. Direct. Direct. Def. N. Direct.	$\begin{array}{c} -68 & 28.7 \\ -68 & 45.7 \\ -68 & 52.2 \\ -67 & 28.0 \\ -68 & 48.0 \end{array}$	W.S.W. W. E. E. E. by s.	$ \begin{array}{r} -12 \\ +20 \\ +20 \\ +20 \\ +30 \\ +4 \end{array} $	-35 -35 -35 -81 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Steady.
	*		Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{array}{c cccc} -67 & 29.5 \\ -68 & 52.0 \\ -68 & 29.0 \\ -68 & 28.1 \end{array} $	E. by s. E. by s. E. by s. E. by s.	+ 4 + 4 + 4 + 4	-81 -35 -35 -35	$ \begin{array}{r rrr} -68 & 47 \\ -69 & 23 \\ -69 & 00 \\ -68 & 59 \end{array} $	Swell from nor ward. Table steady.
5.	-49 23	188 54	Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$ \begin{vmatrix} -68 & 42.7 \\ -69 & 01.0 \\ -68 & 43.9 \\ -67 & 31.6 \\ -68 & 42.2 \\ -68 & 42.6 \end{vmatrix} $	E. by s.	+ 4 + 4 + 4 + 4 + 4	35 35 35 81 35 35	$ \begin{array}{c c} -69 & 14 \\ -69 & 32 \\ -69 & 15 \\ -68 & 49 \\ -69 & 13 \\ -69 & 14 \end{array} $	J
	-49 3 8	189 44	Mag. N.S. Mag. S. Direct. Direct. Def. N.	$ \begin{array}{r} -68 & 40 \cdot 1 \\ -68 & 30 \cdot 6 \\ -68 & 44 \cdot 2 \\ -68 & 15 \cdot 9 \\ -67 & 25 \cdot 5 \end{array} $	E. by s.	+ 4 + 4 + 4 + 4	_35 _35 _35 _35	$ \begin{array}{c cccc} -69 & 11 \\ -69 & 02 \\ -69 & 15 \end{array} $	Table steady.
	-	G.	Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	$ \begin{vmatrix} -68 & 06 \cdot 1 \\ -67 & 57 \cdot 8 \\ -68 & 01 \cdot 6 \\ -68 & 22 \cdot 7 \\ -68 & 14 \cdot 3 \end{vmatrix} $	E. by s.	+ 4 + 4 + 4 + 4	-35 -35 -35 -35 -35	-68 37 -68 29 -68 33 -68 54 -68 45	i di
6.	-49 50	190 46	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by s.	+ 4 + 4 + 4 + 4 + 4	-35 -81 -35 -35 -35	-68 44 -68 40 -68 41 -68 38 -68 36	
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Mag. S. Direct. Direct. Direct. Def. N.	$\begin{array}{c} -68 & 21 \cdot 5 \\ -68 & 16 \cdot 3 \\ -68 & 09 \cdot 8 \\ -68 & 17 \cdot 0 \\ -67 & 22 \cdot 2 \end{array}$	E. by s.	+ 4 + 4 + 4 + 4 + 4	_35 _35 _35 _35 _35 _81	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Swell from north- ward. Table steady.
		а	Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{c cccc} -68 & 16.8 \\ -68 & 09.2 \\ -68 & 08.4 \\ -68 & 18.2 \end{array} $	e. by s. e. by s. e. by s.	+ 4 + 4 + 4 + 4	_35 _35 _35	-68 48 -68 40 -68 39 -68 49	

				Observed		Correc	ctions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 7.	_ s°0 32	191 52	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by e. s.e. by e. s.e. by e. s.e. by e.	-27 -27 -27 -27 -27 -27	-35 -81 -35 -35 -35	$ \begin{array}{c cccc} -69 & 26 \\ -69 & 35 \\ -69 & 20 \\ -69 & 04 \\ -68 & 52 \end{array} $	
	-50 45	192 19	Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$\begin{array}{c} -68 & 07.9 \\ -68 & 28.1 \\ -68 & 31.2 \\ -67 & 31.3 \\ -68 & 08.4 \\ -68 & 39.3 \end{array}$	s.e. by e. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e.		-35 -35 -35 -81 -35 -35	$ \begin{vmatrix} -69 & 10 \\ -69 & 30 \\ -69 & 41 \\ -69 & 27 \\ -69 & 18 \\ -69 & 49 \end{vmatrix} $	Table steady,
8.	-51 37	194 00	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S.	$ \begin{array}{r} -68 \ 30.9 \\ -68 \ 13.2 \\ -68 \ 30.3 \\ -69 \ 18.9 \\ -68 \ 23.8 \\ -69 \ 20.4 \end{array} $	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. E. by S. E. by S.	$ \begin{array}{r} -35 \\ -35 \\ -35 \\ +4 \\ +4 \\ +4 \end{array} $	$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -31 \\ -35 \\ \end{array} $	$ \begin{bmatrix} -69 & 41 \\ -69 & 23 \\ -69 & 40 \end{bmatrix} $ $ \begin{bmatrix} -69 & 50 \\ -69 & 41 \\ -69 & 51 \end{bmatrix} $	
	-52 00	194 53	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct.	$ \begin{array}{r} -69 & 19.6 \\ -69 & 13.8 \\ -69 & 31.4 \\ -69 & 22.4 \\ -69 & 24.6 \\ -69 & 29.8 \end{array} $	E. by s.	+ 4 + 4 + 4 + 4 + 4	-35 -35 -35 -35 -35 -35	$ \begin{vmatrix} -69 & 51 \\ -69 & 45 \\ -70 & 02 \\ -69 & 53 \\ -69 & 56 \\ -70 & 01 \end{vmatrix} $ $ \begin{vmatrix} -69 & 51 \\ -69 & 51 \\ -69 & 51 \end{vmatrix} $	7
	-02 00	134 00	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{c cccc} -68 & 30 \cdot 1 \\ -69 & 17 \cdot 1 \\ -69 & 08 \cdot 9 \\ -69 & 11 \cdot 7 \\ -69 & 29 \cdot 7 \end{array} $	E. by s.	+ 4 + 4 + 4 + 4 + 4	-81 -35 -35 -35	$ \begin{array}{c cccc} -69 & 47 \\ -69 & 48 \\ -69 & 40 \\ -69 & 43 \\ -70 & 01 \\ -69 & 58 \end{array} $	Table steady,
9.	-52 14	197 49	Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{r} -69 & 27.0 \\ -69 & 41.0 \\ -68 & 37.6 \\ -69 & 29.3 \\ -69 & 38.3 \\ -69 & 56.9 \\ -69 & 35.8 \end{array} $	E. by s.	+ 4 + 4 + 4 + 4 + 4 + 4	-35 -35 -81 -35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	differently.
10.	-52 32 $-53 01$	198 31 202 16	Direct. Direct. Direct. Mag. N.S.	$ \begin{vmatrix} -69 & 42.6 \\ -69 & 41.2 \\ -69 & 47.1 \\ -69 & 19.7 \end{vmatrix} $	E. by s. E. by s. E. by s. E. by s.	$\begin{vmatrix} + & 4 \\ + & 4 \\ + & 4 \\ + & 4 \end{vmatrix}$	-35 -35 -35 -35	$ \begin{array}{c cccc} & -70 & 14 \\ & -70 & 12 \\ & -70 & 18 \\ & -69 & 51 \end{array} $	Motion quick, steering wild. Strong wind, beavy sea. Motion violent,
11.	-52 51	203 56	Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-69 56·5 -69 53·3 -68 59·6 -69 59·1 -69 36·5 -69 30·2 -69 55·8	E. by s. E. ½ N.	$ \begin{array}{r} +26 \\ +26 \\ +26 \\ +26 \\ \end{array} $	-35 -35 -81 -35 -35 -35 -35	$ \begin{array}{c cccc} -70 & 28 \\ -70 & 02 \\ -69 & 55 \\ -70 & 08 \\ -69 & 45 \\ -69 & 39 \\ -70 & 05 \end{array} $	steering well. Head sea, table not very steady.
12.	—52 53	205 07	Direct. Direct. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$\begin{array}{c} -69 & 53.8 \\ -70 & 04.7 \\ -70 & 00.9 \\ -69 & 14.2 \\ -67 & 53.9 \\ -68 & 55.7 \\ -68 & 45.1 \\ -68 & 19.8 \\ -68 & 53.5 \end{array}$	E. ½ N. E. ½ N. E. ½ S. E. S.E E.S.E. E.S.E. E.S.E. E.S.E.	$ \begin{array}{r} +26 \\ +12 \\ -12 \\ -12 \\ -12 \\ -12 \\ -12 \\ \end{array} $	-35 -35 -35 -35 -35 -35 -35 -35	-70 05 -70 14 -70 24 -70 01 -69 27 -69 43 -69 32 -69 07 -69 41	A head swell, steering well.
	-53 12	205 40	Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.S.E. E.S.E.	-12	-35 -35	$ \begin{array}{c c} -70 & 03 \\ -70 & 06 \end{array} $ \rightarrow -69 \ 52	J

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	True Inclination.	Remarks.
Dec. 12.		206 14	Direct. Def. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.S.E. E.S.E.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Table steady, steering wild.
			Def. S. Mag. N. Mag. N.S.	$ \begin{array}{rrrrr} -69 & 05.5 \\ -69 & 07.0 \\ -69 & 01.4 \\ -69 & 58.3 \end{array} $	E.S.E. E.S.E. E.S.E.	$ \begin{vmatrix} -12 & -35 \\ -12 & -35 \\ -12 & -35 \\ -12 & -35 \end{vmatrix} $	$egin{array}{c c} -69 & 53 \\ -69 & 54 \\ -69 & 51 \\ -70 & 45 \\ \end{array}$	A slight motion, steering well.
13.	-54 19	208 24	Mag. S. Direct. Direct. Def. N.	$ \begin{array}{r rrrr} -69 & 19.5 \\ -69 & 18.1 \\ -68 & 59.2 \end{array} $	E.S.E. E.S.E. E.S.E.	$\begin{vmatrix} -12 & -35 \\ -12 & -35 \\ -12 & -81 \end{vmatrix}$	$egin{pmatrix} -70 & 06 \ -70 & 05 \ -70 & 32 \ \end{pmatrix}$	
			Def. S. Mag. N. Mag. N.S. Mag. S.	$ \begin{array}{rrrrr} -69 & 02.6 \\ -69 & 16.0 \\ -69 & 16.0 \\ -69 & 14.0 \end{array} $	E.S.E. E.S.E. E.S.E.	$ \begin{array}{c cccc} -12 & -35 \\ -12 & -35 \\ -12 & -35 \\ -12 & -35 \end{array} $	$ \begin{vmatrix} -69 & 50 \\ -70 & 03 \\ -70 & 03 \\ -70 & 01 \end{vmatrix} -70 & 10$	Table steady,
	-54 53	209 24	Direct. Direct. Def. N. Def. S.	$ \begin{array}{c cccc} -69 & 16.6 \\ -69 & 32.9 \\ -68 & 59.0 \\ -69 & 28.8 \end{array} $	E.S.E. E.S.E. E.S.E.	$ \begin{vmatrix} -12 & -35 \\ -12 & -35 \\ -12 & -81 \\ -12 & -35 \end{vmatrix} $	$\begin{bmatrix} -70 & 04 \\ -70 & 20 \\ -70 & 32 \\ -70 & 16 \end{bmatrix}$	steering whaty.
			Mag. N.S. Mag. S.	$ \begin{vmatrix} -69 & 13.4 \\ -69 & 24.6 \\ -70 & 00.3 \end{vmatrix} $	E.S.E. E.S.E. E.S.E.	$\begin{vmatrix} -12 & -35 \\ -12 & -35 \\ -12 & -35 \end{vmatrix}$	$egin{array}{ccc} -70 & 00 \ -70 & 12 \ -70 & 47 \ \end{array}$	
de colocomitica d'aveniment de la fermanda del la fermanda de la f			Direct. Direct. Def. N. Direct.	$ \begin{vmatrix} -69 & 32.6 \\ -69 & 39.5 \\ -68 & 55.8 \\ -68 & 52.9 \end{vmatrix} $	E.S.E. E.S.E. E.S.E. S.E. by S.	$ \begin{vmatrix} -12 & -35 \\ -12 & -35 \\ -12 & -81 \\ -55 & -35 \end{vmatrix} $	$ \begin{vmatrix} -70 & 20 \\ -70 & 27 \\ -70 & 29 \\ -70 & 23 \end{vmatrix} $	A heavy sea, ship steering badly. A swell from the
Management of the Committee of the Commi			Def. N. Def. S. Mag. N.	$ \begin{vmatrix} -68 & 11.4 \\ -68 & 27.0 \\ -68 & 59.1 \end{vmatrix} $	s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -55 & -81 \\ -55 & -35 \\ -55 & -35 \end{vmatrix} $	$ \begin{vmatrix} -70 & 27 \\ -69 & 57 \\ -70 & 29 \end{vmatrix} $	N.W. Ship tolerably
14.	-56 14	211 43	Mag. N.S. Mag. S. Direct. Direct.	$ \begin{array}{r rrrr} -68 & 46.1 \\ -68 & 34.0 \\ -68 & 52.1 \\ -70 & 08.2 \end{array} $	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -55 & -35 \\ -55 & -35 \\ -55 & -35 \\ -57 & -35 \end{vmatrix} $	$ \begin{bmatrix} -70 & 16 \\ -70 & 04 \\ -70 & 22 \\ -71 & 40 \end{bmatrix} $	steady.
			Def. N. Def. S. Mag. N.	$ \begin{array}{c cccc} -69 & 12.9 \\ -70 & 10.1 \\ -70 & 03.2 \\ -70 & 06.2 \end{array} $	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -57 & -81 \\ -57 & -35 \\ -57 & -35 \\ -57 & -35 \end{vmatrix} $	$ \begin{vmatrix} -71 & 31 \\ -71 & 42 \\ -71 & 35 \\ -71 & 38 \end{vmatrix} $)
Section 200 Val. Heinellanderson			Mag. N.S. Mag. S. Direct. Direct.	$ \begin{array}{r rrrr} -70 & 22.0 \\ -70 & 16.1 \\ -70 & 17.8 \end{array} $	s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -57 & -35 \\ -57 & -35 \\ -57 & -35 \end{vmatrix} $	$ \begin{vmatrix} -71 & 54 \\ -71 & 48 \\ -71 & 50 \end{vmatrix} -71 & 41$	Snip steady,
AND THE PROPERTY OF THE PROPER			Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{vmatrix} -69 & 11.7 \\ -70 & 12.1 \\ -70 & 04.2 \\ -70 & 00.2 \end{vmatrix} $	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -57 & -81 \\ -57 & -35 \\ -57 & -35 \\ -57 & -35 \end{vmatrix} $	$ \begin{bmatrix} -71 & 30 \\ -71 & 44 \\ -71 & 36 \\ -71 & 32 \end{bmatrix} $	
	56 30	211 50	Mag. S. Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by s. s.e. by s. s.e. by s.	$\begin{vmatrix} -57 & -35 \\ -57 & -35 \\ -57 & -35 \end{vmatrix}$	$\begin{bmatrix} -71 & 54 \\ -71 & 49 \\ -71 & 52 \end{bmatrix}$	
	To a propagation of the control of t		Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{array}{rrrrr} -69 & 29.1 \\ -70 & 12.7 \\ -70 & 05.2 \\ -69 & 59.7 \end{array} $	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	$ \begin{vmatrix} -57 & -81 \\ -57 & -35 \\ -57 & -35 \\ -57 & -35 \end{vmatrix} $	$ \begin{bmatrix} -71 & 47 \\ -71 & 45 \\ -71 & 37 \\ -71 & 32 \end{bmatrix} $	
15.	_56 53	212 06	Mag. S. Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.E. by s. s.E. by s. s. s. by E.	$\begin{vmatrix} -57 & -35 \\ -57 & -35 \\ -77 & -35 \\ -75 & -35 \end{vmatrix}$	-72 07 \ -72 00	Ship steady.
-			Direct. Direct. Def. N.	$ \begin{array}{rrrr} -70 & 30 & 3 \\ -70 & 27 \cdot 5 \\ -70 & 30 \cdot 8 \\ -69 & 33 \cdot 8 \end{array} $	s. by E. s.e. by s. s.e. by s.		$\begin{bmatrix} -72 & 12 \\ -72 & 03 \end{bmatrix}$	

				Observed		Correc	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 15.	$-\overset{\circ}{56}\overset{\prime}{53}$	21°2 06	Def. S. Mag. N. Mag. N.S.	$ \begin{vmatrix} -70 & 26.1 \\ -70 & 12.5 \\ -70 & 09.6 \end{vmatrix} $	s.e. by s. s.e. by s. s.e. by s.	-57 -57 -57	-35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
,	-57 16	212 17	Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$\begin{array}{c cccc} -70 & 34.0 \\ -70 & 30.6 \\ -70 & 37.3 \\ -70 & 00.6 \\ -70 & 54.6 \\ -70 & 49.7 \end{array}$	s.e. by s. s.e. by s. s.s.e. s.s.e. s.s.e. s.s.e.	-57 -57 -69 -69 -69	-35 -35 -81 -35 -35	$ \begin{vmatrix} -72 & 06 \\ -72 & 03 \\ -72 & 21 \\ -72 & 31 \\ -72 & 39 \\ -72 & 34 \end{vmatrix} $	Ship very steady,
16.	—57 44	212 59	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$\begin{array}{c cccc} -70 & 25 \cdot 1 \\ -70 & 46 \cdot 1 \\ -70 & 41 \cdot 5 \\ -71 & 03 \cdot 3 \\ -70 & 29 \cdot 6 \\ -71 & 08 \cdot 2 \\ -71 & 09 \cdot 6 \end{array}$	S.S.E. S.S.E. S.S.E. S.S.E. S.S.E. S.S.E.		$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -81 \\ -35 \\ \end{array} $	$egin{array}{cccc} -72 & 09 \ -72 & 30 \ -72 & 26 \ \end{array} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	
	—58 28	213 08	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$ \begin{vmatrix} -71 & 02.8 \\ -71 & 15.7 \\ -71 & 11.9 \\ -71 & 56.4 \\ -71 & 20.8 \\ -71 & 52.3 \\ -71 & 39.7 \end{vmatrix} $	S.S.E. S.S.E. S.S.E. S.S.E. S.S.E. S.S.E.	$ \begin{bmatrix} -70 \\ -70$	-35 -35 -35 -35 -81 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ship steady, steering well.
*	58 44	213 11	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	$\begin{array}{ c c c c }\hline -71 & 23.9 \\ -71 & 59.3 \\ -72 & 04.4 \\ -72 & 16.2 \\ -71 & 24.5 \\ -72 & 22.6 \\ -71 & 57.1 \\ \hline \end{array}$	S.S.E. S.S.E. S.S.E. S.S.E. S.S.E.	$ \begin{bmatrix} -70 \\ -70$	-35 -35 -35 -35 -81 -35 -35	$egin{array}{cccc} -73 & 09 & & & & & \\ -73 & 44 & & & & & \\ -73 & 49 & & & & & \\ -74 & 01 & & & & & \\ \end{array}$	Ship steady, steering well.
17.	-60 48	213 51	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	-71 47·8 -72 01·3 -72 16·1 -73 24·1 -72 33·2 -73 29·4 -73 01·5	S.S.E. S.S.E. S.S.E. S.S.E. S.S.E. S.S.E.	-70 -70 -70 -73 -73 -73 -73	-35 -35 -35 -35 -81 -35 -35	$egin{array}{cccccccccccccccccccccccccccccccccccc$	Slight motion, steering well.
	—61 3 7	213 54	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c} -73 & 04\cdot2 \\ -73 & 31\cdot1 \\ -73 & 28\cdot8 \\ -74 & 10\cdot9 \\ -73 & 06\cdot9 \\ -73 & 59\cdot8 \\ -73 & 52\cdot8 \\ -73 & 39\cdot5 \end{array}$	S.S.E. S.S.E. S.S.E. S. \frac{1}{2} E. S. \frac{1}{2} E. S. \frac{1}{2} E.	-73 -73 -73 -81 -81 -81 -81	-35 -35 -35 -35 -81 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ship steady,
18.	-62 34	212 34	Mag. S. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	-74 08·6 -74 13·1 -74 51·6 -73 48·3 -74 43·7 -74 23·1 -74 23·9	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. by E. S. by E. S. by E. S. by E.	-81 -81 -79 -79 -79 -79 -79	-35 -35 -35 -81 -35 -35 -35	-70 18 (la	Ship steady, sailing amongst loose ice.
	-62 51	212 50	Mag. S. Direct. Direct.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by E. s. by E. s. by w.		$ \begin{array}{r r} -35 \\ -35 \\ -35 \end{array} $	$ \begin{array}{c c} -76 & 33 \\ -76 & 40 \\ -77 & 14 \end{array} $	

						Correc	etions.		
1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 19.	_63 o6	210 55	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.w.	$-74 \\ -80$	-35 -35	$ \begin{array}{c c} -77 & 41 \\ -77 & 40 \end{array} $	
			Def. N. Def. S.	-74 56.9 $-75 35.6$	s. by w.	$-80 \\ -80$	$-81 \\ -35$	$ \begin{bmatrix} -77 & 38 \\ -77 & 31 \end{bmatrix} $	
			Mag. N.	-75 24.5	s. by w.	-80	-35	-77 20	
			Mag. N.S.	-75 21·2	s. by w.	-80	$-35 \\ -35$	$\begin{vmatrix} -77 & 16 \\ -77 & 33 \end{vmatrix}$ $-77 & 37$	Ship steady, sailing
			Mag. S. Direct.	$\begin{vmatrix} -75 & 37.8 \\ -75 & 51.8 \end{vmatrix}$	s. by w.	$-80 \\ -80$	$-35 \\ -35$	$-77 \ 33$ $-77 \ 47$	amongst loose ice.
1	-63 21	209 55	Direct.	-76 08.3	s.w. by s.	-62	-35	$-77 \ 45$	
			Direct.	-76 00.0	$s.s.w.\frac{1}{2}w.$	-68	-35	$ -77 \ 43 $	
			Direct.	-77 00·8	w. by s. $\frac{3}{4}$ s.		-35	$\left(\begin{array}{cc} -77 & 48 \\ -77 & 36 \end{array} \right)$	
20.	-63 36	208 20	Direct. Direct.	$\begin{vmatrix} -76 & 36.2 \\ -76 & 13.7 \end{vmatrix}$	s.w.byw.½w. s.s.w.	$-25 \\ -74$	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	$\begin{bmatrix} -77 & 30 \\ -78 & 03 \end{bmatrix}$	
~0.	-00 00	200 20	Def. N.	$-75\ 10.8$	s.s.w.	-74	-81	-77 46	
			Def. S.	-76 04.8	s.s.w.	-74	-35	-7754	
1			Mag. N.	$-75 \ 45.5$	s.s.w.	-74	-35	-77 35 77 34	;
	1.0		Mag. N.S. Mag. S.	$\begin{vmatrix} -75 & 44.8 \\ -76 & 08.0 \end{vmatrix}$	S.S.W.	$\begin{vmatrix} -74 \\ -74 \end{vmatrix}$	$-35 \\ -35$	$\left \begin{array}{c} -77 & 34 \\ -77 & 57 \end{array} \right -77 53$	Ship steady, steer- ing amongst loose
			Direct.	-76 013	s. by w.	_80	-35	-77 56	ice.
			Direct.	-76 24.9	s.w. by s.	-62	-35	-78 02	
			Direct.	-76 00.4	s.	-82	-35	-77 57	
			Direct.	$\begin{vmatrix} -76 & 45.2 \\ -76 & 24.3 \end{vmatrix}$	S.W.	$\begin{vmatrix} -49 \\ -62 \end{vmatrix}$	$-35 \\ -35$	$\begin{bmatrix} -78 & 09 \ -78 & 01 \end{bmatrix}$	
1			Direct. Direct.	-76 24.3 $-76 45.5$	s.w. by s.	-49	-35	$\begin{bmatrix} -78 & 01 \\ -78 & 10 \end{bmatrix}$	
	-63 53	208 32	Direct.	-76 069	s.	-82	-35	-78 04	
1			Def. N.	-75 01.3	s.	-82	-81	-77 44	
1			Def. S.	-75 53·4	s.	$-82 \\ -82$	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	$\left \begin{array}{c} -77 & 50 \\ -77 & 42 \end{array} \right\} -77 56$	Ship steady, steer-
1			Mag. N. Mag. N.S.	$\begin{vmatrix} -75 & 44.5 \\ -75 & 36.8 \end{vmatrix}$	s. s.	-82	-35	$\begin{vmatrix} -77 & 42 \\ -77 & 34 \end{vmatrix}$	ing amongst loose ice.
1			Mag. S.	-75 57.7	s.	_82	-35	-77 55	
l			Direct.	-76 08.9	s.	_82	-35	-78 06	
	2.		Direct.	$-76\ 15.3$	s. by w.	-80	-35	$\begin{bmatrix} -78 & 10 \end{bmatrix}$	*
21	-64 11	206 35	Direct.	$\begin{vmatrix} -76 & 32.9 \\ -75 & 31.5 \end{vmatrix}$	s.s.w.	$-75 \\ -75$	$-35 \\ -81$	$\begin{bmatrix} -78 & 23 \\ -78 & 08 \end{bmatrix}$	
1			Def. N. Def. S.	-76 29.6	s.s.w.	-75	-35	-78 20	
1			Mag. N.	-76 10·0	s.s.w.	_75	-35	-78 00	
		4	Mag. N.S.	-76 01.2	s.s.w.	-75	-35	-7751	
			Mag. S.	$-76\ 00.8$	s.s.w.	$\begin{vmatrix} -75 \\ -82 \end{vmatrix}$	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	$\begin{bmatrix} -77 & 51 \\ -78 & 40 \end{bmatrix}$	
		-	Direct. Direct.	$\begin{vmatrix} -76 & 43.1 \\ -76 & 32.7 \end{vmatrix}$	s. $\frac{1}{2}$ E. s. by E.	-81			Ship steady, sailing amongst loose ice.
1			Direct.	-76 41.8	s. by E. $\frac{1}{2}$ E.	-78	-35	-78 35	
	-64 51	206 19	Direct.	-77 03.2	S. $\frac{3}{4}$ E.	-82	-35	-7900	
			Direct.	-77 06.4	s. by w.	-81	$-35 \\ -81$	$\begin{bmatrix} -79 & 02 \\ -78 & 49 \end{bmatrix}$	
			Def. N. Def. S.	$\begin{vmatrix} -76 & 06.6 \\ -77 & 02.2 \end{vmatrix}$	s. by w.	-81 -81	-35	-78 49 -78 58	
1			Direct.	-77 04.7	s. by w.	-81	-35	$-79 \ 01$	
22	-65 19	205 08	Direct.	-7729.4	$S \cdot \frac{1}{2} W \cdot$	_83		-79 27	
			Def. N.	$-76 \ 37.6$	S. ½ W.	-83		-79 22	
1			Def. S. Mag. N.	$\begin{vmatrix} -77 & 20.3 \\ -77 & 08.4 \end{vmatrix}$	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W.	$-83 \\ -83$	$-35 \\ -35$	$\begin{vmatrix} -79 & 18 \\ -79 & 06 \end{vmatrix}$	
			Mag. N.S.	-76 59.9	$S \cdot \frac{1}{2} W \cdot S \cdot \frac{1}{2} W \cdot$	-83		-78 58	
1			Mag. S.	-77 30.4	$S \cdot \frac{1}{2} W$	-83	-35	-79 28	
			Direct.	-77 28·6	S. 1/2 W.	-83		-79 27 70 25	
	_65 3/	205 00	Direct.	$\begin{vmatrix} -77 & 26.4 \\ -77 & 27.8 \end{vmatrix}$	s. s.	-84 -84	1	$\begin{bmatrix} -79 & 25 \\ -79 & 27 \end{bmatrix}$	guillian a surround
1	00 07	~00 00	Def. N.	-76 20.5	s.	-84		$ -79 \ 05 > -79 \ 16$	Sailing amongst loose ice, very
1		1	Dei. N.	-10 20.9	s.	-04	-01	-13 00 7-13 10	steady.

				Observed		Correct	tions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 22.	$-65\ 34$	205 00	Def. S. Mag. N.	-77 14.7 $-77 04.0$	S• S•	-84 -84	$-35 \\ -35$	$-\mathring{79} \stackrel{1}{14} > -\mathring{79} \stackrel{1}{16} \\ -79 \stackrel{1}{03} > -\mathring{79} \stackrel{1}{16}$	Sailing amongst loose ice, very
			Mag. N.S. Mag. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. s.	$-84 \\ -84$	$-35 \\ -35$	$ \begin{array}{rrr r} -78 & 52 \\ -79 & 23 \end{array} $	steady.
23.	65 47	204 19	Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S. $\frac{3}{4}$ W. N.E. N.E. $\frac{1}{2}$ E.	+69	$-35 \\ -35 \\ -35$	$egin{array}{cccc} -79 & 27 \ -79 & 21 \ -79 & 17 \ \end{array}$	
			Direct. Direct. Def. N.	$ \begin{array}{rrr} -79 & 30.8 \\ -77 & 34.8 \\ -76 & 44.1 \end{array} $	s.	-84	$-35 \\ -35 \\ -81$	$egin{array}{c c} -79 & 07 \\ -79 & 34 \\ -79 & 29 \\ \end{array}$	6
	·		Direct. Def. S.		е. by n. е. by n.	+32 +32	$-35 \\ -35$	$ \begin{array}{c c} -79 & 15 \\ -79 & 08 \end{array} $ $ \begin{array}{c c} -79 & 26 \end{array} $	Sailing amongst loose ice, very
			Mag. N.S. Mag. S. Direct.	$ \begin{vmatrix} -78 & 44.5 \\ -77 & 15.9* \\ -78 & 10.8 \end{vmatrix} $	E. by N. E. by N. s.w. $\frac{1}{4}$ s.	+32	$-35 \\ -35 \\ -35$	$egin{array}{c c} -78 & 48 & \\ -77 & 19 & \\ -79 & 41 & \\ \end{array}$	steady.
			Direct. Def. N. Direct.	$ \begin{array}{rrrr} -77 & 46 \cdot 2 \\ -77 & 23 \cdot 0 \\ -77 & 45 \cdot 1 \end{array} $	s. by w. s. by w. s. \frac{1}{4} w.	-82	$-35 \\ -81 \\ -35$	$egin{array}{c c} -79 & 43 \\ -80 & 06 \\ -79 & 43 \\ \end{array}$	-
		*	Direct. Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. 3/4 W. s.s.w.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-35 -35	$\begin{bmatrix} -79 & 42 \\ -79 & 49 \end{bmatrix}$	
			Direct. Direct.	$\begin{vmatrix} -79 & 51 \cdot 1 \\ -79 & 57 \cdot 6 \end{vmatrix}$	S. N.E. $\frac{1}{2}$ E. N.E.	+63 +69	$-35 \\ -35 \\ -35$	$egin{array}{c c} -79 & 33 & \\ -79 & 23 & \\ -79 & 24 & \\ \end{array}$	
		-	Direct. Direct. Direct.	$ \begin{vmatrix} -79 & 32 \cdot 1 \\ -78 & 18 \cdot 6 \\ -78 & 14 \cdot 3 \end{vmatrix} $	N.E. by E. $\frac{1}{2}$ E. s.E. by E. $\frac{1}{2}$ E. s.E. by E.	-27	$-35 \\ -35 \\ -35$	$\left \begin{array}{c} -79 & 15 \\ -79 & 21 \\ -79 & 25 \end{array} \right -79 \ 28$	Sailing amongst loose ice, very steady.
			Direct. Direct. Direct.	$ \begin{vmatrix} -78 & 23.0 \\ -80 & 26.0 \\ -80 & 03.9 \end{vmatrix} $	e.s.e. n. n.e. by n.	+86	$-35 \\ -35 \\ -35$	$egin{array}{c c} -79 & 15 \\ -79 & 35 \\ -79 & 24 \\ \end{array}$	
24.	65 50	004.00	Direct. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	n.n.e. n. by e.	$ +81 \\ +85 $	$-35 \\ -35$	$\begin{bmatrix} -79 & 26 \\ -79 & 29 \end{bmatrix}$	
24.	65 50	204 08	Direct. Direct. Def. N.	$ \begin{vmatrix} -80 & 31.9 \\ -80 & 28.8 \\ -79 & 26.9 \end{vmatrix} $	n. by w. n. by w. n. by w.	+85 +85	$-35 \\ -35 \\ -81$	$\left egin{array}{c} -79 & 42 \ -79 & 39 \ -79 & 23 \ \end{array} \right $	
			Mag. S. Mag. N. Mag. N.S.	$ \begin{array}{c cccc} -80 & 21.4 \\ -80 & 08.5 \\ -80 & 00.0 \end{array} $	n. by w. n. by w. n. by w.	+85	-35 -35 -35	$ \begin{vmatrix} -79 & 31 \\ -79 & 19 \\ -79 & 10 \end{vmatrix} -79 & 30$	Ship fast to a piece
			Direct. Mag. S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.E. N.E. N.N.W.	+69 +69	$-35 \\ -35 \\ -35$	$\begin{bmatrix} -79 & 28 \\ -79 & 17 \end{bmatrix}$	of ice,
ø s	_66·01	204 00	Direct. Direct.	$ \begin{vmatrix} -80 & 29.2 \\ -79 & 01.3 \end{vmatrix} $	N.W.	+69 + 16	$-35 \\ -35$	$ \begin{bmatrix} -79 & 44 \\ -79 & 55 \\ -79 & 19 \end{bmatrix} $	
<i>2</i> .0•	-00 01	204 00	Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by N. E. $\frac{3}{4}$ S. N.W. $\frac{1}{4}$ N.	+ 4 + 70	-35 -35 -35	$egin{array}{c c} -79 & 12 \\ -79 & 28 \\ -79 & 56 \\ \end{array}$	
26.	-65 57	204 27	Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by s. $\frac{3}{4}$ s. N. by w. N.W. $\frac{3}{4}$ W.	+85	$-35 \\ -35 \\ -35$	$\left \begin{array}{c} -79 & 26 \\ -79 & 49 \\ -80 & 06 \end{array} \right -79 \ 39$	Sailing amongst ice very steady.
27.	_66 08	203 50	Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. E.S.E. E.S.E.	$\begin{vmatrix} -51 \\ -18 \end{vmatrix}$	$-35 \\ -35 \\ -35$	$\begin{bmatrix} -79 & 47 \\ -79 & 32 \\ -79 & 37 \end{bmatrix}$	
		Annual designation of the control of	Direct. Def. N. Def. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by s. E.S.E. E.S.E.	$\begin{vmatrix} -1 \\ -18 \end{vmatrix}$	-35 -81 -35	$\left \begin{array}{cc} -79 & 36 \\ -79 & 17 \end{array} \right $	
			Direct.	-80 38·3	n.w. by n.	$\begin{vmatrix} -18 \\ +75 \end{vmatrix}$		$\begin{vmatrix} -79 & 23 \\ -79 & 58 \end{vmatrix}$ $\rightarrow -79 & 39$	Sailing amongst ice very steady.

^{*} The result is omitted in the mean, as it differs so widely from all others of the same period.

				Observed		Corre	ctions.		
1841.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Dec. 27.	−6°6 0′8	203 50	Mag. N. Mag. N.S. Mag. S. Direct.	-80 16·1 -79 58·1 -80 34·0 -78 03·0	n.w. by n. n.w. by n. n.w. by n. s. by E.	+75 +75 +75 +83	-35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sailing amongst ice, very steady.
28.	-66 10	202 54	Direct. Direct. Def. N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by N. w. by N.		$-35 \\ -35 \\ -81$	$egin{array}{ccc} -79 & 48 iggr \\ -80 & 03 \iggr \\ -79 & 42 \iggr \end{array}$	
	-66 11	202 54	Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c c} N. \frac{1}{2} W. \\ s.w. by s. \end{array}$	$+85 \\ -65$	$-35 \\ -35$	$ \begin{array}{c c} -80 & 00 \\ -80 & 09 \end{array} $	
29.	-66 20	203 20	Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. N.W. ½ W. N.W.	$+16 \\ +64 \\ +69$	$-35 \\ -35 \\ -35$	$ \begin{array}{c ccccc} -79 & 42 \\ -80 & 15 \\ -80 & 14 \end{array} $	g.:
30.	-66 25	203 12	Direct. Direct. Direct. Direct. Direct. Direct.	-79 26·8 -79 24·7 -81 13·2 -79 45·3 -79 59·8 -80 09·2	E. ½ N. E. by s. N. w. by N. E. E. by N. E.N.E.	$ \begin{array}{r} +24 \\ 0 \\ +75 \\ +16 \\ +32 \\ +46 \end{array} $	-35 -35 -35 -35 -35 -35	-79 38 -80 00 -80 33 -80 04 -80 03 -79 58	Sailing amongst ice, very steady.
31.	-66 30	203 08	Direct. Direct. Direct. Direct. Direct. Direct. Direct.	-80 14·0 -81 15·6 -81 17·6 -81 15·5 -81 10·2 -81 11·8 -80 28·6	N.E. by E. $\frac{1}{2}$ E. N. by W. N. $\frac{1}{2}$ W. N. $\frac{1}{2}$ E. N. by E. W. $\frac{1}{2}$ N.		-35 -35 -35 -35 -35 -35	-79 57 \ -80 26 \ -80 28 \ -80 25 \ -80 20 \ -80 22	Fast to a piece of ice: Erebus fast to the same piece distant fifty yards. Ter- ror's head to North*. Erebus bearing E.
1842. Jan. 1.	66 36	203 29	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-81 14·8 -80 22·2 -81 06·3 -81 03·7 -80 50·7 -81 01·3 -81 15·4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+64 +64 +64 +64 +64 +64 +64	-35 -81 -35 -35 -35 -35 -35	-80 46 -80 39 -80 37 -80 34 -80 22 -80 32 -80 46	Ditto; Erebus N. Ditto; Erebus N. E.
2. 3.			Direct. Direct. Direct. Direct. Direct.	$ \begin{vmatrix} -81 & 12.4 \\ -78 & 46.1 \\ -78 & 26.1 \end{vmatrix} $	N.W. $\frac{1}{2}$ W. N. $\frac{1}{2}$ W. S.E. S. by W. s. by W. $\frac{1}{2}$ W.	+85 -52 -83	-35 -35 -35 -35	-80 22 -80 13 -80 24	Ditto; Erebus E.
5. 6.	$-66 \ 14$ $-66 \ 09$	203 17 203 58	Direct. Direct. Direct.	$ \begin{array}{rrrr} -79 & 36.7 \\ -77 & 46.2 \\ -80 & 15.8 \end{array} $	E. ½ S. S. ¾ W. N. ¾ E.	$ \begin{array}{r} -83 \\ -85 \end{array} $	$-35 \\ -35$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Running amongst loose ice, very steady.
7.	-66 20	203 39	Direct. Def. N. Def. S.	$ \begin{array}{c cccc} -80 & 31.9 \\ -79 & 32.1 \\ -80 & 26.2 \\ -80 & 15.7 \end{array} $	N.W. N.W. N.W.	+69 +69 +69 +69	-35 -81 -35 -35	$ \begin{bmatrix} 79 & 58 \\ -79 & 44 \\ -79 & 52 \\ -79 & 42 \end{bmatrix} $	
8.	66 05	204 02	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct. Direct.	-80 05·8 -80 34·5 -80 37·9 -79 53·0 -78 00·9	N.W. N.W. N.W. s. s. by E. s. by W. ½ W.	$ \begin{array}{r} +69 \\ +69 \\ +69 \\ -85 \\ -83 \end{array} $	-35 -35 -35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Running amongst loose ice, very steady.
5			Direct. Def. N. Def. S. Mag. N.	-80 44·1 -79 45·4 -80 41·6 -80 27·8	N. N. N.	+86 +86 +86 +86	$-35 \\ -81 \\ -35$	$ \begin{array}{c cccc} -79 & 53 \\ -79 & 40 \\ -79 & 51 \\ -79 & 37 \end{array} $ $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Running amongst loose ice, very steady.

^{*} These observations are omitted in the general table of results, and in the map: the proximity of the two ships appears however to have produced scarcely any sensible effect on the inclination needle.

						Correc	etions.		
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Jan. 8.	-66 ó 5	204 02	Mag. N.S. Mag. S. Direct. Direct.	-80 20.7 -80 46.2 -80 45.4 -78 00.6	N. N. N. s. by E.	+ 86 + 86 + 86 - 83	-35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Running amongst loose ice, very steady.
	0		Direct. Direct. Direct. Direct.	$ \begin{vmatrix} -78 & 25.8 \\ -80 & 40.4 \\ -80 & 43.1 \\ -79 & 10.0 \end{vmatrix} $	s.w. by s. N. by w. N. E. $\frac{1}{2}$ s.	$-65 \\ +85 \\ +86 \\ +8$	-35 -35 -35 -35	$ \begin{array}{c cccc} -80 & 06 \\ -79 & 50 \\ -79 & 52 \\ -79 & 37 \end{array} $	
9.	-66 01	204 04	Direct. Direct.	$ \begin{vmatrix} -77 & 56.0 \\ -78 & 58.2 \\ -79 & 22.2 \end{vmatrix} $	s. E. by s. E. ¹ / ₄ N.	$ \begin{array}{r} -85 \\ -1 \\ +20 \end{array} $	$-35 \\ -35 \\ -35$	$egin{array}{ccc} -79 & 56 \ -79 & 34 \ -79 & 37 \ \end{array}$	
		4	Direct. Direct. Def. N. Direct. Direct. Def. S.	$\begin{array}{c cccc} -78 & 46.0 \\ -78 & 33.8 \\ -77 & 34.8 \\ -78 & 36.3 \\ -79 & 00.8 \\ -79 & 10.9 \end{array}$	s.w. by w. s.w. $\frac{1}{2}$ w. s.w. $\frac{1}{2}$ w. s.w. w.s.w. w.s.w.	$ \begin{array}{r} -36 \\ -44 \\ -44 \\ -52 \\ -18 \\ -18 \\ \end{array} $	-35 -35 -81 -35 -35 -35	$ \begin{vmatrix} -79 & 57 \\ -79 & 53 \\ -79 & 40 \\ -80 & 03 \\ -79 & 54 \\ -80 & 04 \end{vmatrix} $ $ -79 & 50$	
10.	-65 57	203 56	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N.	$ \begin{array}{c ccccc} -78 & 28.8 \\ -78 & 24.4 \\ -78 & 48.6 \\ -78 & 45.2 \\ -79 & 03.7 \\ -79 & 30.4 \\ 78 & 23.7 \end{array} $	s.w. by w. s.w. by w. s.w. by w. s.w. by w. w.s.w. w.s.w.	$ \begin{array}{r} -36 \\ -36 \\ -36 \\ -18 \\ -1 \\ -1 \end{array} $	_35 _35 _35 _35 _35 _35	$egin{array}{cccc} -79 & 40 \\ -79 & 35 \\ -80 & 00 \\ -79 & 56 \\ -79 & 57 \\ -80 & 06 \\ 70 & 46 \\ \end{array}$	Running amongst > loose ice, very steady.
			Def. S. Mag. N. Direct. Mag. S. Mag. N.S.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by s. w. by s. w. by s. E. E.	-1 -1 $+16$ $+16$ $+16$	-81 -35 -35 -35 -35 -35	$\begin{vmatrix} -79 & 46 \\ -79 & 51 \\ -79 & 53 \\ -79 & 34 \\ -79 & 37 \\ -79 & 14 \end{vmatrix} -79 & 47$	
	-65 58	203 37	Direct. Direct. Direct. Direct. Direct.	$ \begin{array}{c cccc} -79 & 15.7 \\ -78 & 29.0 \\ -79 & 41.5 \\ -79 & 23.8 \end{array} $	S.E. by E. $\frac{1}{2}$ E. W. $\frac{1}{4}$ S. W. by S. $\frac{1}{2}$ S.	$+12 \\ -8$	-35 -35 -35 -35	$ \begin{array}{r rrrr} -79 & 35 \\ -79 & 31 \\ -80 & 05 \\ -80 & 07 \\ \end{array} $	
11.	-65 56		Direct. Direct.	$ \begin{array}{c cccc} -78 & 44.5 \\ -78 & 46.3 \\ -77 & 58.3 \end{array} $	s.w. by w. s. by E.	$ \begin{array}{r} -36 \\ -36 \\ -83 \end{array} $	-35 -35 -35	$ \begin{bmatrix} -79 & 55 \\ -79 & 57 \end{bmatrix} $ $ \begin{bmatrix} -79 & 56 \end{bmatrix} $	
			Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{vmatrix} -77 & 53 \cdot 2 \\ -76 & 51 \cdot 8 \\ -77 & 56 \cdot 7 \\ -77 & 31 \cdot 0 \\ -77 & 35 \cdot 4 \end{vmatrix} $	S. S. S.	-85 -85 -85 -85 -85	35	$ \begin{vmatrix} -79 & 53 \\ -79 & 58 \\ -79 & 57 \\ -79 & 31 \\ -79 & 35 \end{vmatrix} $ $ \begin{vmatrix} -79 & 51 \end{vmatrix} $	
12 .	-65 45 -66 06	203 23	Mag. S. Direct. Direct. Direct. Direct.	$ \begin{vmatrix} -77 & 49.3 \\ -78 & 30.4 \\ -78 & 20.6 \\ -78 & 44.4 \\ -78 & 13.7 \end{vmatrix} $	s. s.w. s.w. by s. s.w. by w.	$ \begin{bmatrix} -85 \\ -52 \\ -65 \\ -36 \\ -9 \\ \end{bmatrix} $	-35 -35 -35 -35	$ \begin{bmatrix} -79 & 49 \\ -79 & 57 \\ -80 & 01 \\ -79 & 55 \end{bmatrix} $	
10.		202 10	Direct. Direct. Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by w. s. n.n.e.		_35 _35 _35	$ \begin{bmatrix} -80 & 11 \\ -79 & 49 \\ -79 & 36 \\ 70 & 55 \end{bmatrix} $	Very steady, working about in a hole of water.
			Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$ \begin{vmatrix} -80 & 38.4 \\ -79 & 44.5 \\ -80 & 39.1 \\ -80 & 22.8 \\ -80 & 20.0 \end{vmatrix} $	N. N. \frac{1}{2} E.	+85 +85 +85 +85 +85	-35 -35 -81 -35 -35 -35	$ \begin{vmatrix} -79 & 55 \\ -79 & 48 \\ -79 & 41 \\ -79 & 49 \\ -79 & 33 \\ -79 & 30 \end{vmatrix} $ $ \begin{vmatrix} -79 & 48 \\ -79 & 36 \end{vmatrix} $	
			Mag. S. Direct. Direct. Direct.	$ \begin{vmatrix} -80 & 37.4 \\ -80 & 39.8 \\ -78 & 07.0 \\ -77 & 58.2 \end{vmatrix} $	N. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E. S.S.E. S.	+85 +85 -77 -85		$ \begin{bmatrix} -79 & 47 \\ -79 & 50 \\ -79 & 59 \\ -79 & 58 \end{bmatrix} $	

				Observed		Correc	ctions.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Jan 14.	 	201 46	Direct.	$-\mathring{7}7 \ 58.8$	S.		$-35^{'}$	$-7^{\circ}95^{\circ}7$ ° ′	
0411. 1 1.	00 00	701 10	Direct.	-78 09.0	s. by .E	-83	-35	-80 07	
			Direct.	-80 23.5	N.N.E.	+81	-35	-79 38	
			Direct.	-80 20.4	N.E.	+69	-35	-79 46	
			Direct.	—79 51·7	N.E. by E.	+59	-35	-79 28	
			Def. N.	—79 01·7	N.E. by E.	+59	-81	-79 24 > -79 35	
			Def. S.	_80 00.4	N.E. by E.	+59	-35	$-79 \ 36$	
			Mag. N.	-79 39·7	n.e. by e.	+ 59	-35	-79 16	
			Mag. N.S.	-79 28.8	N.E. by E.	+59	-35	-79 05	
	-		Mag. S.	$-80\ 17.5$	N.N.E.	+81	-35	$-79 \ 32$	
1.5	Gr FO	202 20	Direct. Direct.	_80 22·0	N.N.E.	$ +81 \\ -18 $	$-35 \\ -35$	$\begin{bmatrix} -79 & 36 \\ -79 & 39 \end{bmatrix}$	Very steady, working about
15.	-65 59 $-65 58$	202 22 202 21	Direct.	_78 45·5 _79 19·4	E.S.E. E.	+16	-35	$\begin{bmatrix} -79 & 39 \\ -79 & 38 \end{bmatrix}$	in a hole of
	-05 58	202 21	Direct.	$-79 19^4$ $-78 31.4$	s.w. by s.	-65	-35	-80 11	water.
			Direct.	$-78 \ 45.9$	E.S.E.	-18	-35	$ -79 \ 39 $	
16.	-65 47	202 08	Direct.	-79 23.8	E.	+16	-35	$-79 \ 43$	
	00 .,	707 00	Def. N.	_ 78 32·3	Е.	+16	-81	$-79 \ 37$	
		141	Def. S.	-79 13.2	E.	+16	-35	$-79 \ 32 > -79 \ 38$	
			Mag. N.	—79 06·4	Е.	+16	 35	-79 25	
			Mag. N.S.	_79 00.0	Е.	+16	-35	-79 19	
			Mag. S.	_79 19·3	Е.	+16	-35	-79 38	
			Direct.	_79 23.4	E.	+16	-35	-79 42	
			Direct.	—79 25·3	E.	+16	-35	-79 44	J
17.	$-65 \ 47$		Direct.	-80 05.9	N.E.	+69	-35	$\begin{bmatrix} -79 & 32 \end{bmatrix}$	Fast to a piece of ice.
19.	-66 11	200 45	Direct.	-80 55·9	N.	+86 +82	$-35 \\ -35$	$\begin{bmatrix} -80 & 05 \\ -80 & 03 \end{bmatrix}$]
			Direct.	-80 50.3	N. by E. $\frac{3}{4}$ E. s.s.w. $\frac{1}{2}$ w.	$ + 62 \\ -71 $	-35	$\begin{bmatrix} -80 & 03 \\ -80 & 33 \end{bmatrix}$	Ship steady.
20	-67 37	200 12	Direct. Direct.	$\begin{vmatrix} -78 & 47.2 \\ -79 & 51.6 \end{vmatrix}$	w. by s.	_ 1	-35	-80 28	{
20.	-07 37	200 12	Direct.	$-80 \ 25.6$	w. by s.	+32	-35	$-80\ 29$	-
			Direct.	-80 03.1	w.	+16	-35	_80 00	Long swell, ship
			Direct.	$-80 \ 47.6$	N. by E.	+85	-35	$\begin{vmatrix} -79 & 58 \\ -79 & 58 \end{vmatrix}$ $-80 & 22$	striking heavily against pieces
			Direct.		N. by E. $\frac{1}{2}$ E.	f . a - 1	-35	-80 12	of ice.
			Direct.	-78 26.8	s. by w.	-83	-35	-80 25	
21.	-66 43	202 50	Direct.	-78 44.7	s.s.w.	-77	-35	$-80 \ 37$	i i
			Direct.	-78 38.3	s. by w.	-83	-35	$-80 \ 36$	Swell from
			Direct.	-78 35.4	s.	-85	—35	$-80 \ 35$	W.N.W.
26.	-67 12	203 12	Direct.	$-80\ 12.8$	E. by N.	+32	-35	$-80 \ 16$	
		-	Def. N.	-79 15.3	E. by N.	+32	-81	-80 04	
			Def. S.	-80 14.2	E. by N.	$\begin{vmatrix} +32 \\ +32 \end{vmatrix}$	$-35 \\ -35$	$\begin{bmatrix} -80 & 17 \\ -80 & 10 \end{bmatrix}$	-
			Mag. N.	-80 07.4	E. by N.	+32	-35		
			Mag. N.S. Direct.	-79 55·1	E. by N.	+16	-35	$\begin{vmatrix} -79 & 38 \\ -80 & 22 \end{vmatrix} - 80 & 06*$	Both ships made fast
			Direct.	$\begin{vmatrix} -80 & 03 & 0 \\ -78 & 54 \cdot 4 \end{vmatrix}$	s.e. by E.	-36	-35	-80 05	to a piece of ice; Erebus N. by W.,
			Mag. N.S.	-78 23.2	s.E. by E.	-36	-35	$ -79 \ 34 $	distant 20 fathoms.
,			Mag. S.	$-78 \ 46.7$	s.E. by E.	-36	-35	-79 58	
			Direct.	-79 28.2	E.S.E.	-18	-35	-80 21	
28.	-6746	204 17	Direct.	-80 38.8	E. by N.	+32	-35	$-80 \ 42$	n
			Def. N.	$-79 \ 40.5$	E. by N.	+32	-81	-80 30	
			Def. S.	—81 31·3	N.	+86	-35	-80 40	
			Direct.	—80 46·1	E.N.E.	+46		-80 35	
-			Direct.	$-81 \ 45.8$	N. by E.	+85	-35	-80 56	
			Def. N.	-81 02.7	N. by E.	+85	-81	-81 07	
			Direct.	-81 31.0	N.N.E.	+81	-35	-80 45	Swell from
			Def. N.	-80 43.8	N.N.E.	+81	$-81 \\ -35$	$\begin{vmatrix} -80 & 44 \\ -80 & 38 \\ -80 & 43 \end{vmatrix}$	W.S.W.
	1		Mag. N.	-81 24.4	N.N.E.	+81	55	-00 00 7-00 40	> Table steady.

^{*} Omitted in the Map, in consequence of the vicinity of the other ship.

	-			Observed		Correction	s.	
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	True Inclination.	Remarks.
Jan. 28.	$-67 ext{ } 46$	204 17	Mag. N.S. Mag. S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.E.	+ 81 -3 + 81 -3		Table steady.
			Direct.	-79 06.5	$s. \frac{3}{4} w.$	-84 -	35 -81 06	
			Def. N.	-78 00.0	s. \(\frac{3}{4}\) w.	-84 -8		
			Def. S.	-78 38.0	S. $\frac{3}{4}$ W.	-84 -		
			Mag. N. Mag. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. $\frac{3}{4}$ w. s. $\frac{3}{4}$ w.	$\begin{vmatrix} -84 & -8$		
			Mag. S.	$-78 \ 45.8$	$s. \frac{3}{4} w.$	-84 -		
			Direct.	-79 04.5	S. 3/4 W.	-84 -		
			Direct.	-81 39.3	N.	+86 -	35 -80 48	
· ·			Direct.	$-81\ 42.2$	\mathbf{N} . by \mathbf{W} . $\frac{3}{4}$ \mathbf{W} .			
			Direct.	$-81 \ 47.6$	N. by w. $\frac{1}{2}$ w.	+84 -		
			Direct.	$\begin{vmatrix} -78 & 47.4 \\ -78 & 50.6 \end{vmatrix}$	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	-84 -84 -84 -84 -84 -84 -84 -84 -84 -84		
	-67 48	204 18	Direct.	$-79 \ 45.4$	s.w. by w.	$\begin{vmatrix} -36 \\ -36 \end{vmatrix}$		
			Direct.	-80 40.8	w.	+16 -		K
			Direct.	-81 31.5	n.w. by w.	+59 -		
			Direct.	$-80\ 15.3$	Е.	+16 -		Very steady.
			Direct.	-80 01·3	E. by s.	-1 -		
•.			Direct. Direct.	$\begin{vmatrix} -79 & 46.6 \\ -80 & 31.9 \end{vmatrix}$	E.S.E. E. by N.	$\begin{vmatrix} -18 & -18 \\ +32 & -1 \end{vmatrix}$		
29.	-67 24	204 05	Direct.	$-80 \ 38.5$	E.N.E.	$\begin{vmatrix} +32 \\ +46 \end{vmatrix} - \begin{vmatrix} -16 \\ -16 \end{vmatrix}$		K
1 ~3.		201 00	Direct.	-79 10.2	s. by w.	-83 -		
			Def. N.	-78 06.9	s. by w.	-83 -	81 -80 51	
			Def. S.	$-78 \ 44.1$	E.N.E.	+46 -		
			Mag. N.	$ -78 \ 38.6$	E.N.E.	+46 -	-	
21	67 10	202 24	Mag. N.S. Direct.	-78 33.9	E.N.E.	$\begin{vmatrix} +46 \\ -77 \end{vmatrix}$		
31.	-07 12	202 24	Def. N.	$\begin{vmatrix} -78 & 59.8 \\ -78 & 07.9 \end{vmatrix}$	s.s.w.	-77 -	81 _80 46	Ctuona buona
			Def. S.	-78 55·8	s.s.w.	-77 -		Strong breeze, steady.
			Mag. N.	-78 36.9	s.s.w.	-77 -	35 -80 29	
			Mag. N.S.	-78 29.0	s.s.w.	-77 -		
			Mag. S.	-79 07.7	s.s.w.	-77 -		
			Direct. Def. N.	-79 23·3	s.w.	$\begin{vmatrix} -52 \\ -52 \end{vmatrix}$ -		
			Der. N. Direct.	$\begin{vmatrix} -78 & 09.4 \\ -79 & 15.3 \end{vmatrix}$	s.w.	$\begin{vmatrix} -3z \\ -65 \end{vmatrix} - \begin{vmatrix} -5z \\ -5z \end{vmatrix}$		
			Def. N.	-78 23.5	s.w. by s.	-65 -		
Feb. 1.	-67 12	201 34	Direct.	-80 15.5	w. by s.	- 1 -	$35 \mid -80 \; 52\tilde{1}$	Ĭ
			Def. N.	-79 14.5	w. by s.	-1 -		
			Direct.	-80 06.5	Е.	+17 -	1	Ship steady, ice
			Def. N. Direct.	$\begin{vmatrix} -79 & 05.2 \\ -79 & 29.1 \end{vmatrix}$	E.S.E.	$\begin{vmatrix} +17 \\ -18 \end{vmatrix}$ -		all around.
			Direct.	$-80 \ 25.9$	W.	+17 -	$\begin{vmatrix} -80 & 22 \\ -80 & 44 \end{vmatrix}$	
			Direct.	-79 51.9	w.s.w.	-18 -	35 -80 45	
	-67 16	5	Direct.	-7858.6	s.s.w.	-77 -		
		-	Def. N.	-7759.0	s.s.w.	-77 -		Table steady.
1			Def. S.	$\begin{vmatrix} -78 & 53.6 \\ -78 & 32.1 \end{vmatrix}$	S.S.W.	$\begin{vmatrix} -77 \\ -77 \end{vmatrix}$ -	35 -80 40	
1			Mag. N. Mag. N.S.	$-78 32^{\circ}1$ $-78 30^{\circ}2$	s.s.w.	-77 -		
			Mag. S.	-78 49.0	s.s.w.	-77 -		
			Direct.	-79 00.8	s.s.w.	-77 -	35 -80 53	
1			Direct.	_81 30·0	$N_{\bullet} \frac{3}{4} W_{\bullet}$	+86 -	- 1	
			Def. N.	$-80 \ 37.0$	N. 3/4 W.	+86 -		
	-		Direct. Def. N.	$\begin{bmatrix} -79 & 08.1 \\ -78 & 11.1 \end{bmatrix}$	s.w.	$\begin{vmatrix} -52 \\ -52 \end{vmatrix}$ -		
			1761. IV.	10 111	20.44.	"~ -	~_ ~~	

^{*} Omitted in the mean; apparently the degree should have been written 80 instead of 78.

			35.1.1	Observed	Dimetion	Correc	tions.		•
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Feb. 2.	-67 56	199 48	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c cccc} -79 & 28.6 \\ -78 & 37.8 \\ -79 & 15.1 \\ -78 & 53.6 \\ -79 & 07.5 \end{array}$	s. by w.	-83 -83 -83 -83 -83	-35 -81 -35 -35 -35	-81 27 -81 22 -81 13 -80 52 -81 06	
3.	-68 21	200 06	Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	-79 26·9 -79 27·4 -79 34·2 -78 31·9 -79 26·7 -79 24·2	s. by w. s. by w. s.s.w. s.s.w. s.s.w.	-83 -83 -77 -77 -77 -77	-35 -35 -35 -81 -35 -35	-81 25 -81 25 -81 26 -81 10 -81 19 -81 16	Table steady.
4.	68 45	199 41	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S.	-79 23·4 -79 28·6 -79 36·1 -79 32·5 -78 50·3 -79 36·6	s.s.w. s.s.w. s.s.w. s.	-77 -77 -77 -85 -85 -85	-35 -35 -35 -35 -81 -35	$ \begin{array}{c cccc} -81 & 15 \\ -81 & 21 \\ -81 & 29 \\ -81 & 33 \\ -81 & 36 \\ -81 & 37 \end{array} $	
			Mag. N. Mag. N.S. Mag. S. Direct. Def. N.	-79 17·2 -79 12·4 -79 43·4 -79 32·1 -78 50·4	s. s. s. by e. s. by e.	-85 -85 -85 -83 -83	-35 -35 -35 -35 -81	$ \begin{vmatrix} -81 & 17 \\ -81 & 12 \\ -81 & 43 \\ -81 & 30 \\ -81 & 34 \end{vmatrix} -81 & 33$	
	-68 49	199 26	Def. S. Direct. Def. N.	$ \begin{vmatrix} -79 & 25.8 \\ -82 & 31.4 \\ -81 & 48.7 \end{vmatrix} $	s. by E. N.N.W.	$\begin{vmatrix} -83 \\ +82 \\ +82 \end{vmatrix}$	$-35 \\ -81$		Fresh breeze, steady.
5.	-68 52	198 24	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-81 51·5 -79 59·5 -80 58·7 -80 48·0 -80 36·8 -81 04·1	S.W. S.W. S.W. S.W.	-52 -52 -52 -52 -52 -52	-35 -81 -35 -35 -35 -35	-83 19 -82 13 -82 26 -82 15 -82 04 -82 31	
6.	69 55	192 17	Direct. Direct. Direct. Def. N. Def. S.	-81 21·6 -81 20·0 -81 09·2 -80 15·1 -81 04·2	s.w. ½ w. s.w. by w. s. by w. s. by w. s. by w.	44 36 84 84 84	-35 -35 -35 -81 -35	$ \begin{bmatrix} -82 & 41 \\ -82 & 31 \end{bmatrix} $ $ -83 & 08 \\ -83 & 00 \\ -83 & 03 $	
			Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N	-80 52·3 -80 39·1 -81 09·2 -81 12·8 -80 56·9 -80 00·2	s. by w. s.	-84 -84 -84 -86 -86	$-35 \\ -35$	$ \begin{vmatrix} -82 & 51 \\ -82 & 38 \\ -83 & 08 \\ -83 & 12 \\ -82 & 58 \\ -82 & 47 \end{vmatrix} -83 & 00$	Steering well, but table not steady.
7	70 05	191 03	Direct. Direct. Def. N. Direct. Direct. Direct. Def. S.	-81 12.6 -81 35.1 -80 38.2 -81 56.4 -81 35.3 -81 20.0	s. by w. s.s.w. s.s.w. s.w. s.by w. ³ / ₄ w. s.s.w.		_35 _35 _81 _35 _35 _35	$\begin{bmatrix} -83 & 12 \\ -83 & 28 \\ -83 & 17 \\ -83 & 23 \\ -83 & 30 \\ -83 & 13 \end{bmatrix} -83 & 20$	Strong breeze, ship
8	70 08	186 39	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N.	-81 24·7 -81 15·6 -81 23·9 -81 29·6 -81 56·9 -81 16·7	s.s.w. s.s.w. s.s.w. s.by w. ½ w s.w. s.w.		_35 _35 _35 _35 _35 _81	-83 18 -83 09 -83 17 -83 26 -83 24 -83 30	steering wildly.
			Direct. Def. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.w. by w. s.w. by w.	$\begin{vmatrix} -36 \\ -36 \end{vmatrix}$	$\begin{bmatrix} -35 \\ -83 \end{bmatrix}$	$ \begin{vmatrix} -83 & 30 \\ -83 & 23 \\ -83 & 31 \end{vmatrix} -83 & 23$	Table steady.

					· · · · · · · · · · · · · · · · · · ·		1		
				Observed		Correc	ctions.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attrac- tion.	Index.	True Inclination.	Remarks.
Feb. 8.	70 ó s	186 39	Def. S. Mag. N. Mag. N.S.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	s.w. by w. s.w. by w. s.w. by w.	$ \begin{array}{r} -36 \\ -36 \\ -36 \end{array} $	-35 -35 -35	$ \begin{array}{c c} -83 & 21 \\ -83 & 21 \\ -83 & 21 \\ -83 & 15 \end{array} $	Table steady.
	-70 17	186 04	Mag. S. Direct. Direct. Direct. Def. N. Def. S.	-82 10·3 -82 15·9 -81 19·7 -81 16·1 -80 37·6 -81 38·5	s.w. by w. s.w. by w. s. s. s. s.		$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -81 \\ -35 \\ \end{array} $	-83 21 -83 27 -83 22 -83 18 -83 26 -83 41	
9.	_70 32	185 38	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.S. Direct.	-81 11·6 -81 04·5 -81 33·4 -81 20·6 -83 51·8 -83 09·4 -83 55·8 -83 36·2 -82 08·5	s. s. s. w. by n.	$ \begin{bmatrix} -87 \\ -87 \\ -87 \\ +32 \\ +32 \\ +32 \\ +32 \\ +32 $	-35 -35 -35 -35 -35 -35 -35 -35	-83 14 -83 07 -83 35 -83 23 -83 55 -83 58 -83 59 -83 39 -82 12	
10.	.—69 56	184 43	Def. N. Direct. Def. S. Mag. N.S. Direct. Direct. Def. N. Def. S. Mag. N.	-81 14·8 -82 02·7 -82 01·0 -82 03·5 -82 12·6 -83 33·0 -82 37·3 -83 31·5 -83 25·9	w. by N. s.e. ½ s. s.e. ½ s. s.e. ½ s. s.e. by s. w. by s. w. by s. w. by s. w. by s.	$ \begin{array}{r} +32 \\ -59 \\ -59 \\ -66 \\ -1 \\ -1 \\ -1 \\ \end{array} $	-81 -35 -35 -35 -35 -81 -35 -35	-82 04 -83 30 -83 37 -83 35 -83 38 -83 54 -84 09 -83 59 -84 07 -84 02	Head swell, un- steady.
11.	_69 51	183 02	Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N. Def. S.	-83 11·0 -83 33·1 -83 34·2 -83 46·2 -83 21·8 -82 21·1 -83 04·0	w. by s. w. by s. w. by s. w. s.w. w.s.w. w.s.w.	$ \begin{array}{r r} -1 \\ -1 \\ -1 \\ +17 \\ -18 \\ -18 \\ -18 \\ \end{array} $	-35 -35 -35 -35 -35 -81 -35	-83 47 -84 09 -84 10 -84 04 -84 15 -84 00 -83 57	Heavy swell, un- steady.
12.	-70 03 $-71 03$		Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N.	-83 25·7 -82 58·0 -83 20·5 -82 45·0 -82 46·6 -81 48·5	w.s.w. w.s.w. s.w. by s. s.e. by s.		-35 -35 -35 -35 -35 -35	-84 19 -83 51 -84 14 -84 26 -84 28 -84 16	Strong wind, westerly swell, ship unsteady.
	-71 02	180 58	Def. S. Mag. N. Mag. N.S. Mag. S. Direct. Direct.	-82 39·3 -82 24·9 -82 21·1 -82 34·9 -82 45·2 -83 08·2	s.e. by s.		$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ \end{array} $	-84 20 -84 20 -84 06 -84 02 -84 16 -84 26 -84 49	Cross sea, table very unsteady. Table very unsteady, a cross
13	72 07		Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct.	-83 16 8 -82 21 1 -83 18 6 -83 06 9 -82 55 3 -83 17 7 -83 20 2 -83 37 9 -83 40 5	s.e. by s.	-66 -66 -66 -66 -66 -66 -66	-35 -81 -35 -35 -35 -35 -35 -35	-84 48 -84 48 -85 00 -84 48 -84 36 -84 59 -85 01 -85 19 -85 22	A swell from N.W., ship unsteady, steering badly.

				01 1		Corre	ctions.	·	
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Feb. 14.	_^2 55	181 33	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-83 58·2 -83 21·7 -84 07·0 -84 01·7 -83 29·5 -83 58·4	s.e. by e. s.e. by e. s.e. by e. s.e. by e. s.e. by e.	-36 -36 -36 -36 -36 -36	-81 -35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	A swell from the W.N.W., unsteady.
	-73 23 $-74 20$ $-74 51$	177 55	Direct. Direct. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	-84 00·6 -84 16·8 -84 51·4 -85 13·4 -84 17·5 -85 10·6 -85 08·8 -84 53·3	s.e. by e. s.e. by s. s.s.e. s.s.e. s.s.e. s.s.e. s.s.e.	$egin{array}{c} -36 \\ -52 \\ -66 \\ -79 \\ -79 \\ -79 \\ -79 \\ -79 \end{array}$	-35 -35 -35 -35 -81 -35 -35 -35	-85 12 -85 44 -86 32 -87 07 -86 58 -87 05 -87 03 -86 47	Strong breeze, un- steady. Heavy sea, very un- steady.
	—75 05 —75 09		Mag. S. Direct. Direct. Direct. Direct. Direct. Def. N.	-85 12·0 -85 15·6 -85 49·1 -86 56·1 -86 33·0 -85 35·9	s.s.e. s.s.e. s.e. e. ½ s. e. by s. e. by s.		-35 -35 -35 -35 -35 -81	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. swell, slight motion.
17.	—75 57 —76 0 6		Def. S. Mag. N.S. Direct. Direct. Def. N. Def. S. Mag. N.	$ \begin{vmatrix} -86 & 39.6 \\ -86 & 13.2 \\ -87 & 15.8 \\ -87 & 12.6 \\ -86 & 31.1 \\ -87 & 05.2 \\ -86 & 50.8 \end{vmatrix} $	E. by s. E. N.E. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	$\begin{vmatrix} +39 \\ +39 \\ +39 \end{vmatrix}$	$\begin{vmatrix} -35 \\ -35 \end{vmatrix}$	$ \begin{bmatrix} -87 & 17 \\ -86 & 50 \end{bmatrix} $ $ -87 & 05 \\ -87 & 09 \\ -87 & 13 \\ -87 & 01 \\ -86 & 47 \end{bmatrix} $ $ -87 & 03 $	Very unsteady, steering badly.
18.	—77 02	181 37	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	-86 39.4 -87 33.9 -87 08.0 -87 06.3 -86 16.8 -87 21.3 -87 14.9 -86 45.6	E. by N. \(\frac{1}{2}\) N. E. by N. \(\frac{1}{2}\) N. E. by N. \(\frac{1}{2}\) N. E.N.E. E.N.E. E.N.E. E.N.E. E.N.E.	+39		$ \begin{vmatrix} -86 & 35 \\ -87 & 30 \\ -87 & 04 \end{vmatrix} $ $ \begin{vmatrix} -86 & 55 \\ -86 & 52 \\ -87 & 10 \\ -87 & 04 \\ -86 & 35 \end{vmatrix} $ $ \begin{vmatrix} -86 & 56 \end{vmatrix} $	
19.	-77 0 9 -76 48		Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	-87 15·2 -87 37·4 -86 56·5 -87 27·6 -86 54·2 -87 45·2 -87 16·6	E.N.E. N.E. \frac{1}{2} E. N.E. by E. \frac{1}{2} E. N. by E. N. by E. N. by E. N. by E.	$\begin{vmatrix} +46 \\ +64 \\ +52 \\ +88 \\ +88 \\ +88 \\ +88 \end{vmatrix}$	-35 -35 -35 -35 -81 -35 -35	$ \begin{bmatrix} -87 & 04 \\ -87 & 08 \\ -86 & 39 \end{bmatrix} $ $ \begin{bmatrix} -86 & 35 \\ -86 & 47 \\ -86 & 52 \\ -86 & 24 \end{bmatrix} $ $ \begin{bmatrix} 86 & 30 \\ \end{bmatrix} $	Cross sea, table
20.	—76 50 —76 20		Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N. Def. S.	-87 15·1 -86 53·6 -87 29·1 -87 01·3 -86 44·6 -86 04·7 -86 42·3	N. by E. N. by E. N. by E. N.E. ½ N. N.E. N.E.	+88 +88 +72 +69 +69	-35 -35 -35 -35 -35 -81 -35	-86 22 -86 01 -86 36 -86 24 -86 11 -86 17 -86 08	unsteady.
21.	-76 14 -75 45		Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct.	$\begin{array}{c} -86 & 26.7 \\ -86 & 23.0 \\ -86 & 48.5 \\ -86 & 39.1 \\ -85 & 56.9 \\ -84 & 13.7 \end{array}$	N.E. N.E. N.E. N.E. by E. S.W.	$ \begin{array}{r} +69 \\ +69 \\ +69 \\ +59 \\ -52 \end{array} $	-35 -35 -35 -35 -35 -35	$ \begin{array}{c c} -85 & 53 \\ -85 & 49 \\ -86 & 15 \\ -86 & 05 \\ -85 & 33 \\ -85 & 41 \end{array} \right\} $	Strong gale, heavy sea, a great deal of motion.

				*	× .	Correc	tions.		
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Feb. 22.	-76 ź4	184 54	Direct. Def. N. Def. S. Mag. N.	-83 41.5 -82 56.0 -83 37.0 -83 19.8	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	-66 -66 -66	-35 -81 -35 -35	-85 23 -85 23 -85 18 -85 01	A head sea, ship unsteady.
	-76 46 -77 13	1	Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N. Def. S. Mag. N.	-82 59·8 -83 29·9 -83 45·2 -84 19·4 -84 37·4 -83 51·4 -84 50·8 -84 31·6	s.e. by s. s.e. by s. s.e. by s. e.s.e. e. by s. e. by s. e. by s. e. by s.	$ \begin{bmatrix} -66 \\ -66 \\ -18 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 $	$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -81 \\ -35 \\ -35 \\ \end{array} $	$ \begin{vmatrix} -84 & 41 \\ -85 & 11 \\ -85 & 26 \\ -85 & 12 \\ -85 & 13 \\ -85 & 13 \\ -85 & 27 \\ -85 & 08 \end{vmatrix} $	Light swell, gen-
<i>2</i> 3.	-77 48 -77 47		Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N. Def. S.	_84 17.0 _84 27.8 _85 02.7 _84 14.6 _85 13.0 _84 34.3 _85 21.1	E. by s. E. s.w.byw.½w. N.E. by E. N.E. by E. N.E. by E.	$\begin{vmatrix} - & 1 \\ - & 1 \\ +17 \end{vmatrix}$	-35 -35 -35 -35 -35 -81 -35 -35	-84 53 -85 04 -85 21 -85 17 -84 49 -84 56 -84 57	tle motion.
24.	—77 14	199 29	Direct. Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	-85 05.7 -84 21.4 -84 41.7 -85 00.2 -85 05.5 -84 00.0 -83 17.5 -83 57.7 -83 42.9	E.N.E. E.N.E. E.N.E. S.W. by S. S.W. by S. S.W. by S.	$\begin{vmatrix} +46 \\ +46 \\ +46 \\ +46 \\ -66 \\ -66 \\ -66 \\ -66 \end{vmatrix}$	-35 -35 -35 -35 -35 -81 -35 -35	-84 10 -84 31 -84 49 -84 55 -85 41 -85 45 -85 39 -85 94	Table very steady.
25.	-77 00 -75 20		Mag. N.S. Mag. S. Direct. Direct. Direct. Def. N. Def. S. Mag. N.	-83 32·3 -84 11·7 -85 13·3 -84 25·8 -85 30·9 -84 33·1 -85 28·4 -85 15·5	s.w. by s. s.w. by s. w. s.w. by w. w. w. w.	$ \begin{array}{r} -66 \\ -66 \\ +17 \\ -36 \\ +17 \\ +17 \\ +17 \\ +17 \end{array} $	$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -81 \\ -35 \\ -35 \end{array} $	-85 13 -85 53 -85 31 -85 37 -85 49 -85 37 -85 46 -85 34	Swell from N.E., steady.
26.	-73 10	189 21	Mag. N.S. Mag. S. Direct. Direct. Direct. Direct. Direct. Direct.	-84 59·3 -85 22·7 -85 38·6 -84 34·6 -86 03·9 -85 37·4 -84 44·0	w. w. s.w. by s. w.n.w. n.w. by w. n.w. by w.	$\begin{vmatrix} +17 \\ +17 \\ +17 \\ -66 \\ +46 \\ +60 \\ +60 \end{vmatrix}$		$ \begin{vmatrix} -85 & 17 \\ -85 & 41 \\ -85 & 57 \\ -86 & 16 \\ -85 & 53 \\ -85 & 12 \\ -85 & 05 \end{vmatrix} $	Swell from the E.N.E., steady.
27.	. —72 03	187 40	Def. S. Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S.	-85 36·9 -85 19·6 -85 37·8 -85 30·6 -85 35·6 -83 30·8 -82 37·6 -83 36·5	N.w. by w. S.w. S.w. S.w.	$egin{array}{c} +60 \\ +60 \\ +60 \\ +60 \\ -52 \\ -52 \\ -52 \end{array}$	$ \begin{array}{r} -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ -35 \\ \end{array} $	-85 12 -84 55 -85 13 -85 06 -85 11 -84 58 -84 51 -85 04	Strong breeze, motion great.
	-71 43	187 15	Mag. N. Direct. Mag. N.S. Mag. S. Direct. Direct.	-83 07 6 -84 56 8 -84 25 5 -83 43 4 -83 52 3 -84 56 8	s.w. w. by N. ½ N. w. by N. ½ N. s.w. w.s.w.	-52 + 39	-35 -35 -35 -35 -35 -35	$ \begin{vmatrix} -84 & 35 \\ -84 & 53 \\ -84 & 22 \\ -85 & 10 \\ -84 & 45 \\ -85 & 50 \end{vmatrix} $ $ -84 & 56$	Swell from the eastward, motion slight. Table steady.

				Observed		Corrections.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	True Inclination.	Remarks.
Feb. 28.	-71 20	184 30	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	-84 01·9 -82 59·6 -83 56·9 -83 37·9 -83 23·9	w. by s.	$ \begin{vmatrix} & & & & \\ - & & 1 & -35 \\ - & & 1 & -81 \\ - & & 1 & -35 \\ - & & 1 & -35 \\ - & & 1 & -35 \end{vmatrix} $	-84 38 -84 22 -84 33 -84 14 -84 00	
	—70 55	183 56	Mag. S. Direct. Direct. Direct.	-84 00·7 -83 35·3 -84 32·0 -84 36·8	w. by s. s.w. by w. w. ½ s. w.	$ \begin{vmatrix} - & 1 & -35 \\ - & 36 & -35 \\ + & 8 & -35 \\ + & 17 & -35 \end{vmatrix} $	-84 37 -84 46 -84 59 -84 55	Table steady.
Mar. 1.	$-70 ext{ } 49 \\ -69 ext{ } 54$	183 46 179 55	Direct. Direct. Def. N. Def. S.	-85 31.6 -85 00.0 -84 06.3 -84 54.4 -84 44.4	N.W. ½ W. W.N.W. W.N.W.	$\begin{vmatrix} + & 64 & -35 \\ + & 54 & -35 \\ + & 54 & -81 \\ + & 54 & -35 \\ + & 54 & -35 \end{vmatrix}$	-85 03 -84 41 -84 33 -84 35 -84 25	*
2.	68 09	183 10	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Direct.	$ \begin{array}{rrrrr} -34 & 44^{4} \\ -84 & 35 \cdot 4 \\ -84 & 44 \cdot 7 \\ -84 & 54 \cdot 2 \\ -84 & 28 \cdot 0 \\ -83 & 45 \cdot 8 \end{array} $	W.N.W. W.N.W. W.N.W. W.N.W. N.N.E.	$\begin{vmatrix} + 54 & -35 \\ + 54 & -35 \\ + 54 & -35 \\ + 54 & -35 \\ + 37 & -35 \\ + 99 & -35 \end{vmatrix}$	-84 26 -84 26 -84 26 -84 26 -84 26 -82 42	Swell from the eastward, table steady.
~			Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	-82 29·8 -83 33·2 -83 31·2 -83 17·5 -83 26·9 -83 40·9	N.N.E. N.N.E. N.N.E. N.N.E. N.N.E.	+ 99 -81 + 99 -35 + 99 -35 + 99 -35 + 99 -35 + 99 -35	-82 12 -82 29 -82 27 -82 14 -82 23 -82 37	Table steady.
3.	—67 35	185 18	Direct. Direct. Direct. Def. N. Def. S. Mag. N.	-82 27.4 -82 53.4 -82 21.8 -81 31.3 -82 16.9 -82 04.0	N.E. by E.	$ \begin{vmatrix} +71 & -35 \\ +83 & -35 \\ +71 & -35 \\ +71 & -81 \\ +71 & -35 \\ +71 & -35 \end{vmatrix} $	-81 517 -82 05 -81 46 -81 41 -81 41 -81 28	Cross sea, un- steady.
4.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	185 32 187 40	Mag. N.S. Mag. S. Direct. Direct. Direct.	$ \begin{vmatrix} -81 & 58.7 \\ -82 & 02.7 \\ -82 & 28.2 \\ -82 & 12.6 \\ -82 & 18.4 \end{vmatrix} $	N.E. by E. N.E. ½ E. W. N. by W.	$egin{array}{c cccc} + & 71 & -35 \\ + & 71 & -35 \\ + & 76 & -35 \\ + & 18 & -35 \\ + & 103 & -35 \\ \hline \end{array}$	$ \begin{vmatrix} -81 & 23 \\ -81 & 27 \\ -81 & 52 \\ -82 & 30 \\ -81 & 10 \end{vmatrix} $	
-	C= 00	100 00	Def. N. Def. S. Mag. N. Mag. S.	-81 14·9 -82 28·2 -82 07·0 -82 22·0	n. by w. n. by w. n. by w. n. by w.	$\begin{vmatrix} +103 & -81 \\ +103 & -35 \\ +103 & -81 \\ +103 & -35 \end{vmatrix}$		Strong gale, heavy sea, very unsteady.
3.	—67 09	188 02	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	-82 13·3 -81 40·1 -81 45·6 -82 19·7 -82 01·2 -82 16·6	N. N. N. N.	+104 $-35+104$ $-81+104$ $-35+104$ $-35+104$ -35	_80 52 _81 08	Heavy sea, very unsteady.
6.	-65 28	191 24	Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	-82 20·0 -81 09·3 -80 06·6 -80 50·1 -80 47·0 -80 34·9	n. by e.	$ \begin{array}{r} +104 & -35 \\ +102 & -35 \\ +102 & -81 \\ +102 & -35 \\ +102 & -35 \\ +102 & -35 \\ \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	South-westerly
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	192 00 192 21	Mag. S. Direct. Direct. Direct. Direct.	-81 00·6 -81 03·5 -80 44·2 -80 28·9 -80 30·4	 N. by E. N. by E. N. by E. ¹/₂ E. N. by E. ¹/₂ E. 	$ \begin{array}{r} +102 \\ +102 \\ -35 \\ +102 \\ -35 \\ +99 \\ -35 \\ +99 \\ -35 \\ \end{array} $	$\begin{bmatrix} -79 & 54 \\ -79 & 57 \\ -79 & 37 \\ -79 & 25 \\ -79 & 26 \end{bmatrix}$	swell, unsteady.

7						Corrections.		
			35.41.3	Observed	Dimetion of	Corrections.		
1842.	Lat.	Long.	Method employed.	Inclination.	Direction of ship's head.	Ship's	True Inclination.	Remarks.
			empio jeu:	Face east.	omp s noud.	attrac- Index.		
						tion.		
	. ,	0 /		.0 /2		1 2	0 /_ 0 /	
Mar. 7.	-6330	194 15	Direct.	-79 46.4	N. by E.	+100 -35	-78-41)	
			Def. N.	-78 34.4	N. by E.	+100 -81	$-78 \ 15$	
			Def. S.	-79 29.2	N. by E.	+100 -35	-78 24 Table 24	
			Mag. N.	-79 26.0	N. by E.	+100 -35	$ -78 \ 21 \ -78 \ 30$	Steady.
			Mag. N.S.	-79 24.0	n. by E.	+100 -35	-78 19	
			Mag. S.	-79 50.3	n. by E.	+100 -35	78 45	
	00.15		Direct.	-7949.3	n. by E.	+100 -35	$\begin{bmatrix} -78 & 44 \end{bmatrix}$	
8.	-62 17	195 55	Direct.	-78 44.7	N. by E.	+100 -35	-77 40	
			Def. N.	-77 54·4	N. by E.	$\begin{vmatrix} +100 \\ +100 \end{vmatrix} = 35$	$\begin{bmatrix} -77 & 35 \\ 77 & 91 \end{bmatrix}$	
			Def. S.	-78 25·8	N. by E.	$\begin{vmatrix} +100 & -35 \\ +100 & -35 \end{vmatrix}$	$\begin{vmatrix} -77 & 21 \\ -77 & 23 \\ -77 & 30 \end{vmatrix}$	
			Mag. N.	-78 27·8	N. by E.	+100 -35 +100 -35	$\begin{vmatrix} -77 & 23 \\ -77 & 15 \end{vmatrix}$	Steady.
			Mag. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	n. by E.	+100 -35	-77 38	
1			Mag. S. Direct.	$-78 \ 40.3$	N. by E.	+100 -35	-77 35	
9.	-61 06	198 08	Direct.	$-77 \ 41.6$	N.E. $\frac{1}{2}$ N.	+ 85 -35	$\begin{bmatrix} -76 & 52 \\ -76 & 52 \end{bmatrix}$	
9.	-01 00	190 00	Def. N.	-76 24.7	N.E. 2 N.	+85 -81	-76 22	
			Def. S.	-77 25.9	N.E. 1/2 N.	+85 -35	-76 36	
1			Mag. N.	-77 16.4	N.E. by N.	+88 -35	76 93	
			Direct.	-77 38.4	N.E. by N.	+88 -35	$\begin{vmatrix} -76 & 25 \\ -76 & 45 \end{vmatrix} - 76 & 32$	Steady.
			Mag. N.S.	-77 11.9	N.E. by N.	+88 -35	_76 19	
1			Mag. S.	-77 16·9	N.E. by N.	+ 88 -35	-76 24	
-			Direct.	-77 28.6	N.E. by N.	+ 88 -35	$-76 \ 36$	
			Direct.	-77 16.7	N.E.	+81 -35	_76 31	
10.	-60 57	199 03	Direct.	-75 32.7	E.N.E.	+ 53 -35	$-75 \ 15$	-
		-00	Def. N.	$-74 \ 41.0$	E.N.E.	+ 53 - 81	_75 19	
			Def. S.	-75 33·6	E.N.E	+ 53 - 35	_75 16	
			Mag. N.	-75 14.2	E.N.E.	+53 -35	-74 56 > -75 08	Table unsteady.
			Mag. N.S.	-75 08.5	E.N.E.	+ 53 -35	_74 51	·
			Mag. S.	-75 27.1	E.N.E.	+ 53 -35	_75 09	
			Direct.	-75 30.9	E.N.E.	+ 53 - 35	_75 13	
11.	-60 15	208 06	Direct.	-74 20.6	E. by N.	+37 -35	-74 197	
			Def. N.	_73 57·2	E. by N.	+37 -81	_74 41	
			Def. S.	_74 16·0	E. by N.	+ 37 -35	_74 14	
			Mag. N.	-74 32.4	E. by N.	+37 -35	$-74 \ 30 > -74 \ 21$	Strong gale, heavy
			Mag. N.S.	-74 16.0	E. by N.	$ + \frac{37}{25} - \frac{35}{25}$	_74 14	sea, ship unsteady.
			Mag. S.	-74 20.9	E. by N.	+37 -35	$\begin{bmatrix} -74 & 19 \\ 74 & 27 \end{bmatrix}$	
	22.22		Direct.	-74 28.5	E. by N.	+37 -35	_74 27	
12.	-60 16	211 45	Direct.	-74 07.4	E. by N.	$\begin{vmatrix} + & 37 & -35 \\ + & 37 & -81 \end{vmatrix}$	$\begin{bmatrix} -74 & 05 \\ 74 & 15 \end{bmatrix}$	
			Def. N.	-73 31·1	E. by N.	1 1 0 -	$\begin{bmatrix} -74 & 15 \\ -74 & 18 \end{bmatrix}$	1.
			Def. S.	-74 20·5	E. by N.	0 - 0 -	$\begin{vmatrix} -74 & 18 \\ -74 & 07 \end{vmatrix}$	
			Mag. N.	$\begin{vmatrix} -74 & 08.9 \\ -74 & 28.0 \end{vmatrix}$	E. by N.	0 - 0	$\begin{array}{c c} -74 & 07 \\ -74 & 26 \end{array} > -74 & 14 \end{array}$	Heavy swell, ship
1			Mag. N.S.	-74 280 $-74 33.4$	E. by N.	$\begin{vmatrix} + & 37 & -35 \\ + & 37 & -35 \end{vmatrix}$	-74 31	unsteady.
			Mag. S. Direct.	$-74 \ 33 \ 4$ $-74 \ 11.5$	E. by N.	1 0 - 0 -	-74 09	
l .	-60 18	212 39	Direct.	-73 59.8	E. by N.	$\begin{vmatrix} + & 37 & -35 \\ + & 37 & -35 \end{vmatrix}$	$\begin{bmatrix} -73 & 58 \\ -73 & 58 \end{bmatrix}$	
13.			Direct.	$-73 \ 33 \ 6$ $-74 \ 15.6$	N.E. 1/2 E.	+74 -35	$-73 \ 375$	
1	0,00	~10 ~0	Def. N.	-73 29.3	N.E. 1/2 E.	+ 74 -81	_73 36	
			Def. S.	-74 15·9	N.E. $\frac{1}{2}$ E.	+74 -35	-73 37	
			Mag. N.	-74 09.7	$N \cdot E \cdot \frac{1}{2} E \cdot$	+74 -35	$-73 \ 31 > -73 \ 36$	Heavy swell, steer-
1		-	Mag. N.S.	-74 15·3	N.E. $\frac{1}{2}$ E.	+74 - 35	_73 36 (ing very wildly.
			Mag. S.	-74 16.5	N.E. 1/2 E.	+74 -35	—73 37	
			Direct.	-74 18.2	N.E. $\frac{1}{2}$ E.	+74 -35	-73 39	
14	-59 22	218 14	Direct.	-75 02.4	N.E. by E.	+69 -35	−74 285	
			Def. N.	-74 26.8	N.E. by E.	+69 -81	-74 39	TT
			Def. S.	—75 01·0	N.E. by E.	+69 -35	-74 27	Heavy swell from W.S.W., very un-
l			Mag. N.	-74 50·0	N.E. by E.	+69 -35	$-74 \ 16 > -73 \ 48$	steady, steering very badly.
l	1	1	1		1		1	1 Tory Damy.

				Observed		Corrections.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	True Inclination.	Remarks.
Mar. 14.	5°9 2′2	218 14	Mag. N.S. Mag. S. Direct.	$ \begin{vmatrix} -74 & 58.0 \\ -75 & 01.0 \\ -75 & 09.6 \end{vmatrix} $	N.E. by E. N.E. by E. N.E. by E.	$\begin{vmatrix} +69 & -35 \\ +69 & -35 \\ +69 & -35 \end{vmatrix}$		Heavy swell from W.S.W., very un- steady, steering very badly.
15.	—58 4 9	221 25	Direct. Direct. Direct. Def. N. Def. S. Mag. N.	-75 07·1 -75 13·7 -73 06·6 -72 15·7 -73 21·2 -73 08·4	N.E. by E. N.E. by E. E.N.E. E.N.E. E.N.E.	$ \begin{vmatrix} +69 & -35 \\ +69 & -35 \\ +53 & -35 \\ +53 & -81 \\ +53 & -35 \\ +53 & -35 \end{vmatrix} $	$ \begin{vmatrix} -74 & 33 \\ -74 & 40 \\ -72 & 49 \\ -72 & 44 \\ -73 & 03 \\ -72 & 50 \end{vmatrix} $	
16.	-58 48 -58 59 -59 01	222 22 227 30 227 43	Mag. N.S. Mag. S. Direct. Direct. Direct. Direct. Dorect. Def. N. Def. S.	$\begin{array}{c} -73 & 13 \cdot 1 \\ -73 & 07 \cdot 7 \\ -73 & 10 \cdot 8 \\ -74 & 05 \cdot 2 \\ -73 & 24 \cdot 8 \\ -73 & 21 \cdot 9 \\ -72 & 33 \cdot 3 \\ -73 & 14 \cdot 1 \end{array}$	E.N.E. E.N.E. E. by N. E. E.	$\begin{array}{c cccc} +53 & -35 \\ +53 & -35 \\ +53 & -35 \\ +37 & -35 \\ +21 & -35 \\ +21 & -35 \\ +21 & -35 \end{array}$	$\begin{bmatrix} -72 & 55 \\ -72 & 50 \\ -72 & 53 \\ -74 & 03 \\ -73 & 39 \\ -73 & 36 \\ -73 & 30 \\ -73 & 3$	
17.	-59 32	231 46	Mag. N. Mag. N.S. Mag. S. Direct. Direct.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. E. E. E.	$\begin{array}{c cccc} +21 & -35 \\ +21 & -35 \\ +21 & -35 \\ +21 & -35 \\ +21 & -35 \\ +21 & -35 \end{array}$	$ \begin{vmatrix} -73 & 28 \\ -73 & 14 \\ -73 & 24 \\ -73 & 21 \\ -73 & 41 \\ -72 & 55 \end{vmatrix} $	Heavy sea from W.S.W., very un- steady, steering very badly.
18.	60 05	235 56	Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c cccc} -72 & 19.5 \\ -71 & 10.6 \\ -72 & 24.0 \\ -72 & 29.7 \\ -72 & 04.7 \end{array}$	E. by s.	$\begin{array}{c cccc} + & 2 & -35 \\ + & 2 & -81 \\ + & 2 & -35 \\ + & 2 & -35 \\ + & 2 & -35 \end{array}$	$ \begin{array}{c cccc} -72 & 53 \\ -72 & 30 \\ -72 & 57 \\ -73 & 03 \\ -72 & 38 \end{array} $	Heavy sea from W.S.W., very unsteady, steering very
	-60 17	236 38	Mag. S. Direct. Direct. Def. N. Def. S.	$\begin{array}{c cccc} -72 & 52.0 \\ -73 & 01.1 \\ -72 & 59.1 \\ -71 & 56.0 \\ -73 & 02.3 \end{array}$	E. by s. E. by N. E. E.	$ \begin{array}{c cccc} + & 2 & -35 \\ + & 37 & -35 \\ + & 21 & -35 \\ + & 21 & -81 \\ + & 21 & -35 \end{array} $	$ \begin{vmatrix} -73 & 25 \\ -72 & 59 \\ -73 & 13 \\ -72 & 56 \\ -73 & 16 \end{vmatrix} $	Table more steady, and steering very well.
,	-60 24	237 29	Mag. N. Mag. N.S. Mag. S. Direct. Direct. Def. N.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	e. e. e. by n.	$ \begin{array}{c cccc} +21 & -35 \\ +21 & -35 \\ +21 & -35 \\ +21 & -35 \\ +37 & -35 \\ \end{array} $	$\begin{bmatrix} -73 & 24 \\ -73 & 14 \\ -73 & 13 \\ -73 & 16 \\ -73 & 06 \end{bmatrix}$	
			Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	$\begin{array}{c cccc} -72 & 17.2 \\ -73 & 09.0 \\ -73 & 09.7 \\ -73 & 06.2 \\ -73 & 07.2 \\ -73 & 07.1 \end{array}$	e. by n.	$ \begin{array}{r rrr} & +37 & -81 \\ & +37 & -35 \\ & +37 & -35 \\ & +37 & -35 \\ & +37 & -35 \\ & +37 & -35 \\ \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Table more steady, and steering very well.
19. 20. 21.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	240 57 245 29 247 17	Direct. Direct. Direct. Def. N. Def. S.	$\begin{array}{ccccc} -73 & 07^{\cdot 1} \\ -71 & 59^{\cdot 1} \\ -72 & 17^{\cdot 9} \\ -71 & 23^{\cdot 1} \\ -70 & 26^{\cdot 9} \\ -71 & 26^{\cdot 8} \end{array}$	e. by n. e.n.e. e. by n. e. by n. e. by n.	$ \begin{array}{rrrr} +37 & -35 \\ +53 & -35 \\ +78 & -35 \\ +37 & -35 \\ +37 & -81 \\ +37 & -35 \\ \end{array} $	$egin{array}{cccccccccccccccccccccccccccccccccccc$	Strong gale, heavy sea, steering badly.
	59 00	248 49	Mag. N. Mag. N.S. Mag. S. Direct. Direct.	$\begin{array}{c cccc} -71 & 32.0 \\ -71 & 20.1 \\ -71 & 22.7 \\ -71 & 20.9 \\ -71 & 53.4 \end{array}$	E. by N. E. by N. E. by N. E. by N. N.E. \(\frac{1}{2} \) E.	$ \begin{array}{c cccc} +37 & -35 \\ +37 & -35 \\ +37 & -35 \\ +37 & -35 \\ +73 & -35 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Cross sea, slight motion. Head sea, table unsteady.

i.				Observed		Corre	ctions.		
1842.	Lat.	Long.	Method employed.	Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Mar. 22.	58 26	251 42	Direct.	_7°1 0′6·1	E. by N.	+37	3´5	-71 047 ° ′	j.
			Def. N.	-70 01:3	E. by N.	+37	-81	-70 45 70 49	
		, ,	Def. S. Mag. N.	$-70 45.2 \\ -71 03.3$	E. by N.	+37 +37	$-35 \\ -35$	$\begin{vmatrix} -70 & 43 & \\ -71 & 01 & > -70 & 55 \end{vmatrix}$	Cross sea, unsteady.
			Mag. N.S.	$-70 \ 44.0$	E. by N.	+37	-35	$\begin{bmatrix} -71 & 01 \\ -70 & 42 \end{bmatrix}$	cross sea, unsteauy.
			Mag. S.	-71 07.8	E. by N.	+37	-35	-71 06	
			Direct.	-71 02.9	E. by N.	+37	-35	$-71 \ 01$	
23.	-58 33	254 45	Direct.	-70 24·7	E. $\frac{1}{2}$ N.	+30	-35	$-70 \ 30$	
			Def. N. Def. S.	$ \begin{array}{r rrr} -69 & 05.4 \\ -69 & 57.5 \end{array} $	$E. \frac{1}{2} N.$	+30	$-81 \\ -35$	$ \begin{array}{c cccc} -69 & 56 \\ -70 & 03 \end{array} $	
			Mag. N.	-70 02.7	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	$+30 \\ +30$	-35		Slight motion.
			Mag. N.S.	$-70 \ 21.7$	$E \cdot \frac{1}{2} N \cdot$	+30	-35	-70° 27	ongite motion.
			Mag. S.	—70 10·1	E. $\frac{1}{2}$ N.	+30	35	$-70 \ 15$	
			Direct.	-70 31·2	E. $\frac{1}{2}$ N.	+30	_35	$-70 \ 36$	
24.	$-58 \ 40$	257 32	Direct.	$-70 \ 01.8$	E. by N.	+37	—35	-70 00)
			Def. N. Def. S.	-69 09.1 $-69 43.7$	E. by N.	$+37 \\ +37$	_81 _35	$ \begin{array}{c c} -69 & 53 \\ -69 & 42 \end{array} $	
			Mag. N.	$-69 \ 47.0$	E. by N.	$+37 \\ +37$	-35	$\begin{bmatrix} -09 & 42 \\ -69 & 45 \end{bmatrix}$	
			Mag. N.S.	$-69 \ 37.4$	E. by N.	+37	-35	_69 35	Slight motion.
			Mag. S.	—70 03·0	E. by N.	+37	_35	$-70 \ 01 \ -69 \ 50$	
			Direct.	-70 01.8	E. by N.	+37	35	-70 00	
			Direct.	-69 52.9	Е.	+22	_35	-70 06	J
	-5849	258 13	Direct.	-69 51·1	E. by N.	+37	_35	$-69 \ 49$	Table steady, very
05	-5853	258 55 263 35	Direct. Direct.	$\begin{vmatrix} -69 & 24 \cdot 2 \\ -69 & 17 \cdot 9 \end{vmatrix}$	E. by N.	+37	-35 -35	$ \begin{array}{ccc} -69 & 32 \\ -69 & 00 \end{array} $	} slight motion.
	$-58 54 \\ -58 59$	267 50	Direct.	-68 19.8	E.N.E. E. by N. ½ N.	$+53 \\ +44$	—35	_68 11	
~ 0.	00 03	20, 00	Def. N.	-67 03.0	E. by N. $\frac{1}{2}$ N.		_81	$-67 \ 40$	
			Def. S.	-68 05.4	E. by N. $\frac{1}{2}$ N.		_35	-67.56 i a	
			Mag. N.	-67 44.2	E. by N. $\frac{1}{2}$ N.			-07 33	Heavy sea, steering badly, a little mo-
			Mag. N.S.	-67 52·6	E. by N. $\frac{1}{2}$ N.	+44	_35	$-67 \ 44$	tion.
			Mag. S. Direct.	$ \begin{array}{r rrrr} -67 & 52.5 \\ -68 & 15.6 \end{array} $	E. by N. $\frac{1}{2}$ N.	+44	-35	$\begin{bmatrix} -67 & 44 \\ -68 & 07 \end{bmatrix}$	
27.	-59 01	272 06	Direct.	-67 19.3	E. by N. $\frac{1}{2}$ N. E.N.E.	$ +44 \\ +52 $	$-35 \\ -35$	-67 02	
21.	-09 01	212 00	Def. N.	$-66\ 46.0$	E.N.E.	+52	-81	$-67 02 \\ -67 15$	
			Def. S.	-67 09·6	E.N.E.	+52	-35	-66 53	
			Mag. N.	-6653.0	E.N.E.	+52	-35	$-66 \ 36 \ -66 \ 53$	A swell from the
			Mag. N.S.	-6659.0	E.N.E.	+52	-35	-00 42	W.S.W., ship
			Mag. S. Direct.	$\begin{vmatrix} -67 & 05.8 \\ -67 & 17.8 \end{vmatrix}$	E.N.E.	+52	-35	-66 49	unsteady.
			Direct.	$-67 \ 17.8$ $-67 \ 04.7$	E.N.E.	$+52 \\ +52$	$-35 \\ -35$	$ \begin{array}{c c} -67 & 01 \\ -66 & 48 \end{array} $	
28.	-58 54	276 18	Direct.	$-66 \ 51.5$	N.E. by E.	+64	-35	-66 23	
~3.			Def. N.	$-65\ 48.2$	N.E. by E.	+64	-81	-66 05	
			Def. S.	-66 53.4	N.E. by E.	+64	-35	-66 24	
			Mag. N.	-66 15·2	N.E. by E.	+64	-35	$-65 \ 46 > -66 \ 10$	Swell from the
			Mag. N.S.	$\begin{vmatrix} -66 & 18.7 \\ -66 & 51.6 \end{vmatrix}$	N.E. by E.	+64	-35	-65 50	W.S.W., ship un- steady.
			Mag. S. Direct.	$-66 \ 51.8$	N.E. by E.	$^{+64}_{+64}$	$-35 \\ -35$	$ \begin{array}{c c} -66 & 23 \\ -66 & 23 \end{array} $	
29.	-58 25	279 44	Direct.	-65 05.3	N.E. by E.	+62 + 62	-35	$-64 \ 38$	
~3.			Direct.	-65 27.9	N.E. by E.	+62	-35	-65 01	
			Def. N.	_64 13.0	N.E. by E.	+62	-81	-64 32	
			Def. S.	-65 20.9	N.E. by E.	+62	-35	$-64 \ 54 \ -64 \ 44$	Swell from S.W.,
			Mag. N.	-65 03·0	N.E. by E.	+62	-35	-04 30	slight motion.
			Mag. N.S.	$\begin{bmatrix} -65 & 01.6 \\ -65 & 08.8 \end{bmatrix}$	N.E. by E.	+62	-35	$ \begin{array}{c c} -64 & 35 \\ -64 & 42 \end{array} $	
			Mag. S. Direct.	-65 22.6	N.E. by E.	$ +62 \\ +62$	$-35 \\ -35$	$\begin{bmatrix} -64 & 42 \\ -64 & 56 \end{bmatrix}$	
				~~ 0	11.11. Ny 11.	1.02	00	01,00	

						Correc	ctions.		
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	True Inclination.	Remarks.
Mar. 30.	58 31	281 33	Direct. Direct. Def. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.N.E. N.E. by E. N.E. by E.	+51 +62 +62	-35 -35 -81	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	·
	-58 30		Def. S. Mag. N. Mag. N.S. Mag. S. Direct. Direct.	-64 11.8 -64 05.6 -64 09.8 -64 27.0 -64 17.7 -64 14.9	N.E. by E.	$ \begin{array}{r} +62 \\ +62 \\ +62 \\ +62 \\ +62 \\ +62 \end{array} $	-35 -35 -35 -35 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Swell from S.W., slight motion.
31.	—58 36	285 33	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. Direct.	$\begin{array}{c} -63 \ 42.0 \\ -62 \ 50.6 \\ -63 \ 49.8 \\ -63 \ 22.5 \\ -63 \ 17.2 \\ -63 \ 24.6 \\ -63 \ 44.5 \end{array}$	N.E. N.E. N.E. N.E. N.E. N.E.	+69 +69 +69 +69 +69 +69	-35 -81 -35 -35 -35 -35	$ \begin{array}{c c} -63 & 08 \\ -63 & 03 \\ -63 & 16 \\ -62 & 49 \\ -62 & 43 \\ -62 & 51 \\ -63 & 11 \end{array} $	Swell from S.W., slight motion.
April 1.	-57 21	289 36	Direct. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	$\begin{array}{cccc} -62 & 26.9 \\ -61 & 16.8 \\ -62 & 04.7 \\ -62 & 04.4 \\ -62 & 12.7 \\ -62 & 12.4 \end{array}$	N.E. by N.	+71 +71 +71 +71 +71 +71 +71	-35 -81 -35 -35 -35 -35	$ \begin{bmatrix} -61 & 51 \\ -61 & 27 \\ -61 & 29 \end{bmatrix} $	Ship unsteady, steer- ing very wildly.
2.	—57 26	291 32	Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c} -62 & 12.4 \\ -62 & 17.0 \\ -58 & 55.8 \\ -57 & 57.1 \\ -58 & 43.2 \\ -58 & 49.5 \\ -58 & 29.2 \end{array}$	N.E. by N. S.E. S.E. S.E. S.E.	+71 +71 -33 -33 -33 -33 -33	-35 -35 -81 -35 -35 -35	$ \begin{array}{cccc} -61 & 41 \\ -60 & 04 \\ -59 & 51 \\ -59 & 51 \\ -59 & 58 \end{array} $	Heavy sea, ship un- steady.
3.	$-57 25 \\ -56 37$	292 02 294 34	Mag. S. Direct. Direct. Direct. Def. N. Def. S. Mag. N.	-58 23·7 -58 59·8 -58 22·4 -59 50·8 -58 33·4 -59 43·5 -59 19·3	S.E. S.E. S.S.E. N.E. N.E. N.E.	$ \begin{array}{r} -33 \\ -33 \\ -62 \\ +65 \\ +65 \\ +65 \\ +65 \\ \end{array} $	-35 -35 -35 -35 -81 -35 -35	-59 32 -60 08 -59 59 -59 21 -58 49 -59 13	Steering badly.
4.	-54 48	297 21	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N.	-59 26·3 -59 21·8 -59 45·5 -57 27·0 -56 43·5 -57 23·2 -57 10·4	N.E. N.E. N. by E. N. by E. N. by E. N. by E.	$ \begin{array}{r} +65 \\ +65 \\ +66 \\ +66 \\ +66 \\ +66 \\ \end{array} $	-35 -35 -35 -35 -81 -35 -35	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Heavy sea, strong
5.	-52 40	299 52	Mag. N.S. Mag. S. Direct. Direct. Def. N. Def. S. Mag. N. Mag. N.S.	$\begin{array}{c} -57 & 13\cdot 4 \\ -57 & 11\cdot 0 \\ -57 & 19\cdot 0 \\ -54 & 40\cdot 0 \\ -53 & 51\cdot 3 \\ -54 & 43\cdot 4 \\ -54 & 31\cdot 9 \\ -54 & 22\cdot 3 \end{array}$	N. by E. N. by E. N. by E. N.N.E. N.N.E. N.N.E. N.N.E. N.N.E.	$+66 \\ +66 \\ +66 \\ +58 \\ +58 \\ +58 \\ +58 \\ +58 \\ +58 \\ +68 $	-35 -35 -35 -35 -81 -35 -35 -35	56	breeze, steering badly.
	-52 35 -52 28	300 33 300 42	Mag. S. Direct. Direct. Direct. Def. N. Def. S.	$\begin{array}{r} -54 & 32.3 \\ -54 & 15.0 \\ -54 & 32.3 \\ -53 & 51.0 \\ -53 & 08.3 \\ -52 & 26.4 \\ -53 & 07.9 \end{array}$	N.N.E. N.N.E. N.N.E. N. by E. N. by E. N. by E.	$ \begin{array}{r} +58 \\ +58 \\ +58 \\ +57 \\ +57 \\ \end{array} $	-35 -35 -35 -35 -81 -35	-53 42 -54 09 -53 28 -52 46 -52 50	Ship steady.

Mothed Observed Direction of	Corrections.		
1842. Lat. Long. employed Inclination. shin's head	Ship's attraction. Index.	True Inclination.	Remarks.
April 5. $-5\overset{\circ}{2}\overset{2}{2}\overset{2}{8}$ $3\overset{\circ}{0}\overset{\circ}{0}\overset{4}{2}$ $\overset{\circ}{4}$ $\overset{\circ}{4}}$ $\overset{\circ}{4}$ $\overset{\circ}{4}$ $\overset{\circ}{4}$ $\overset{\circ}{4}$ 4	+57 -35 +57 -35 +57 -35 +57 -35 +57 -35 +54 -35 +54 -35 +54 -35 +54 -35 +32 -35 +32 -81 +32 -35 -35 -35 -35 -35 -35 -35 -35 -35 -35	$ \begin{array}{c cccc} -52 & 06 \\ -52 & 13 \\ -52 & 07 \\ -52 & 07 \\ -52 & 21 \\ -52 & 33 \\ -52 & 07 \end{array} $	Ship steady. Strong breeze, slight motion. Single anchor.

	Direct $-\overset{\circ}{5}2$ $\overset{\checkmark}{4}9.6$		Direct $-\overset{\circ}{5}$ 2 $\overset{\checkmark}{4}$ 8.7
	Def. N53 05·3		Def. N53 42.2
* Observed on shore;	Def. S 52 48·3	† Observed on shore;	Def. S52 48.4
face west.	Mag. N53 00.8	face west.	Mag. N53 00.4
	Mag. N.S53 09.7		Mag. N.S53 06.2
	LMag. S −53 12·1		Mag. S53 05.4
	Direct52 39.5		Direct52 41.5
	Def. N 53 30·8		Def. N53 46.8
† Observed on shore;	Def. S52 57.9	§ Observed on shore;	Def. S52 56.4
face west.	{ Mag. N −53 05·7	face west.	Mag. N53 04.0
race west.	Mag. N.S53 01.8		Mag. N.S53 02.4
	Mag. S53 12.7		Mag. S53 07.6
	Direct52 38.6		

						Corre	ctions.						ú
1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Ship's attraction.	Index.	2	True Inc	linati	ion.		Remarks.
Aug. 15.		y Sound, d Islands.	Direct. Def. N.	-51 31·4 -51 00·8 -51 45·5 -51 21·2 -51 29·1 -51 06·2 -50 44·9 -50 23·4 -50 23·8 -49 38·9 -50 43·1 -50 03·0 -50 48·4 -50 21·3 -51 11·2 -50 25·0 -51 31·3 -51 59·2 -52 05·8 -51 27·5 -52 13·7 -52 13·7 -52 13·6 -51 31·3 -51 31·3 -51 31·3 -51 31·3 -51 31·5 -52 13·6 -51 31·5 -52 13·6 -51 31·5 -52 13·6	E. ½ S. E. ½ S. E. £. E. E. E. E. E. S.E. S.E. S.E. S.S.E. S. S. W. S.W. S.W. S.W. W.S.W. N.W. W.S.W. N.W. N	$\begin{array}{c} & , 22 \\ +22 \\ +22 \\ +28 \\ +4 \\ -22 \\ -45 \\ -52 \\ -45 \\ -22 \\ -45 \\ -22 \\ -45 \\ -22 \\ +4 \\ +28 \\ +44 \\ +52 \\ +54 \\ +54 \\ +54 \\ +55 $	-81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35 -81 -35	$\begin{array}{c} -51 & 52 \\ -52 & 14 \\ -52 & 00 \\ -52 & 23 \\ -51 & 58 \\ -52 & 06 \\ -51 & 49 \\ -51 & 58 \\ -51 & 39 \\ -51 & 52 \\ -52 & 03 \\ -52 & 03 \\ -51 & 42 \\ -51 & 42 \\ -51 & 42 \\ -51 & 38 \\ -51 & 51 \\ -51 & 50 \\ -52 & 00 \\ -51 & 49 \\ -51 & 55 \\ -51 & 42 \\ -51 & 55 \\ -51 & 55 \\ -51 & 55 \\ -52 & 01 \\ -51 & 56 \\ \end{array}$	$\left. \left\{ \begin{array}{l} -5z \\ -52 \\ -52 \\ \end{array} \right\}$ $\left. \left\{ \begin{array}{l} -52 \\ -51 \\ \end{array} \right\}$ $\left. \left\{ \begin{array}{l} -51 \\ -51 \\ \end{array} \right\}$ $\left. \left\{ \begin{array}{l} -51 \\ -51 \\ \end{array} \right\}$ $\left. \left\{ \begin{array}{l} -51 \\ -51 \\ \end{array} \right\}$	02 54 46 06 54 42 45 55 53 48 52 58	} —51	56	
			Def. N. Direct. Def. N.	$ \begin{vmatrix} -51 & 11.7 \\ -52 & 13.6 \\ -51 & 33.5 \end{vmatrix} $	N.N.E. N.N.E.	+54 +54 +54	-81 -35 -81 -35 -81 -35	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$iggr\{ -51 \ -51 \ $	58 56			

Observations of the Intensity of the Magnetic Force made in Her Majesty's Ship Erebus, with Needle R. F. 5, between April 17, 1841, and August 23, 1842.

Observers Captain Sir James Clark Ross and Lieutenant Alexander Smith, R.N.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Apr. 19.	vatory, I	c Öbser- Hobarton. 147 24	Def. S. Def. N. wt. 6 grs. wt. 5 grs. wt. 4 grs. wt. 3 grs. wt. 2 grs.	56 28.6 53 02.6 42 55.7 34 23.5 26 47.7 19 37.2 13 02.8*	64 63 61 60 60 60	Observed on shore.	1.820		1.820	Deflector employed R. F. 4.
	At ancho river De	erwent.	Def. S. Def. S. Def. S. Def. S. Def. S.	56 40·5 56 44·8 56 34·3 56 26·1 56 24·4	44 44 45 45 47	N. N.E. N.E. E.N.E. E.	1.809 1.806 1.815 1.820 1.821	+·024 +·022 +·018 +·013	1.832 1.828 1.833	ī
1		To obtain corrections for the ship's attraction.	Def. S. Def. S. Def. S. Def. S. Def. S. Def. S.	56 17.8 55 52.9 55 46.5 55 42.7	47 48 50 48 48	E.S.E. S.E. S.S.E. S	1.825 1.846 1.851 1.854	+·004 -·006 -·016 -·023 -·026	1.825 1.819 1.830 1.828	1.830
		ain corrections attraction.	Def. S. Def. S. Def. S. Def. S.	55 48·7 55 51·0 56 10·3 56 17·8 56 15·3	48 48 48 48	s.s.w. s.w. w.s.w. w.	1.849 1.847 1.832 1.825 1.830	023 016 006 +-004 +-013	1 1.826 1.826 1.829 1.843	
July 7.		g out of n Bay.	Def. S. Def. S. Def. S. Def. S. Def. N.	56 30·5 56 29·0 56 32·8 55 37·6 52 16·3	49 48 48 49 47	N.W. N.N.W. N. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1.817 1.818 1.815 1.858 1.854	$ \begin{array}{c c} + \cdot 018 \\ + \cdot 022 \\ + \cdot 024 \\ \end{array} $	1.845 1.840 1.842 1.842	J
8. 9.	-43 00	148 28	Def. S. Def. N. Def. S. Def. N.	56 20·7 53 12·2 57 03·3 53 37·1	52 52 56 56	N.N.E. N.N.E. N.N.W. N.N.W.	1.823 1.807 1.790 1.785	$\begin{vmatrix} \\ \\ \\ \\ \\ \end{vmatrix} + \cdot 022$		A heavy head swell. A head swell.
	-40 54 $-37 50$ $-37 21$	149 13 150-22 151 33	Def. S. Def. N. Def. S.	57 07·3 53 51·6 54 45·9 58 08·0	54 60 56 61	n. by w. n. by w. n. by w. n. by w.	1·786 1·773 1·732 1·742	$ \begin{vmatrix} + \cdot 024 \\ + \cdot 024 \\ + \cdot 022 \end{vmatrix} $		
14.		151 48 151 21	Def. N. Def. N. Def. S. Def. N. Def. S.	54 59·1 55 08·5 59 41·8 55 55·6	61 58 60 60	N.E. N.W. by N. N.	1.722 1.715 1.676 1.679	+.027	1.7423	Much motion. Running along the land.
15.	Syd	n Island, Iney. 151 17	Def. N. wt. 6 grs. wt. 5 grs. wt. 4 grs. wt. 3 grs.	59 09·0 55 35·9 46 51·7 37 43·3 29 09·2 21 13·7	53 55 55 55 55 55	Observed on shore.	1.698 1.694 1.698 1.680 1.683 1.687	 	1.685 1.685	The results with the face west are included in the
			wt. 2 grs. Def. S. Def. N.	13 57·4 59 11·4† 55 38·1	56 52 52		1.703 1.696 1.692			mean.

wt. 6 grs 43 07.5	Ther. 58		wt. 6 grs 47 32.4	Ther. $6\overset{\circ}{3}$	1.688
wt. 5 grs 34 51.5	Ther. 58	† Observed on	wt. 5 grs 37 38.9	Ther. 63	1.704
wt. 4 grs 27 02.7	Ther. 58	shore; face	\frac{\text{wt. 4 grs 29 32·1}}	Ther. 64	1.680
		west.	wt. 3 grs 21 51.4	Ther. 63	1.667
Wt. 2 grs 13 14.5	Ther. 60		Lwt. 2 grs 14 32.6	Ther. 64	1.662
	wt. 5 grs 34 51·5 wt. 4 grs 27 02·7 wt. 3 grs 19 55·5	wt. 6 grs 43 07.5 Ther. 58 wt. 5 grs 34 51.5 Ther. 58 wt. 4 grs 27 02.7 Ther. 58 wt. 3 grs 19 55.5 Ther. 60 wt. 2 grs 13 14.5 Ther. 60	wt. 5 grs34 51.5 Ther. 58 + Observed on wt. 4 grs27 02.7 Ther. 58 + shore; face wt. 3 grs19 55.5 Ther. 60	wt. 5 grs 34 51.5 Ther. 58 † Observed on wt. 5 grs 37 38.9 wt. 4 grs 27 02.7 Ther. 58 shore; face wt. 4 grs 29 32.1 wt. 3 grs 19 55.5 Ther. 60 west.	wt. 5 grs 34 51.5 Ther. 58 + Observed on wt. 5 grs 37 wt. 5 grs 37 38.9 Ther. 63 wt. 4 grs 27 02.7 Ther. 58 wt. 4 grs 29 32.1 Ther. 64 wt. 3 grs 19 55.5 Ther. 60 west. wt. 3 grs 21 51.4 Ther. 63

1841.	Lat.	Long.	Method employed.	defle	de of ection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.		rected ensity.	Remarks.
July 15. Aug. 1.		151 17 anchor.	Def. S. Def. S.	58	11·5 21·4	64 61	W. S.	1·696 1·733	+·007 -·032	1.701		
		-	Def. S.		15.6	61	s.s.w.	1.737	028		>1.705	
3.			Def. S.		29.0	63	N.E.	1.684	+.025		(- , 00	
5.		g out of	Def. S.		09.4	63	E. by N.	1.698	+.011	1.709		
6		bour.	Def. N.		46.8	$\frac{63}{63}$	E. by N.	1.686	+.011	-)	
6.	-32 32	154 07	Def. S. Def. N.		25·6 52·6	63	E. by N.	1.686 1.681	\rightarrow +.011	1.694	1.694	
7.	-33 51	157 18	Def. S.		05.3	60	е. by n. е. by n.	1.660	1			
	-33 31	10/ 10	Def. N.		30.2	61	E. by N.	1.652	} + •011	1.667	1.667	Much motion.
8.	-33 27	160 43	Def. S.		18.0	63	E. by N.	1.651	1		_	
Ů.	-00 24	100 10	Def. N.	1	53.1	64	E. by N.	1.638	+.011	1.655	1.655	
9.	—33 38	163 42	Def. S.	1	24.0	60	E.	1.647		- 0	- 0	
,	00 00	200 12	Def. N.	Į.	14.4	61	E.	1.623	} +.007	1.642	1.642	
10.	-33 41	166 23	Def. S.		22.7	63	N.E.	1.609	1	- Car	1 Cor	
	00 11		Def. N.		01.2	61	N.E.	1.591	+ .025	1.625	1.625	9
11.	-33 22	167 40	Def. S.		19.8	65	E. by N.	1.611	1	1.617	1.61#	
			Def. N.		49.4	67	E. by N.	1.599	+.012	1.017	1.617	
12.	-3258	169 20	Def. S.	61	40.0	56	E.N.E.	1.598	} +.017	1.607	1.607	
			Def. N.	58	14.8	56	E.N.E.	1.582	7 + 017	1.007	1.007	
13.	-3212	170 27	Def. S.	62	24.2	56	s.e. by e.	1.572	}012	1.560	`	
			Def. N.	58	24.4	55	s.E. by E.	1.576	3 - 012	1.302		Much motion.
15.	-33 55	171 54	Def. S.	61	35.7	60	E. $\frac{1}{2}$ S.	1.590	}+.004	1.503	1.583	A head sea.
			Def. N.		05.6	60	E. ½ S.	1.588	1	1 000	(1000	
17.	-34 29	173 36	Def. S.		20.0	62	E.S.E.	1.611	006	1.594		Much motion.
		1	Def. N.		02.7	62	E.S.E.	1.590	J	-		
20.	At a	nchor.	Def. S.		57.7	66	N.W. $\frac{1}{2}$ N.	1.587	+.025	1.612	1.607	
			Def. S.		42.9	63	s.	1.634	032	1.602	}•	
23.		Islands,	Def. S.		41.1	58		1.599				
		Zealand.	Def. N.		00.0	56		1.592				
	-35 10	174 00	wt. 6 grs.		38.1	58		1.604				
			wt. 5 grs.		10.5 55.0	58 59		1.594 1.597				
			wt. 4 grs. wt. 3 grs.		47.5	59		1.578				
o de la companya de l			wt. 2 grs.		59.3*	59		1.590				
Oct 27	_35 16	174 00	Def. S.		45.2	67	Observed					
000.27.	-00 10	171 00	Def. N.		47.1	70	on shore.		\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	1.594	1.594	The results with the face west are in-
			wt. 6 grs.		35.0	71		1.608				cluded in the mean.
			wt. 5 grs.		59.3	70		1.603				incan.
			wt. 4 grs.		30.6	70		1.619				
			wt. 3 grs.		45.0	70	11	1.583				
			wt. 2 grs.	14	43.2	68		1.620				
			Def. S.	61	$54 \cdot 4$	65		1.590				
Property Company			Def. N.		09.1	65	IJ	1.586				
Nov. 23.	-35 15	174 39	Def. S.	61	00.9	63	E.S.E.	1.623	006	1.611	1.611	
į			Def. N.	57	29.1	63	E.S.E.	1.611]	1 011	. 011	1
24.	-36 27	177 34	Def. S.		26.7	65	E.S.E.	1.607		1.612	1.612	2
1			Def. N.	57	12.7	64	E.S.E.	1.625	1			
<u> </u>		MATERIAL TRANSPORT AND DESCRIPTION OF A SECURITION OF A		CONCRETE SERVICE						<u> </u>		

	(wt. 6 grs 51	2 6·0	Ther. 61	Intensity. 1.591		wt. 6 grs 51	3 8•7	Ther. $6\overset{\circ}{5}$	Intensity. 1.588
* Observed on	wt. 5 grs 40	52.0	Ther.60	1.590	† Observed on	wt. 5 grs 40	51.0	Ther. 65	1.591
shore; face	wt. 4 grs 30	26.9	Ther. 59	1.633	shore; face	wt. 4 grs 31	29.2	Ther. 65	1.586
west.	wt. 3 grs 23	17.9	Ther. 59	1.568	west.	wt. 3 grs 23	17.2	Ther. 64	1.570
	wt. 2 grs 15	23.3	Ther. 60	1.571		wt. 2 grs 15	11.1	Ther. 64	1.593

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Nov. 25.	_3°8 1′7	179 á1	Def. S Def. N.	60 44·4 56 57·2	62 62	s.e. by s.	1·633 1·634	}020	1.614 1.614	
26.	-39 01	182 12	Def. S.	62 02.7	59	E. by s.	1.585	}000	1,605)	Very much motion.
27.	-39 18	182 58	Def. N. Def. S.	57 12·9 60 16·0	57 64	E. by s.	1.625 1.652	1	>1.615	
			Def. N.	56 29.9	62	s.	1.654	-028	1.625	
28.	-40 47	183 03	Def. S. Def. N.	59 58·5 56 03·4	62 65		1.664 1.674	}010	1.659 1.659	-
29.	-41 49	183 41	Def. S.	59 05.1	65	s. by E.	1.701	-026	1.671 1.671	
30	-43 32	183 03	Def. N. Def. S.	55 37·2 58 24·9	65		1.693	= 020	1.0/1 1.0/1	-
30.	-45 52	100 00	Def. N.	54 54.9	59	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W.	1·732 1·724	-027	1.701 1.701	
Dec. 1.	-45 40	183 20	Def. S. Def. N.	58 32.2	63	s.E. by E.	1.725	-010	1.715)	A head sea.
2.	-47 19	184 40	Def. S.	54 58·7 57 40·9	63 57	s.e. by e. s.e. by e. $\frac{1}{2}$ e.	1.722 1.762	1	>1.730	A heavy swell.
			Def. N.	54 30·5 57 41·3	57	s.e. by E. $\frac{1}{2}$ E.	1.744] -·008	1.745	*
	-48 43	180 30	Def. S. Def. N.	54 10.1	51 51	s.e. by e.	1.762 1.760	1 1	1.752	
ĺ,	40.00	105 41	wt. 2 grs.	13 28.0	51	E.S.E.	1.765	005	1.760	
4.	-49 20	187 41	Def. S. Def. N.	57 45·8 54 13·1	55 55	E. by s.	1.757 1.758			
1			wt. 3 grs.	20 30.2	53	E. by s.	1.745	.000	1.752	
5	-49 27	189 13	wt. 4 grs. Def. S.	27 58·0 57 32·7	53 55	E. by s. E. by s.	1.750 1.770	K	- 3:	
	1 23 2.	100 10	Def. N.	54 16.0	55	E. by s.	1.757			*
			wt. 3 grs. wt. 4 grs.	20 18·0 27 32·0	56	E. by s.	1.762 1.775	·000	1.759 1.759	
l			wt. 5 grs.	36 30.1	56	E. by s.	1.729]		
6	-50 00	191 00	Def. S. Def. N.	57 30·2 54 13·5	51	E. by s.	1.771	ו		÷
			wt. 3 grs.	20 22.2	51	E. by s.	1.758 1.754	·000	1.763	
			wt. 4 grs.	27 16.5	51	E. by s.	1.789			
7	_50 48	192 20	wt. 5 grs. Def. S.	36 07·2 57 07·9	51 51	E. by S. s.E. by E.	1.742 1.787	K	1.766	
			Def. N.	53 45.7	51	s.e. by e.	1.779	7-009	1.774	
8	$-51 \ 34$	194 29	Def. S. Def. N.	57 06·4 53 15·7	52 50	E. by s.	1.789 1.804		*	
*			wt. 3 grs.	20 09.1	48	E. by s.	1.771	> .000	1.792 1.792	
			wt. 4 grs. wt. 5 grs.	26 59·7 34 58·0	48	E. by s.	1.804 1.791		1	Weight 5, unsteady.
9	-52 21	197 53	Def. S.	56 44.5	45	E. by s.	1.805	15	1.801	Weight of anstowny
10	-53 01	202 11	Def. N. Def. S.	53 25·1 56 21·2	44 48	E. by s.	1.797	{		Much motion.
			Def. N.	53 27.0	47	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.824		1.815 >1.808	3
11	-5248	203 50	Def. N. Def. S.	53 13·3 56 45·0	45 46	E.	1.807		1.000	A head swell.
			wt. 3 grs.	19 57.7	46	E. E.	1.805 1.797		1.809	
12	-53 01	205 08	Def. S.	56 37.4	45	E.S.E.	1.811	1		
			Def. N. wt. 3 grs.	52 57·3 19 46·7	44 45	E.S.E.	1.818		1.810 1.810	
1			wt. 4 grs.	26 41.5	45	E.S.E.	1.823			÷
13	-54 58	209 30	wt. 5 grs. Def. S.	34 25·7 56 08·7	45 52	1	1.815			
			Def. N.	52 26.0	51	s.E. by E. 1 E	. 1.846			
	-55 08	210 04	Def. S. Def. N.	56 02·2 52 30·7	49	s.e. by E. $\frac{1}{2}$ E s.e. by E. $\frac{1}{2}$ E			1.831 1.831	
	-55 20	210, 28	Def. S.	56 10.0	45	s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$.1.832			
	1		Def. N.	52 38.2	44	s.e. by e. ½ e	1.836	J		

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 14.	$-5^{\circ}6^{\circ}2^{'}0$	211 52	Def. S. Def. N.	55 38·9 52 01·3	51 51	s.e. by s. s.e. by s.	1·857 1·868		÷	
	Ji.		wt. 3 grs. wt. 4 grs. wt. 5 grs.	19 37·5 26 08·7 33 36·0	53 52 52	s.e. by s. s.e. by s. s.e. by s.	1.818 1.860 1.856	-016	1.836 1.836	
	56 55	211 38	wt. 6 grs. Def. S. Def. N.	42 36·0 55 33·2	52 43 43	s.e. by s. s.e. by ~.	1.830 1.863 1.868	7		
15.	-56 55		Def. S. Def. N.	51 59·7 55 28·0 52 17·0	41 40	s.e. by s. s.s.e. s.s.e.	1.865 1.856		1.843	
16.	-57 21 $-58 29$	212 46 213 11	Def. S. Def. N. Def. S.	55 29·8 52 10·0 55 19·7	42 41 42	F.S.E. E.S.E. S.S.E.	1.864 1.860 1.872	004	1.858 ∫	
10.	-5852		Def. N. Def. S.	51 52·9 54 57·6	42 41	S.S.E.	1.874 1.889			
			Def. N. wt. 3 grs. wt. 4 grs.	52 04·5 18 32·2 25 25·0	38 38	S.S.E. S.S.E. S.S.E.	1.865 1.916 1.906	} −.017	1.873 1.873	
17.	-61 03	213 57	wt. 5 grs. Def. S. Def. N.	32 31·2 54 19·2 51 06·0	38 39 36	S.S.E. S.S.E.	1.907 1.923 1.918] } ~·017		
	-61 37	71	Def. S. Def. N.	51 00·0 54 02·4 51 01·2	34 32	s.s.e. s. by e. s. by e.	1.939 1.922	-018	1.913	
	$-62 ext{ } 40$ $-63 ext{ } 23$		Def. S. Def. N. Def. S.	53 43·6 50 50·0 53 39·8	34 32 39	s. s. s.s.w.	1.953 1.931 1.958	019		
, ,	00 20		Def. N. Def. S.	50 26·0 54 33·8	38 42	s.s.w. \ Observed	1.954 1.910	017	1·939 1·939 1·923 1·923	
20.	-63 47	208 26	Def. N. Def. S. Def. N.	50 44.7 53 58.3 50 36.8	35 34	s. by w. s. by w.	1.936 1.941 1.944	1	1.924	
			wt. 3 grs. wt. 4 grs. wt. 5 grs.	18 22·9 25 05·6 32 11·8	35 34 34	s.w. by s.	1.938 1.935 1.926	-012	1.934	
21.	-64 38	206 53	wt. 6 grs. Def. S. Def. N.	40 03·5 54 00·1 50 35·6	34 32 31	s.w. by s.	1.926 1.940 1.944	} } -•016	1.926	
	-64 53	206 30	Def. S. Def. N.	53 34·4 50 23·4	44 39	s. by w. s. by w.	1.963 1.956 1.942	013	>1.933	
			wt. 3 grs. wt. 4 grs. wt. 5 grs.	18 15·6 24 39·8 31 35·1	33 33 33	s. by E.	1.959 1.955	015	1.934	
22.	-65 36	205 32	wt. 6 grs. Def. S. Def. N.	39 11·3 53 33·1 50 00·6	33 37 36	s. by E. s.	1.954 1.964 1.977	-016	1.954	
23.	-65 59	204 16	Def. S. Def. S. Def. N.	53 51·4 53 38·5 49 48·2	37 36	s. by w.	1.948 1.959 1.996	\\ \rightarrow \cdot \cd	1 1 1	
	-65 59		Def. S. Def. N.	53 31·5 50 05·6	39 35	s. s.	1.965 1.973	-014	1 1	
24. 2 5.			Def. S. Def. N. Def. S.	53 21·6 50 19·8 53 56·5	43 43 34		1.976 1.959 1.943	$\left \begin{cases}010 \\ +.002 \end{cases} \right $		fast to a piece of ice.
26.			Def. N. Def. S. Def. N.	50 19·4 53 43·3 50 16·2	35 30 30	s.e. by e. s.e. by e.	1.959 1.955 1.963	1]		
29	-66 24	203 51	Def. S. Def. S.	54 01·9 53 51·7	30 42	N.W. N.E.	1.939 1.947		1.953	

1842		Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan.	1.	_66 32	203 32	Def. S.	53 23.8	44	S.S.E.	1.972	012	1.9667	
	3.	-66 35	203 25		49 53·5 53 48·9	39	s.s.e. n. by w. $\frac{1}{2}$ w.		+.012	1.965	Fast to a piece of ice, the Terror distant 25 fathoms. (This
	6.	-66 0 6	204 24	Def. N. Def. S.	50 21·7 53 28·7	37	N. by w. $\frac{1}{2}$ w.	1.957 1.967	1 + 012	1.900	25 fathoms. (This result is not employed in the Map.)
	0.	00 00	204 24	Def. N.	50 01.7	38	s. s.	1.976			proyect in the map.)
				wt. 3 grs.	18 01.8	37	s.	1.964			
				wt. 4 grs. wt. 5 grs.	24 44:9 30 55:2	37 36	s. s.	1.953 1.994	>014	1.9557	
				wt. 6 grs.	38 50.1	36	s.	1.970			To the state of th
	7.	-66 13	204 25	Def. S.	53 38.9	33	s.	1.958		1,054	Sailing through
	Q	66_16	204 33	Def. N. Def. S.	50 07.5	32	N.W.	1.971 1.948	K		loose ice.
	0.	-00 12	204 96	Def. N.	50 32.2	35	N.W.	1.948		1.958	
				Def. S.	53 47.9	34	S.S.E.	1.951	012	1.939	
	10.	-65 59	204 12	Def. S. Def. N.	53 49.5	36	s.w. by w.	1.949		1.947	
				Def. N.	50 25 4	30	s.w. by w.	1.964			
				wt. 3 grs.	18 09.9	30	E.	1.951			
	200			wt. 4 grs.	24 37.5	30	E.	1.960		1.966	
				wt. 5 grs. wt. 6 grs.	31 12·1 38 45·9	30	E. E.	1.975 1.971		>1.957	•
	12.	65 54	203 32		53 33.4	32	s.w.	1 963		1.955	
			203 05	Def. S.	53 41.3	40	S.S.E.	1.957	010		
			-	Def. N. Def. S.	50 13·9 54 11·3	36 30	S.S.E.	1.965 1.932	}		
				Def. N.	50 46.1	30	N.N.E.	1.935		1.946	9=
	16.	-6549	202 02	Def. S.	54 03.1	45	1	1.938	j.		
			Population of the last of the	Def. N.	50 35.0	45		1.945			
				wt. 2 grs. wt. 3 grs.	12 13·0 18 32·4	50 54	Observed	1.940 1.992		1.943 1.943	
				wt. 4 grs.	24 49.3	54	on ice.	1.952		1 310 1 310	
				wt. 5 grs.	32 02.4	54		1.936			
,	91	66_40	202 40	wt. 6 grs. Def. S.	39 31·4 53 19·1	55 37	s. by E.	1.946 1.975	l'i		
•	21.		202 10	Def. N.	50 05.6	36	s. by E.	1.973	1 3 111.3	1.9617	
			204 01		50 24.8	34	N.	1.955		1.967	
	29.	-67 39	203 59	Def. S. Def. N.	53 28.8	31	s.s.w.	1.967	-012	1.957 >1.960	
	30.	-67 18	203 39		50 08.2	30	S.S.W. S.W. $\frac{1}{2}$ S.	1.971 1.961			
		-, -		Def. N.	50 06.7	36	$s.w. \frac{1}{2} s.$	1.972	>009	1.959	
	21	GH O	202 15	wt. 3 grs. Def. S.	18 00·0 53 36·7	34 35	$S \cdot W \cdot \frac{1}{2} \cdot S \cdot$	1.970			
	31.	-07 Z.	202 16	Def. N.	50 08.2	32	s.w.	1.961 1.971			
				wt. 3 grs.	18 19.6	33	s.w.	1.936	11	1.951 1.951	
	-			wt. 4 grs.	24 44.5	33	s.w.	1.953	11	1 901 1 901	
				wt. 5 grs. wt. 6 grs.	31 23·7 38 52·0	35	s.w.	1.965 1.968			
Feb.	2.	-68 0°	200 1	Def. S.	53 23.2	31	S.S.E. ½ E.	1.972	17	1.071~	
	1			Def. N.	49 46.2	31	S.S.E. 1 E.	1.992	-011	1.971	
	3.	-68 2.	200 0	Def. S. Def. N.	52 54·7 49 52·6	32	S.E. by S.	1.997 1.985		1.981	
	4.	-68 49	199 44		52 57.1	33	s.E. by s. s. $\frac{1}{2}$ E.	1.995		1.975	Much motion.
				Def. N.	49 51.4	30	S. \frac{1}{2} E.	1.987			
				wt. 3 grs.	18 05.7	30	S. 1 E.	1.961		1.974	-
				wt. 4 grs. wt. 5 grs.	23 55·7 31 02·0	30	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	2.014			
		was to provide out the		1			2				

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 5.	-6859	19 [°] 5 51	Def. S.	53 13·7	33	s.w. by s.	1.981		1.972	
6	-69 48	192 25	Def. N. Def. S.	50 07·0 52 42·1	32 36	s.w. by s. s. by w.	1.972 2.010	{		+
0.			Def. N.	49 49.0	34	s. by w.	1.989	} -∙00 8	1.991	A great deal of me
7.	-70 05	191 10	Def. S.	52 46.1	29	s.w.	2.006		2.008	A great deal of mo- tion.
			Def. N. Def. S.	49 18·3 53 21·7	29 33	s.w.	2·020 1·973	Į.		
			Def. N.	49 52.7	30	s.s.w.	1.985		1.972	
8.	-70 18	186 01	Def. S.	53 05·0 49 46·8	37 33	s.	1.989]	
			Def. N. wt. 3 grs.	18 21.8	31	S. S.	1.991 1.931			
			wt. 4 grs.	24 06.1	31	s.	2.001	}−.009	1.977 >1.980	
			wt. 5 grs.	30 40.6	31	s.	2.006			
0	-70 39	185 31	wt. 6 grs. Def. S.	38 05·3 52 56·5	30 32	s. s.e. by s.	2·001 1·996	~		
9.	10 03	100 01	Def. N.	49 47.4	29	s.E. by s.	1.991	} -·006	1.987	,
10.	-70 06	181 50	Def. S.	53 09.0	33	w. by s.	1.985		1.981)	A head swell.
11	-70 10	181 34	Def. N. Def. N.	50 00·2 50 03·7	31 33	w. by s. s.w.	1.978 1.975	1	1.972 >1.983	March are stirm
11. 12.	-70 10		Def. S.	52 49.2	33	s.e. by s.	2.003)	1.000	
	ĺ		Def. N.	49 45.7	32	s.E. by s.	1.992	j	1.992	A heavy cross sea.
13.	-7246	181 46	Def. S.	52 55·6 49 45·5	34	s.E. by s.	1.997			
_	İ		Def. N. wt. 3 grs.	18 17.2	32 31	s.e. by s. s.e. by s.	1·992 1·940	}−.003	1.973 1.973	3-
			wt. 4 grs.	24 23.0	31	s.e. by s.	1.975	J	,	
16.	-74.56	173 36	Def. S.	53 16.1	26	S.S.E.	1.979)		
			Def. N. wt. 3 grs.	49 49·5 17 23·0	26 26	S.S.E. S.S.E.	1.988 2.036	}−.003	1.998	
	-75 10	173 08	Def. S.	52 39.5	36	E.	2.017	ጎ		
			Def. N.	49 45.9	30	. E.	1.992	}	2.008	Very unsteady.
	1		wt. 3 grs. wt. 4 grs.	17 20·9 23 58·7	27 27	E. E.	2·039 2·009	>+.001	2.009	
			wt. 5 grs.	30 59.1	28	· E.	1.987		*	
	TO 00		wt. 6 grs.	38 02.3	27	E.	2.002		J	•
17.	-76 00	175 15	Def. S. Def. N.	52 38·3 49 33·5	33 31	E.N.E. E.N.E.	2·014 2·004		2.010	
18.	-7658	181 03	Def. N.	53 00.7	28	E.N.E.	1.993	1	0000	
			Def. N.	49 29.3	27	E.N.E.	2.009	} + 002	2.003 >2.005	4.
19.	-7642	184 09	Def. S.	53 06.2	25	N. by E.	1.988		2.001	Ship pitching.
22.	-76 42	194 48	Def. N. Def. S.	49 31·3 52 59·0	25 30	и. by е. и. by е.	2·007 1·993	1	1.0003	
~~.			Def. N.	49 41.0	28	N. by E.	1.997	} + 004	1.999	
	-77 05	194 38	Def. S.	53 10·6 49 57·5	36	E. by s.	1.081			
			Def. N. wt. 3 grs.	18 06.5	33 29	E. by s.	1.981 1.960		1.993	A swell from the south.
			wt. 4 grs.	23 18.7	29	E. by s.	2.063		1.991	soum.
	7		wt. 5 grs.	31 25.7	29	E. by s.	1.961		,	
o E	-74 50	193 45	wt. 6 grs. Def. S.	38 04·1 53 14·8	29 30	E. by s. w.	2·000 1·980	ጎ .	J	
20.	7 7 50	130 10	Def. N.	49 54.3	29	w.	1.984		1.983 1.983	
26.	-7246	189 59	Def. S.	53 30.5	37	n.w. by w.	1.966	1 4.000	1.972	
0 #	-72 01	187 35	Def. N.	50 04·5 53 32·7	31 26	w. by w.	1.974 1.964	4	>1.974	
21.	-12 01	101 99	Def. S. Def. N.	49 49.1	25	w. by s.	1.989		1.976	
28.	-7108	184 59	Def. S.	53 27.6	31	w.	1.968	1 4.001	1.975	
			Def. N.	49 57.0	26 95	w.	2.004	Į.	>1.993	
*			wt. 3 grs. wt. 4 grs.	17 39·5 23 52·0	25 25	w.s.w.	2·004 2·020		2.012	
			4.0. I 819.			1	1	1		

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar 1	$-69 \ 52$	180 00	Def. S.	53 10·7	$ \stackrel{\circ}{33}$	w. by N.	1.983	7		
Mai. 1			Def. N.	50 06.0	31	w. by N.	1.972	+.003		A swell from the
1	-69 44	179 53	Def. S. Def. N.	53 28·1 50 09·7	32	n. by E.	1.968 1.969	+.007	1.976	northward.
2.	-68 04	183 25	Def. S.	54 05.0	33	N.N.E.	1.936	+.008	1.962	
			Def. N. Def. S.	50 06·7 53 46·5	32 34	N.N.E. N.E. by N.	1.972 1.951	1	>1.965	
	THE PARTY OF THE P		Def. N.	50 09.3	32	n.e. by n.	1.970	+.008	1.969	
3.	-67 32	185 09	Def. S. Def. N.	53 24·5 50 08·8	$\begin{array}{c c} 30 \\ 31 \end{array}$	E.N.E.	1.971 1.971	+.005	1.976	
5.	-67 16	188 10	Def. N.	50 40.2	35	N. by E.	1.941	1	1.952	A very heavy swell
6.		191 48	Def. N.	50 38.3	34	N. by E.	1.943	7 + 010	1 302).	from westward, observations very
7.	$-63 \ 30$	194 52	Def. S. Def. N.	54 11·9 50 54·2	40 35	N. by E.	1.930 1.927		1.0967	uncertain.
			wt. 3 grs.	18 26.2	33	N. by E.	1.925	+.010	1.936	
8.	-62 16	196 10	wt. 4 grs. Def. S.	25 10·3 54 52·7	33 35	n. by E.	1·922 1·893		>1.925	
		1,00 10	Def. N.	51 32.2	35	N. by E.	1.893	+.010	1.903	
9.	-61 14	198 38	Def. S.	54 38·4 51 23·2	43 35	n.e. by n.	1.907 1.902			
	Y		Def. N. wt. 3 grs.	19 06.9	33	n.e. by n.	1.859	>+·013	1.914	
			wt. 4 grs.	25 25.5	35	N.E. by N.	1.905			-
	-60 50	200 11	wt. 5 grs. Def. S.	$\begin{vmatrix} 32 & 00.5 \\ 55 & 00.4 \end{vmatrix}$	$\frac{34}{38}$	N.E. by N.	1.933 1.888	1	1.909	
1			Def. N.	51 37.2	35	E.N.E.	1.888	+.007	1.895	a constant
10.	-60 18	204 11	Def. S. Def. N.	55 52·5 51 56·5	$\frac{35}{34}$	E. by N.	1.844 1.871			Cross sea, ship very unsteady.
12.	$-60 \ 13$	211 34	Def. S.	55 28.0	35	E. by N.	1.862	+.005	1.869 1.869	A heavy swell, very unsteady.
14.	-59 24	218 58	Def. N. Def. S.	51 47·5 55 52·2	$\begin{array}{c} 35 \\ 37 \end{array}$	e. by n.	1.879 1.846	K	-	A heavy swell, very
1		210 00	Def. N.	52 20.0	37	N.E. by E.	1.851	>+.011	1.863	unsteady.
	-59 16	219 30	Def. S. Def. N.	55 37·4 52 18·2	$\frac{37}{37}$	n.e. by e.	1·859 1·853		>1.863	
r 5.	-58 04	222 04	Def. S.	55 54.2	37	E.N.E.	1.844	K		
			Def. N.	52 16·4 18 57·0	$\frac{37}{38}$	E.N.E.	1.844 1.876	+.009	1.864	-
16.	-59 04	228 57	wt. 3 grs. Def. S.	55 28.7	39	E.	1.864	+ .002	1.860)	
177	50.00	000 40	Def. N.	51 57·5 55 21·3	39 39	E. E. 1/2 S.	1.870 1.872	7 002		A great deal of mo-
17.	-59 39	232 48	Def. S. Def. N.	51 57.5	39		1.870	+.001		tion.
	-5945	233 53	Def. S	55 12.0	40	E. $\frac{1}{2}$ S.	1.879	L 401	20,00	
18.	-60 16	236 11	Def. N. Def. S.	51 41·2 54 40·7	38 36		1.885 1.901	nan.	1.897	Very unsteady.
			Def. N.	51 33.2	35	E. by s.	1.893	}	1.894	
-	-60 21	237 02	Def. S. Def. S.	55 00·2 55 12·5	$\frac{37}{39}$		1·888 1·879	+.003		Ship rolling, very unsteady.
- Constitution of the Cons			Def. N.	51 25.6	39	E.	1.899	<u> </u>		anomany.
	-60 20	237 50	Def. S. Def. N.	55 33·4 51 25·5	39 39		1·862 1·899	} + .009		
TTYNCOME	-60 19	238 00	Def. S.	55 10.2	40	E. by N. $\frac{1}{2}$ N.	1.880	1 +.010	1.894	
19.	-60 01	241 38	Def. N. Def. S.	51 37·9 55 58·9	$\frac{39}{39}$	E. by N. ½ N. E.N.E.	1.887	1	_	Much motion.
The state of the s			Def. N.	52 25.0	37	E.N.E.	1.846	+.011	1·851)	
Name of the Control o			Def. S. Def. N.	56 13·5 52 30·0	42 40		1·829 1·842			
21.	-59 15	248 12	Def. S.	56 07.0	39	E. by N.	1.836	} +.009	1.839	
	-58 58	249 24	Def. N. Def. S.	52 51·5 56 11·2	38 39		1·824 1·831	J		
	50 50	~ 20 ~ 2	Def. N.	52 56.0	38		1.820	} + .015	1.841	

			employed.	deflect Face ea	ast.	ture.	Ship's head.	Intensity	for ship's attraction.	Corre Inter		Remarks.
Iar. 22.	5°8 2′9	252 22	Def. S.	56 30	_ [88		1.816	} + .002	1.9165		
23.	-58 35	255 10	Def. N. Def. S.	53 05 56 36		88 84	= 1	1.812 1.812	\ \frac{1}{2}	1 810	1.807	A head sea.
			Def. N.	53 13	1	33		1.807			100,	-
25.	-58 44	257 49	Def. S.	56 35	. 1	36	~ {	1.812	>+.006	1・804ノ		- 1.
			Def. N. wt. 3 grs.	$\begin{vmatrix} 53 & 16 \\ 20 & 17 \end{vmatrix}$	• 1	35 34		1·803 1·756				
26.	-59 02	268 30	Def. S.	57 19			E. by N. $\frac{1}{2}$ N.		1			
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	00 010	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Def. N.	54 05			E. by N. $\frac{1}{2}$ N.		+.012	1.783		
27.	-59 02	272 02	Def. S.	58 55		37	• -	1.707	+.014	1.700	1.722	Ship unsteady.
	- *		Def. N.	55 17	- 1	35		1.708	\(\frac{1}{2} \tau \tau \tau \tau \tau \tau \tau \tau	1722	71700	
28.	-58 50	277 12	Def. S.	59 34	. 1	10		1.681	} +.018	1.694		
29.	-58 23	280 03	Def. N. Def. S.	$\begin{bmatrix} 56 & 07 \\ 60 & 45 \end{bmatrix}$	- 1	39 14	N.E. by E.	$\begin{array}{c} 1.671 \\ 1.633 \end{array}$	}	_		
29.	-00 20	280 03	Def. N.	57 03		5	4	1.631	\rightarrow + \cdot 019	1.651		
30.	-5829	282 04	Def. S.	60 30			N.E. by E. \(\frac{1}{2}\) E.		3		>1.639	
	00 100	707 01	Def. N.	57 08	- 1		N.E. by E. $\frac{1}{2}$ E.		+.016	1.651	>1.099	
31.	-58 29	286 04	Def. N.	58 34		15		1.570	+.024	1.594		A heavy swell from
Apr. 1.	-5722	289 50	Def. S.	63 22	- 1	17	N.E. by N.	1.539	+.025	1.554		the southward.
			Def. N.	60 00	- 1	7	N.E. by N.	1.519	1 + 1020	1 004	>1.532	
2.	-57 10	292 11	Def. S.	63 27	1	4	S.E.	1.535	}017	1.510	1 002	
	FC 40	22.4.40	Def. N.	59 57		4	S.E.	1.520	1	ر ۱۰۰۰		
3.	56 40	294 46	Def. S. Def. N.	$\begin{vmatrix} 65 & 36 \\ 61 & 36 \end{vmatrix}$	- 1	16	N.E.	1.465	+.023	1.466	1.466	
4.	-54 50	298 10	Def. N.	64 10		14	N.E.	1·469 1·395	+.023	1.400	1.400	
5.	-52 54		Def. S.	70 13		18	N.N.E.	1.342	\dashv			
	0.0 0 1	000 0,	Def. N.	66 55		15	N.N.E.	1.327				
			wt. 3 grs.	27 57	- 1	13	N.N.E.	1.300	>+.025	1.355	1.355	
			wt. 4 grs.	37 33	3.2 4	14	N.N.E.	1.340				
			wt. 5 grs.	49 40	• (14	N.N.E.	1.343	IJ			
11.		uis, Falk-	Def. S.	70 51	1	17)	1.328	Ŋ			
		Islands.	Def. N.	67 08	1	17		1.322				
	-51 32	301 53	wt. 2 grs.	18 31 27 49		15		1.291				
			wt. 3 grs. wt. 4 grs.	37 58	- 1	13		1·311 1·331				-
			wt. 5 grs.	48 5		13		1.361				
			wt. 6 grs.	66 49		13	Observed				1.000	The manufacturish th
lug. 19.			wt. 2 grs.	17 57		37	on shore.		}	1.322	1.322	The results with th
			wt. 3 grs.	27 43	3.3 3	37		1.310				included in the mean.
			wt. 4 grs.	37 40		37		1.339				
			wt. 5 grs.	49 31		38		1.347				
			wt. 6 grs.	67 23		38		1.339				
	*	-	Def. S. Def. N.	71 39 67 19		34		1.311				

	wt. 2 grs.	18 50.4	42	1.287
	wt. 2 grs. wt. 3 grs.	28 30.0	42	1.296
	wt. 4 grs.	38 51.0	41	1.315
	wt. 5 grs.	51 27.9	41	1.326
* Observed on shore;	wt. 6 grs.	68 40·3	41	1.332
face west.	wt. 2 grs.	18 32.9	39	1.306
	wt. 3 grs.	28 26.6	40	1.299
	wt. 4 grs.		40	1.309
	wt. 5 grs.	51 19.2	40	1.329
	wt. 6 grs.		40	1.324

Observations of the Intensity of the Magnetic Force made in Her Majesty's Ship Terror, with Needle F. C. B., between April 16, 1841, and August 15, 1842.

Observers Captain Francis Rawdon Crozier, and Mr. Thomas Moore, Mate, R.N.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera-	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Apr. 17.		on Mag- servatory. 147 24	Def. S. Mag. N.S. Mag. N.	33 20·4 39 59·2 30 04·0	60 60 60					A spare needle marked C. was used as a deflector, and the observa-
19.		Š	Def. S. wt. 1 gr.* wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	21 03·1 12 11·9 18 29·4 25 13·7 31 43·0 39 02·3	60 60 60 60 60	Observed on shore.	1.820		1.820	tions with it are those registered as "Deflector S." and "Deflector N." The deflect- ing magnets be- longing to the ap- paratus were also employed, N alone,
20.			wt. 3 grs. wt. 3½ grs. Def. N. Def. S. Mag. N.S. Mag. N.	36 00.6 33 25.6 40 11.6 30 24.1	60 60 60 60		*			and N. and S. con- jointly. The obser- vations with these are distinguished as "Mag. N.?" and "Mag. N.S." The temperatures are taken from the register in the
June 22.	At ancho river D	erwent.	Def. N. Def. N. Def. N.	35 58·5 35 49·1 35 34·5	48 48 48	W. W.S.W. S.W.	1.821 1.831 1.844			Erebus.
		To obtain corrections for the ship's attraction.	Def. N. Def. N. Def. N. Def. N. Def. N.	35 09·6 35 09·3 34 58·0 35 00·0 34 59·9	48 48 48 48 48	S.S.W. S. S.S.E. S.E. E.S.E.	1.868 1.868 1.879 1.877 1.877			
		otain corrections for ship's attraction.	Def. N. Def. N. Def. N. Def. N. Def. N.	35 06·4 35 13·9 35 18·4 35 21·6 35 23·0	48 48 48 48 48	E. E.N.E. N.E. N.N.E. N.	1.871 1.863 1.859 1.857 1.855		÷	
T 3 4	G,		Def. N. Def. N. Def. N.	35 23·7 36 04·1 35 21·4	48 48 48	N.N.W. N.W. W.N.W.	1.854 1.816 1.857		,	
July 7.		n Bay.	Def. N. Def. S. Def. N.	34 57·0 32 40·0 35 23·6	48 48 52	S.E. $\frac{3}{4}$ E. S.E. $\frac{3}{4}$ E. W. $\frac{1}{2}$ N.	1.880 1.864 1.854	-012	1.860	Very steady.
9.			Def. S. Def. N.	33 11·5 36 03·7	52 56	W. ½ N. N.N.W.	1.832 1.816	+.006	1.849	Very steady.
	-40 51	149 28	Def. S. Def. N.	33 57·6 36 33·8	56 56	n.n.w. n. by w.	1·785 1·787	+:022	1.822	Very steady.
	-38 17	150 22	Def. S. Def. N.	33 51·3 36 46·1	56 56	N. by w.	1·792 1·775	$\left \begin{array}{c} +.025 \\ +.027 \end{array} \right $	1.814	Very steady.
12.	-37 28	151 30	Def. S. Def. N.	34 43·3 37 09·4	56 61	N. by E. N.E. ½ N.	1·741 1·752	} + 027	1.758	Slight motion.
13. 14.	-36 21	151 39	Def. S. Def. N. Def. N.	35 06·4 37 15·1 38 06 6	61 58 60	N.N.W. $\frac{1}{2}$ W.	1.697	$\left.\begin{array}{c} + .025 \\ + .026 \\ + .031 \end{array}\right.$	1.738	Steering very steady. Heavy cross sea, unsteady.
19.		n Island, ackson.	Def. S. Def. N.	35 42·8 38 05·9	60	Observed on shore.	1) , ,,,		A slight motion. Steering steady.
	-33 51	151 17	Def. S.	35 15.7	60) on shore.	1.708			

* Observed on shore;
$$\begin{cases} \text{wt. 1 gr. } & \text{1}^{\circ} \text{1 } 42.0 \\ \text{wt. } 1\frac{1}{2} \text{ gr. } & 17 52.6 \\ \text{wt. } 2 \text{ grs. } 24 15.6 \\ \text{wt. } 2\frac{1}{2} \text{ grs. } 31 00.7 \\ \text{wt. } 3 \text{ grs. } 38 42.3 \\ \text{wt. } 3\frac{1}{2} \text{ grs. } 46 06.3 \end{cases}$$
 Intensity 1.820

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
July 19.		Island, ackson.	Mag. N.S. Mag. N. Mag. S.	41 45·3 31 47·2 22 06·6	60 60	Observed on shore.	1.696		1	
			wt. 1 gr.* wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	13 08·8 20 02·0 27 00·7 34 25·2	60 60 60		1.691 1.685 1.708 1.692	}	1.699	Including the results with the "face west."
Aug. 5.		g out of	wt. 3 grs. wt. $3 \frac{1}{2} \text{ grs.}$ Def. N.	42 06·9 51 13·5 37 45·1	60 60 63	E. by N. ½ N.				
	har	oour.	Def. S. Def. N. Def. S.	35 36·2 37 36·2 35 34·5	63 63 63	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	1.726	+•014	1.719	A head swell.
6.	-34 01 $-33 54$	153 17 153 54	Def. N. Def. S. Def. N.	38 06·3 36 11·3 37 32·3	63 63 63	E. by N. E. by N. E. by N.	1.698 1.654 1.731	+.011	1.703	×.
7.	-33 56	156 38	Def. S. Def. N. Def. S.	35 38·8 38 16·4 36 19·2	63 61 61	E. by N. E. by N.	1.685 1.688 1.647	} + •011	1.679	Steering wildly, much motion.
	-33 31 -33 42	160 20 163 34	Def. N. Def. S. Def. N.	38 36·0 36 13·2 38 58·3	63 63 61	E. by N. E. by N.	1.669 1.652 1.648	+.011	1.671	A good deal of mo- tion, steering tolerably.
	*	164 05	Def. S. Def. N. Def. S.	36 16·0 38 46·2 36 18·3	61 61 61	E. E.	1.650 1.659 1.648	+.007	1.658	Much motion, steer- ing badly. Motion violent,
10.	-33 47 $-33 42$	166 39 166 36	Def. N. Def. S. Def. N.	38 57·3 37 01·9 39 30·7	62 62 62	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	1.648 1.604 1.616	+.014	1.627	steering wild. A long swell, motion quick, steering
			Def. S. Mag. N. Mag. S.	36 57·2 32 50·1 23 37·2	62 62 62	E. E.	1.609 1.609	+.007		well.
11.	-33 34	167 37	Def. N. Def. S. Mag. N.	40 07·5 37 58·5 33 03·0	66 66 66	N.E. by E. N.E. by E.	1·579 1·549 1·592	\right	1.600	-
_			Mag. S. Mag. N.S. Def. N.	23 12·0 43 13·0 39 46·4	66 66 66	N.E. by E. N.E. by E. E.	1.590 1.600	+.007		Light wind, heavy swell, with quick motion.
12.	—32 58	169 20	Def. N. Def. S. Mag. N.	40 10·5 37 19·5 32 56·3	56 56 56 56	E.N.E. E.N.E. E.N.E.	1.576 1.586 1.601	+.018	1.607	Wind fresh, motion
13.	-32 12	170 27	Mag. S. Mag. N.S. Def. N. Def. S.	24 07·8 43 17·9 39 31·5 37 17·6	56 55 55	N.E. S.E. by E. S.E. by E.	1.585 1.615 1.588	+•026	J .	quick, steering badly. A head sea, steering ing steadily.
14.	-32 11	171 20	Def. N. Def. S. Mag. N.	38 55·5 36 58·7 33 30·8	55 55 55	s.E. by E. s.E. by E. s.E. by E.	1.650 1.607 1.554	-012	1.589	Strong wind, heavy sea, motion quick, ship steering well.
b			Mag. N.S. Mag. S.	43 09·9 23 34·3	55 55	s.e. by e.	1.595			

	ſ	wt.	1 gr.	12	44.1		1.674
		wt.	$1\frac{1}{2}$ gr.	19	03.3		1.712
served on sh	ore;	wt.	2 grs.	26	01.2		1.705
ace west.	1	wt.	$2\frac{1}{2}$ grs.	33	17.7		1.709
		wt.	3 grs.	41	35.2		1.715
	L	wt.	$3\frac{1}{2}$ grs.	51	02.1		1.687
	served on sh face west.	served on shore;	eserved on shore; wt. wt. face west. wt. wt. wt. wt. wt. wt.		$ \begin{cases} \text{wt. 1 gr.} & 12 \\ \text{wt. } 1\frac{1}{2} \text{ gr.} & 19 \\ \text{wt. 2 grs.} & 26 \\ \text{wt. 2}\frac{1}{2} \text{ grs.} & 33 \\ \text{wt. 3 grs.} & 41 \\ \text{wt. } 3\frac{1}{2} \text{ grs.} & 51 \end{cases} $	$\begin{array}{c} \text{wt. 1 gr.} & 12 & 44\cdot 1 \\ \text{wt. } 1\frac{1}{2} \text{ gr.} & 19 & 03\cdot 3 \\ \text{wt. 2 grs.} & 26 & 01\cdot 2 \\ \text{wt. } 2\frac{1}{2} \text{ grs.} & 33 & 17\cdot 7 \\ \text{wt. 3 grs.} & 41 & 35\cdot 2 \\ \text{wt. } 3\frac{1}{2} \text{ grs.} & 51 & 02\cdot 1 \\ \end{array}$	wt. $1\frac{1}{2}$ gr. 19 03·3 wt. 2 grs. 26 01·2

Intensity.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Aug. 15.	$-\mathring{3}3 \ 5\acute{5}$	171 5 9	Def. N. Def. N.	39 35·3 39 46·2	60 60	E. by s. E. ½ N.	1.611 1.600	·000 +·010		
	-33 58	172 06	Def. N.	39 09.4	60	E.S.E.	1.637		>1.601	A head sea, table
			Def. S. Mag. N. Mag. N.S.	37 06·3 33 20·9 43 00·2	60 60 60	E.S.E. E.S.E.	1.600 1.566 1.609	}006		very unsteady.
1.6	04.15	150 50	Mag. S.	23 21.3	60	E.S.E.				
16.	-34 15	172 50	Def. N. Def. S.	39 43 1 37 44·5	61	N.W. by N.	1.603 1.562	1.000		
			Mag. N. Mag. N.S.	33 10.3	61	N.W. by N.	1.583 1.573	+.029	>1.597	A head sea, wind
			Mag. S.	43 25·9 23 38·1	61 61	N.W. by N.		ال	1 097	strong, steering well.
17	-34 24	172 42	Mag. N.S. Def. N.	43 40.5	61 62	E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s.		-∙004		Heavy swell, steer- ing well.
17.	54 24	173 43	Def. S.	38 52·7 36 57·2	62	E. by s. $\frac{1}{2}$ s.	1.609			Otnore mind and
			Mag. N. Mag. N.S.	32 46.0	62 62	E. by s. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s.	1.620	├- 004	1.619	Strong wind, good deal of motion,
			Mag. S.	42 50·3 23 06·2	62	E. by s. $\frac{1}{2}$ s.		J		A heavy sea, steering
18.		?	Def. N. Def. N.	38 54.8	64	s.w.	1.631 1.606	∙018		wild,
21.		Islands, Zealand.	Def. N.	39 40·9 36 59·8	59 59		1.606			
			Mag. N.	32 50.2	59		1.610			
	-35 16	174 00	Mag. N.S. Mag. S.	43 01·9 23 37·6	59 59		1.606			*
*			wt. 1 gr.*	14 03.2	59		1.584			-
			wt. $1\frac{1}{2}$ gr. wt. 2 grs.	21 17·9 28 22·1	59 59	-	1.601 1.633			
			wt. $2\frac{1}{2}$ grs.	36 50.7	59		1.596			
			wt. 3 grs. wt. $3\frac{1}{2}$ grs.	44 58·3 55 09·9	59 59	Observed	1.622 1.618			
Oct. 29.			Def. N.	39 32.8	64	on shore.	1.613	\}	1.608	At the Magnetic Ob- servatory. (The results with "face west" are include
3			Def. S. Mag. N.	36 57·6 32 51·5	64		1.608 1.608			west" are include
		*	Mag. N.S.	42 54.9	64		1.616			the rise modifie)
			Mag. S.	23 37.6	64 64		1.606			
			wt. 1 gr.† wt. $1\frac{1}{2}$ gr.	13 51·7 20 53·0	64		1.620			
			wt. 2 grs.	28 22.4	64 64		1.633 1.587			
	,		wt. $2\frac{1}{2}$ grs. wt. 3 grs.	37 05·6 45 02·2	64		1.621		,	-
NT OR	D ·		wt. $3\frac{1}{2}$ grs.	55 19.1	64	J	1.616	J		
Nov. 23.	Running Bay of I		Def. N.	39 41.1		E. by s.	1.605	}+.004	1.610	Ship steady, about one mile off shore
0.4	off Arch	Point.	Def. S.	36 59.1		E. by s.	1.607	1		
24.	-36 20	177 27	Def. N. Def. S.	39 11·0 36 24·1		E.S.E.	1.635 1.642	1,.001	1.616	Ship not very steady
			Mag. N.	33 07.5		E.S.E.	1.586	+:001	1.616	a sea from S.W.
			Mag. N.S. Mag. S.	43 07·0 23 09·3		E.S.E.	1.599	J		

	wt. 1 gr.	_{ရှိ}	64.9	Intensity.		wt. 1 gr.	° 1°2	ó6.9	Intensity.
	wt. 1 gr.	19	24.9	1.592		w. 1 gi.	10	200	1 000
	wt. 1½ gr.	20	30.5	1.595		wt. 1½ gr.	20	16.4	1.616
* Observed on shore;	wt. 2 grs.	27	46.9	1.605	† Observed on shore;	wt. 2 grs.	27	38.8	1.613
face west.	wt. 2½ grs.	35	43.0	1.607	face west.	wt. $2\frac{1}{2}$ grs.	35	45.1	1.606
	wt. 3 grs.	44	38.7	1.619		wt. 3 grs.	44	47.7	1.616
	wt. 3½ grs.	55	23.7	1.594		wt. $3\frac{1}{2}$ grs.	5 5	26.4	1.594

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Nov. 25.	_3°8 0′0	1 [°] 79 3 [′] 4	Def. N. Def. S. Mag. N.	39 01·2 36 28·2 32 25·3	o		1.645 1.638 1.645	018	7	A head sea, table not very steady.
	-38 27	179 59	Mag. N.S. Mag. S. Def. N. Def. S.	42 31·1 23 06·8 38 52·4 36 29·4		s.e. by s. s.e. by s. s.e. by e. ½ e. s.e. by e. ½ e.		<u>ل</u> ا	1.634	A form A - C XX
	,	0	Mag. N. Mag. N.S. Mag. S.	32 22·4 42 30·0 22 37·9		s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$. s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$. s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$.	1.643 1.648	-002	J	A sea from the S.W., ship unsteady.
26.	-38 48	182 05	Def. N. Def. S. Def. N. Def. S.	39 12·6 36 36·7 39 06·7		E.S.E. E.S.E. S.E.	1.633 1.629 1.639 1.633	} +.001		Ship very steady, steering well.
			Mag. N. Mag. N.S. Mag. S.	36 32·6 32 23·2 42 20·3 22 23·4		S.E. S.E. S.E.	1.648 1.662	-013	1.640	
÷	-39 02	182 05	Def. N. Def. S. Mag. N.	38 54·4 36 15·2 32 30·5		E.S.E. E.S.E. E.S.E.	1.653 1.650 1.638	+.001		Head sea, much mo- tion.
27.	-39 14	182 54	Mag. N.S. Mag. S. Def. N. Def. S.	42 19·3 22 25·8 38 52·7 36 27·2	63 63	E.S.E. E.S.E. S.E. by E. S.E. by E.	1.663 1.639	006		A swell from the
	20. 21	109 00	Mag. N. Mag. N.S. Mag. S. Def. N.	32 35·6 42 34·9 22 45·9	63 63 63	s.e. by e. s.e. by e.	1.631 1.641 1.666	J = 1000		S.E., ship steady.
-	-39 31	183 00	Def. N. Def. S. Mag. N. Mag. N.S.	38 39·5 35 59·9 32 11·1 42 13·5	63 63 63	s. by E. s. by E. s. by E. s. by E.	1.665 1.663 1.666	-024		Steering well, ship steady.
28.	—40 35	183 00	Mag. S. Def. N. Def. S. Mag. N.	22 43·5 38 32·3 35 52·8 32 12·2	63 64 64 64	s. by E. E.S.E. E.S.E.	1.673 1.672 1.662	.000	1.652	
	-40 50	183 11	Mag. N.S. Mag. S. Def. N.	41 59·7 22 29·6 38 27·2	64 64 64	E.S.E. E.S.E. E.S.E. S.S.E. \frac{1}{2} E.	1.686	J 1	-	Very steady.
			Def. S. Mag. N. Mag. N.S.	35 35·2 32 02·5 41 46·1	64 64 64	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	1.689 1.675 1.706	019]	
. 29.	-41 34	183 40	Mag. S. Def. N. Def. S. Mag. N.	22 29·8 38 16·1 35 28·7 31 55·0	64 65 65 65	s.s.e. $\frac{1}{2}$ e. s. by e. s. by e. s. by e.	1.689 1.695 1.686			- (0
	*		Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	41 32·6 22 14·3 13 24·0 20 07·1	65 65 65 65	s. by E. s. by E. s. by E.	1.720 1.660 1.678	\\ \> - · 023	1.666	Very steady.
,			wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs.	26 39·6 35 07·5 42 38·1	65 65 65	s. by E. s. by E. s. by E. s. by E.	1.729 1.663 1.692			
	-42 40	183 46	wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N.	52 14·9 38 04·4 35 21·7 31 38·8	65 65 65 65	s. by E. s. s.	1.680 1.700 1.702 1.708		1.682	Very steady.
·			Mag. N.S. Mag. S.	41 34·5 22 01·6	65 65	s. s. s.	1.717			

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Nov. 30.	$-4\overset{\circ}{3}\ \overset{'}{33}$	183 10	Def. N. Def. S. Mag. N.	37 47·0 35 15·2 31 33·3	59 59 59	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W.	1·717 1·709 1·716	024		Very steady.
	—44 15	183 02	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	41 28·2 21 58·1 37 29·0 34 31·6 31 18·9	59 59 59 59 59	s. $\frac{1}{2}$ w. s. $\frac{1}{2}$ w. s. by w. s. by w. s. by w.	1·727 1·734 1·752 1·737	023	1.707	A cross swell, motion slight.
Dec. 1.	-45 30	183 12	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	41 10·5 21 59·4 37 08·5 34 49·3 31 29·9 41 29·2	59 59 63 63 63 63	s. by w. s. by w. s. e. by e. s. e. by e. s. e. by e. s. e. by e.	1.747 1.753 1.735 1.721 1.725	007		Ship pitching con- siderably, steering very steadily.
	45 48	183 25	Mag. S. Def. N. Def. S.	21 42·2 37 11·4 34 52·1	63 63 63	S.E. by E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1·750 1·732	010	1.733	A head sea, table
2.	-47 13	184 30	Mag. N. Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	31 06·0 40 59·4 21 43·6 37 11·8 34 31·8 31 15·8 41 12·7	63 63 56 56 56 56	S.E. \frac{1}{2} E. S.E. \frac{1}{2} E. S.E. \text{by E. \frac{1}{2} E.} 1·752 1·741	002		unsteady, ship steering well. Head sea, ship pitch- ing, steering steadily.	
	-47 39	184 55	Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	21 07·2 36 53·8 34 24·0 30 55·2	56 56 56	s.e. by e. ½ e. s.e. by e.	1·767 1·760 1·768 1·772	007	1.753	
3.	-48 18	185 54	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	40 53·0 21 09·8 36 55·9 34 06·7 30 44·1 40 52·8 21 15·0	56 56 51 51 51 51 51	s.e. by E.	1·765 1·776 1·782 1·772			
			wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs.	12 01·0 18 51·1 25 50·7 32 51·6 40 23·1	51 51 51 51 51	s.e. by e. s.e. by e. s.e. by e. s.e. by e. s.e. by e.	1.844 1.784 1.777 1.760 1.766 1.765	007	1.772	Very steady.
-	-49 05	186 54	wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	48 41·0 36 51·6 34 06·3 30 46·1 40 45·8 21 11·2 12 23·7	51 51 51 51 51 51	S.E. by E. s.E. by E. \frac{1}{2} E.	1.769 1.777 1.780 1.781	-:005	1.772	Very steady.
4.	-49 24	187 23	wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N.	18 37·4 25 50·1 32 30·9 40 32·8 48 59·5 36 41·8	51 51 51 51 51 51 51	s.E. by E. $\frac{1}{2}$ E.	1.804 1.778 1.777 1.760	-		-,,
			Def. N. Def. S. Mag. N. Mag. N.S.	36 44.7 34 22.0 30 48.7 40 56.3	54 54 54 54	E. by s. E. by s. E. by s. E. by s.	1·776 1·762 1·776 1·768	\right	1.772	Swell from the north- ward, steady.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 4.	$-\mathring{4}9$ $\acute{2}4$	187 2 3	Mag. S. wt. 1 gr. wt. 1 ¹ / ₂ gr.	21 25·6 12 24·3 18 55·0	54 54 54	E. by s. E. by s. E. by s.	1·789 1·778	> .000	1.772	Swell from the northward. Steady.
,			wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3½ grs.	25 46·4 32 36·7 40 48·6 48 56·7	54 54 54 54	E. by s.E. by s.E. by s.	1·782 1·774 1·753 1·759			
5.	-49 23	188 54	Def. N. Def. S. Mag. N. Mag. N.S.	36 18·3 34 29·5 30 46·1 40 54·9	55 55 55 55	E. by s.E. by s.E. by s.	1.754 1.780 1.770			
-			Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs.	21 34·1 12 35·7 18 20·9 25 35·5	55 55 55 55	E. by s. E. by s. E. by s. E. by s.	1·762 1·831 1·794			
	-49 38	189 44	wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N.	32 51·2 40 31·3 48 46·6 36 34·4	55 55 55 55	E. by s.E. by s.E. by s.	1.762 1.762 1.764	.000	1.775	Very steady.
	1 <i>j</i> 00	109 11	Def. S. Mag. N. Mag. N.S.	34 28·8 30 54·8 41 01·8	55 55 55	E. by s. E. by s. E. by s.	1·787 1·755 1·766 1·759	j		
6.	-49 50	190 46	Mag. S. Def. N. Def. S. Mag. N.	21 46·8 36 37·1 34 02·5 30 49·4	55 51 51 51	E. by s. E. by s. E. by s. E. by s.	1.784 1.781 1.775			
			Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr.	41 04·2 21 41·3 12 38·8 18 49·6	51 51 51 51	E. by s.E. by s.E. by s.	1.756 1.753 1.785	> .000	1.766	Very steady.
			wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs.	25 40·4 33 28·2 40 37·3 49 09·5	51 51 51 51	E. by s.E. by s.E. by s.	1.788 1.725 1.758 1.753			
۸	-50 08	191 39	Def. N. Def. S. Mag. N.	36 40·0 34 16·4 30 51·3 41 02·2	51 51 51 51	E. by s.E. by s.E. by s.	1.781 1.768 1.774			
77	50 20	101 50	Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	21 42·4 12 35·7 18 50·0	51 51 51	E. by s.E. by s.E. by s.	1.759 1.761 1.785	> .000	1.771	Ship steady.
7.	-50 32	191 52	Def. N. Def. S. Mag. N. Mag. N.S.	35 51·7 33 46·7 30 48·4 40 47·4	51 51 51 51	s.e. by e. s.e. by e. s.e. by e. s.e. by e.	1.828 1.796 1.778 1.780	}007	<u> </u>	
	-50 45	192 19	Mag. S. Def. N. Def. S. Mag. N.	21 27·7 36 01·8 34 06·7 30 40·7	51 51 51 51	S.E. by E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1·818 1·776 1·785		>1.777	Ship steady.
			Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	40 45·7 21 32·3 12 43·0 18 56·2	51 51 51 51	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1·782 1·743 1·776	008		Surp soundy!
			wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs.	25 58·6 32 37·7 40 35·6 48 00·8	51 51 51 51	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1.769 1.772 1.759 1.784		J _.	

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 8	sı̈́ 37	19 4 00	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	35 49·9 33 50·1 30 42·2 40 31·4 21 29·1 12 35·5 18 34·6	49 49 49 49 49 49	E. by s.	1.830 1.793 1.784 1.796 1.760 1.806	} ·000	1·794	Ship steady.
	-52 00	195 00	wt. $1_{\frac{1}{2}}$ grs. wt. 2 grs. wt. $2_{\frac{1}{2}}$ grs. wt. 3 grs. wt. $3_{\frac{1}{2}}$ grs. Def. N. Def. S.	25 16·9 32 08·9 40 00·3 48 01·8 36 01·2 33 59·6 30 36·5	49 49 49 49 49 49	E. by s.	1.813 1.794 1.780 1.782 1.819 1.783 1.792			Strong breeze, table steady,
9	-52 14	197 49	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	40 38·6 20 59·5 35 53·6 33 44·6 30 21·9	49 49 45 45 45 45	E. by s.	1.786 1.826 1.798 1.812	-000	1.799	steering wildly.
	53 01 52 51		Mag. N.S. Mag. S. Mag. N.S. Def. N. Def. S. Mag. N. Mag. N.S.	40 47·0 20 38·5 40 36·2 36 14·8 33 54·6 30 26·7 40 30·9	45 45 46 46 46 46	E. by s. E. by s. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.781 1.791 1.805 1.788 1.806 1.798		~	Ship unsteady, steering wild.
			Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs.	21 26·5 11 50·3 17 43·9 24 29·7 31 19·3 39 46·3	46 46 46 46 46 46	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.871 1.891 1.867 1.837 1.788	 		Violent motion, steering well, head sea, table pretty steady.
12	. — 52 53	205 07	wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	47 43·1 36 41·3 33 40·8 30 30·2 40 20·2 21 23·0	46 45 45 45 45 45	E. ½ N. E.S.E. E.S.E. E.S.E. E.S.E.	1.791 1.780 1.802 1.801 1.813		1.820	Head swell, little
			$\begin{array}{c} \text{wt. 1 gr.} \\ \text{wt. } 1\frac{1}{2} \text{ gr.} \\ \text{wt. } 2\frac{1}{2} \text{ grs.} \\ \text{wt. } 2\frac{1}{2} \text{ grs.} \\ \text{wt. 3 grs.} \\ \text{wt. 3} \frac{1}{2} \text{ grs.} \\ \end{array}$	12 30·8 18 07·9 24 38·0 31 44·7 39 30·1 48 07·9	45 45 45 45 45 45 45	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E.	1.771 1.851 1.857 1.815 1.798 1.779	\\ \rangle003	J	motion, steering well.
. 49	-53 31	206 14	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	36 09·5 33 22·8 30 11·3 39 57·5 21 07·1 12 08·9	45 45 45 45 45 45	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E.	1.811 1.820 1.828 1.841 1.823	\003	1.834	A slight motion,
		i e	wt. $1 \frac{1}{2}$ gr. wt. $2 \frac{1}{2}$ grs. wt. $2 \frac{1}{2}$ grs. wt. $3 \frac{1}{2}$ grs. wt. $3 \frac{1}{2}$ grs.	18 00·7 24 39·1 31 15·2 38 03·7 47 41·3	45 45 45 45 45 45	E.S.E. E.S.E. E.S.E. E.S.E.	1.863 1.856 1.840 1.855 1.834		*	steering very well.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 13.	$-5\overset{\circ}{4}1\overset{'}{9}$	208 24	Def. N. Def. S.	36 02·0 33 17·8	51 51	E.S.E. E.S.E.	1.818 1.825			
	-54 53	209 24	Mag. N. Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	30 23·2 40 28·8 20 27·6 36 03·0 33 14·6 30 10·5 39 59·5	51 51 51 51 51 51 51	E.S.E. E.S.E. E.S.E. E.S.E. E.S.E. E.S.E.	1.811 1.801 1.817 1.828 1.829 1.837	003	1.814	Table steady, steering badly.
	-54 48 -55 04	209 25 209 58	Mag. S. Def. N. Def. N. Def. S. Mag. N.	20 52·6 36 18·6 36 11·8 32 54·1 30 18·1	51 51 48 48 48	E.S.E. E.S.E. by s. s.E. by s. s.E. by s.	1·802 1·808 1·849 1·818	015		Heavy sea, steering badly. Ship much more steady, steering
14.	56 14	211 43	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	40 03·9 20 54·4 35 54·6 32 37·1 29 56·6	48 48 52 52 52 52	s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s.	1.831 1.825 1.867 1.849	<u>]</u>		better.
			Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	39 36·9 20 21·6 35 55·5 32 43·8 29 59·3 39 31·8 20 24·4	52 52 52 52 52 52 52	s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s.	1.867 1.824 1.860 1.845 1.874	015	1.836	Table steady, steering well.
	-56 30	211 50	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	35 36·6 32 43·4 29 59·9 40 01·6 20 33·4 11 46·1 18 10·6	52 52 52 52 52 52 52	s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s. s.e. by s.	1.841 1.861 1.844 1.834 1.884 1.884	\right	1.841	Very steady.
1.5	*C *0	212 26	wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs.	24 02·0 31 08·6 38 07·8 46 00·9	52 52 52 52	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	1.902 1.848 1.855 1.846			
15.	-56 53	212 06	Def. N. Def. S. Mag. N. Mag. N.S.	35 33·1 32 47·5 29 57·1 40 06·1	41 41 41 41 41	s.e. by s. s.e. by s. s.e. by s.	1.845 1.855 1.848 1.828	•015	1.843	Very steady.
	-57 16	212 17	Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	20 33·2 35 28·4 32 21·9 29 25·4 39 39·1	41 41 41 41	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	1.850 1.882 1.895 1.865	>-·015	1 010	very swary.
16.	-57 44	212 59	Mag. S. Def. N. Def. S. Mag. N.	20 14·7 35 13·8 32 22·3 29 51·2 39 30·9	41 42 42 42 42 42	s.e. by s. s.s.e. s.s.e. s.s.e.	1.863 1.882 1.857 1.876			-
			Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	20 15·2 11 45·4 18 00·2 23 38·6 30 04·6	42 42 42 42 42 42	S.S.E. S.S.E. S.S.E.	1.882 1.860 1.929 1.904	}-·019	1.863	Very steady.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 16.	_ s8 28	2 [°] 13 0 [′] 8	Def. N. Def. S.	34 42·2 32 09·3	42 42	S.S.E. S.S.E.	1.895 1.896			
			Mag. N.	29 32.0	42	s.s.e.	1.885			
			Mag. N.S.	39 29.4	42	S.S.E.	1.878			* (
			Mag. S. wt. 1 gr.	20 16·5 11 33·4	42	S.S.E.	1.915			
			wt. $1\frac{1}{2}$ gr.	17 36.2	42	S.S.E. S.S.E.	1.904		ī	
			wt. 2 grs.	23 48.0	42	S.S.E.	1.917	>017	1.878	Very steady.
			wt. $2\frac{1}{2}$ grs.	29 50.1	42	S.S.E.	1.918			
			wt. 3 grs.	36 40.9	42	s.s.e.	1.914			
		212 11	wt. $3\frac{1}{2}$ grs.	44 52.1	42	s.s.e.	1.877			20
	-5844	213 11	Def. N. Def. S.	35 11.8	42	S.S.E.	1.865 1.882			
			Mag. N.	32 22·7 29 28·0	42	S.S.E.	1.891			
			Mag. N.S.	39 16.0	42	S.S.E.	1.896			
			Mag. S.	19 46.3	42	S.S.E.	0-			
17.	-6048	213 51	Def. N.	34 58.7	36	S.S.E.	1.878	1	*	
			Def. S.	31 59.8	36	S.S.E.	1.905	 j		
			Mag. N.	29 19.8	36	S.S.E.	1.903			
			Mag. N.S. Mag. S.	39 06·6 19 45·9	36 36	S.S.E.	1.907			
			wt. 1 gr.	11 51.7	36	S.S.E.	1.863	> - ⋅016	7	
			wt. $1\frac{1}{2}$ gr.	16 49.6	36	S.S.E.	1.987			
			wt. 2 grs.	23 56.7	36	S.S.E.	1.907			
			wt. $2\frac{1}{2}$ grs.	29 43.5	36	S.S.E.	1.923		1.892	Very slight motion,
			wt. 3 grs.	36 48.8	36	S.S.E.	1.906			steering well.
	-61 37	213 54	wt. $3\frac{1}{2}$ grs. Def. N.	44 22·1 34 28·6	36 34	S.S.E.	1.893 1.908	\forall		
	-01 37	210 04	Def. N.	31 43.6	34	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	1.922			
			Mag. N.	29 09.5	34	S. ½ E.	1.918	├- •016		
			Mag. N.S.	39 10.2	34	$S \cdot \frac{1}{2} E .$	1.903		,	
			Mag. S.	19 54.3	34	S. 1/2 E.				
18.	-62 34	212 34	Def. N.	34 27.6	32	s. by E.	1.909			
			Def. S.	31 38.4	32	s. by E.	1.928			
			Mag. N. Mag. N.S.	29 06·9 38 39·3	$\begin{array}{ c c }\hline 32\\ 32\\ \end{array}$	s. by E.	1.922 1.945			
			Mag. S.	19 21.5	32	s. by E.	1 340			
			wt. 1 gr.	11 30.6	32	s. by E.	1.920	>016	1.916	Very steady, sailing
			wt. $1\frac{1}{2}$ gr.	16 59.2	32	s. by E.	1.968	Í		amongst loose ice.
			wt. 2 grs.	23 55.7	32	s. by E.	1.905		* (
			wt. $2\frac{1}{2}$ grs.	29 07.6	32	s. by E.	1.958			
			wt. 3 grs. wt. $3\frac{1}{2}$ grs.	36 00·5 43 45·9	$\begin{array}{ c c }\hline 32\\ 32\\ \end{array}$	s. by E. s. by E.	1.942 1.920			
19.	-63 06	210 55	Def. N.	34 27.4	40	S.S.W.	1.910	K		
			Def. S.	31 50.7	40	s.s.w.	1.914			
			Mag. N.	29 08.0	40	s.s.w.	1.920			
			Mag. N.S.	38 52.6	40	s.s.w.	1.927			Want atonder municipal
20.	63 36	208 20	Mag. S. Def. N.	19 37.4	40	s.s.w.	1.017	} −·015	1.910	Very steady, running amongst loose ice.
20.	-03 30	200 20	Def. N.	34 20·3 31 19·9	$\begin{vmatrix} 34 \\ 34 \end{vmatrix}$	S.S.W.	1.917 1.946			
			Mag. N.	28 59.8	34	S.S.W.	1.932			
			Mag. N.S.	38 48.0	34	S.S.W.	1.933			
		1	Mag. S.	19 37.0	34	s.s.w.				
	-63 53	208 32	Def. N.	34 21.3	34	s.	1.916	1		
		•	Def. S.	31 23.0	34	s.	1.943	>014	\Box	
			Mag. N. Mag. N.S.	28 47·5 38 39·1	34	s. s.	1.950 1.945			
	-		Mag. S.	19 21.6	34	s.	1 310	ار	>1.927	Very steady, running
										amongst loose ice.

-					0					
1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 21.	_64 11	206 35	Def. N. Def. S. Mag. N.	34 01·3 31 15·8 28 54·2	34 34 34	s.s.w. s.s.w.	1.936 1.950 1.941	013	1.927	Verysteady, running amongst loose ice.
	_64 51	206 19	Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr.	38 44·7 19 15·2 11 10·3	34 34 35 35	s.s.w. s.s.w. s. 3/4 w.	1.937 1.978 1.948]]		
-			wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs.	17 10·4 23 07·5 29 07·7 35 52·4	35 35 35	s. 34 w. s. 34 w. s. 34 w. s. 43 w. s. 43 w.	1.968 1.959 1.949	-013	1.943	Very steady, steering amongst loose ice.
22.	-65 19	205 08	wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Def. N.	42 59·5 34 05·5 31 01·8 34 07·6	35 35 35 37	S. $\frac{3}{4}$ W. S. $\frac{3}{4}$ W. S. $\frac{3}{4}$ W. S. $\frac{1}{2}$ W.	1.947 1.932 1.965 1.930			
	÷		Def. S. Mag. N. Mag. N.S. Mag. S.	31 17·5 28 50·9 38 42·3 19 29·9	37 37 37 37	S. ½ W. S. ½ W. S. ½ W. S. ½ W.	1.948 1.945 1.940	 >-·013	1.931	Very steady, steering
	-65 34	205 00	Def. N. Def. S. Mag. N. Mag. N.S.	33 59·5 31 00·9 28 53·2 38 37·7	37 37 37 37	s. s. s.	1.937 1.966 1.942 1.946			smongat 100sc 10c.
23.	-65 47	204 19	Mag. S. Def. N. Def. S. Mag. N.	19 25·2 34 02·2 31 23·8 28 42·6	37 36 36 36	S. N.E. N.E.	1.935 1.942 1.958		ר	Very steady, sailing amongst loose ice.
24.	-65 54	204 08	Mag. N.S. Mag. S. Def. N. Def. S.	38 44·3 19 44·9 34 15·9 31 21·8	36 36 42 42	N.E. N.E. N. by w. N. by w.	1.938 1.921 1.944	h	1.950	Fast to a piece of ice.
27.	-66 08	203 50	Mag. N. Mag. N.S. Mag. S. Def. N.	28 51·3 38 45·8 19 29·0 34 07·9	42 42 42 30	n. by w. n. by w. n. by w. E.S.E.	1.945 1.936 1.929]
~,	00 00		Def. S. Mag. N. Mag. N.S.	30 57.8 28 46.1 38 45.3 19 24.3	30 30 30 30 30	n.w. by n.	1.969 1.953 1.937	1 .010	1.949	Working in a hole of water.
28. 1842.	-66 10	202 54	Mag. S. Def. N.	33 56.0	30	w. by n.	1.941	+.003		
Jan. 1.	-66 36	203 29	Def. N. Def. S. Mag. N. Mag. N.S.	34 06·6 31 17·7 28 46·6 38 35·1	44 44 44 44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.931 1.948 1.951 1.950			- ,
			Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs.	19 28·8 11 20·8 16 59·2 22 44·6	44 44 44	N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W.	1.950 1.950 1.967 2.001	+.009	1.961	Fast to a piece of ice, Erebus fifty yards N.E. (This re-
	CC 00	200 25	wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs.	29 21·5 35 50·3 43 33·7	44 44 44 44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.947 1.952 1.922			sult is not employ- ed in the map.)
7	-66 20	203 39	Def. N. Def. S. Mag. N. Mag. N.S.	34 13·5 31 20·0 29 00·1 38 40·2	33 33 33 33	N.W. N.W. N.W.	1.924 1.946 1.932 1.943	+.009		Working in a hole of
			Mag. S.	19 29.8	33	N.W.			> 1.944	water.

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1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 8.	-66 ó 5	204 02	Def. N. Def. S. Mag. N. Mag. N.S.	34 13·8 31 22·2 29 05·0 38 47·0	35 35	s. by w. \(\frac{1}{2}\) w.	1·944 1·925	011	>1.944	Working in a hole of water.
			Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	19 29·8 11 14·4 17 07·6 23 02·1 29 01·7	35 35 35 35 35	s. by w. ½ w. N. N. N.				1
9.	-66 01	204 04	wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N. Def. S.	35 44·9 43 14·8 33 45·1 31 12·7	35 35 35 35	N. N. N. S.W. $\frac{1}{2}$ W.	1.953 1.930 1.952 1.954	.007		
10	65 57	203 56	Mag. N.S. Mag. S. Def. N. Def. S.	28 59·9 38 37·6 19 16·0 33 53·7 30 59·0	35 35 35 30 30	s.w. by w. s.w. by w. w. by s. w. by s.	1.932 1.946 1.943 1.968	} ·000	<u> </u>	,
		-	Mag. N. Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	28 46·5 38 36·3 19 16·3 11 28·5 16 59·9	30 30 30 30 30	w. by s. E. w. by s. ½ s. w. by s. ½ s	1.965	+.001		Working in a hole of
			wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N.	22 55·0 29 09·5 35 46·6 42 54·2 33 54·5	30 30 30 30 30	w. by s. $\frac{1}{2}$ s s.w. by w.	1·955 1·950 1·942 1·942	003	>1.949	water.
11	65 56	203 31	Def. S. Mag. N. Mag. N.S. Mag. S. Def. N.	31 22·4 28 46·7 38 30·3 19 19·4 33 51·4	30 30 30 30 30	s.w. by w.	1.944 1.952 1.957	000	J	
13			Def. S. Mag. N. Mag. N.S. Mag. S.	31 05·2 28 45·2 38 40·3 19 21·0	30 30 30 30	s. s. s.	1.962 1.953 1.943 1.922	012		
			Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	34 14·7 31 23·1 28 52·6 38 49·4 19 36·1	33 33 33 33 33	N. ½ E.	1.943 1.942 1.931	+.012	1.945	Working in a hole of water.
14	-	201 46	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	34 10·3 31 15·2 28 49·5 38 38·4 19 27·1	33 35 35 35 35	N.E. by E.	1.927 1.951 1.947 1.946	+.008		
16	6.5 47	202 08	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	33 47·6 31 16·1 28 52·7 38 45·7 19 44·8	50 50 50 50 50		1.949 1.951 1.942 1.936			
			wt. 1 gr. wt. 1½ gr. wt. 2 grs. wt. 2½ grs. wt. 3 grs.	11 25·4 17 08·3 23 02·9 29 16·2 36 17·4	50 50 50 50 50	Observed on ice.	1.940 1.957 1.979 1.955 1.935		1.948	
			wt. $3\frac{1}{2}$ grs.		50		1.932			

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 26.		203 12	Def. N.	33 14·0	$ {35}$	e. by n.	1.984	· ·		
Jan. 20.	-07 12	200 12	Def. S.	31 00.0	35	E. by N.	1.967			Fact to a miner of in-
			Mag. N.	28 30.9	35	E. by N.	1.977	>+.003	1	Fast to a piece of ice Erebus N. by W.
			Mag. N.S.	38 28.5	35	E. by N.	1.960	J	1.972*	20 fathoms*.
			Mag. N.S.	38 22.2	35	s.E. by s.	1.966	009	J	Fast to a piece of ice: Erebus N.E. by E
			Mag. S.	19 15.7	35	s.e. by s.	1 040			
28.	-67 46	204 17	Def. N.	33 47.7	35 35	E. by N.	1.949 1.966	+·003 +·012		
			Def. S. Def. N.	$\begin{vmatrix} 31 & 00.7 \\ 33 & 47.5 \end{vmatrix}$	35	n. by E.	1.949	+.011		*
			Def. N.	33 43.8	35	N. Dy E.	1.954	7		
			Mag. N.	28 45.1	35	N.N.E.	1.955	>+·010	>1.960	A swell from
			Mag. N.S.	38 29.8	35	N.N.E.	1.957] .	1 300	W.S.W., table steady.
			Mag. S.	19 21.1	35	N.N.E.			=	steady.
			Def. N.	33 45.2	35	$s. \frac{3}{4} W.$	1.952			
			Def. S.	30 52.2	35	$s_{\bullet} \frac{3}{4} W_{\bullet}$	1.975	-012	IJ	
			Mag. N.	28 39.0	35	S. $\frac{3}{4}$ W.	1.965			
			Mag. N.S.	38 22.4	$\begin{vmatrix} 35 \\ 35 \end{vmatrix}$	S. $\frac{3}{4}$ W.	1.968	7		
00	-67 46	204 17	Mag. S. wt. 1 gr.	19 16·9 10 53·5	35	s. ³ / ₄ w.	2.028	1	_	4.00
28.	-07 40	204 17	wt. $1\frac{1}{2}$ gr.	16 57.2	35	N.	1.972	+.012		
	-	-	wt. 2 grs.	23 09.2	35	N. by W. 3 W.		Г		
	-		wt. $2\frac{1}{2}$ grs.	29 14.4	35	$N.$ by $W.\frac{3}{4}$ $W.$		>+.011		
			wt. 3 grs.	35 37.6	35	N. by w. $\frac{3}{4}$ w.	1.959	7+1011	>1.965	Table steady.
			wt. $3\frac{1}{2}$ grs.		35	N. by W. $\frac{3}{4}$ W.		Ŋ		
29.	-67 24	204 05	Def. N.	33 42.1	31	s. by w.	1.956			
			Def. S.	30 58.3	31	s. by w.	1.969	>012	j	
			Mag. N. Mag. N.S.	28 49·8 38 41·5	31 31	s. by w.	1.947 1.941			
21	-67 19	202 24	Def. N.	33 51.2	32	s. by w.	1.946	K		
91.	-0, 1,	202 24	Def. S.	30 50.5	32	s.s.w.	1.976	1 1	5	
			Mag. N.	28 38.1	32	s.s.w.	1.966	├- 011		
			Mag. N.S.	38 30.3	32	s.s.w.	1.957	IJ	>1.946	Strong breeze, tabl
			Mag. S.	19 21.8	32	s.s.w.			1310	steady.
			Def. N.	33 52.1	32	s.w.	1.945			
h	C= 1	201 04	Def. N.	33 52·3 34 30·6	32	s.w. by s.	1.945 1.906		5	10
reb. 1.	-67 1	2 201 34	Def. N. Def. N.	34 04.4	32	w. by s.	1.933			-
	-67 1	3	Def. N.	33 56.0	32	s.s.w.	1.941	7 ' "	-	
	0, 1		Def. S.	31 03.0	32	s.s.w.	1.964	-011		
			Mag. N.	28 46.3	32	s.s.w.	1.951		>1.935	Table very steady.
			Mag. N.S.	38 31.8	32	s.s.w.	1.954	IJ		
			Mag. S.	19 21.1	32	s.s.w.		1.077		
			Def. N.	34 07.1	32	N. 3/4 W.	1.930			
0	67 5	100 40	Def. N. Def. N.	33 51·1 33 33·9	32	s.w.	1.946 1.964		1	
2	-07 3	6 199 48	Def. S.	31 00.5	31	s. by w.	1.966	1 2		
			Mag. N.	28 51.5	31	s. by w.	1.944			
			Mag. N.S.	38 23.3	31	s. by w.	1.967			
			Mag. S.	19 15.5	31	s. by w.			1.955	Cross sea ship un
3	-68 2	1 200 06	Def. N.	33 45.4	31	s.s.w.	1.952			steady.
			Def. S.	30 51.4	31	s.s.w.	1.976			
±-			Mag. N.	28 22.2	31	S.S.W.	1.990 1.970	11	Γ	*
			Mag. N.S. Mag. S.	38 21·2 19 13·8	$\begin{vmatrix} 31\\31 \end{vmatrix}$	s.s.w. s.s.w.	1.970	7		
		1	mag. b.	13 100		13.23. VV ·				

^{*} This result has not been employed in the map.

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 4.	$-$ 68 $\overset{\prime}{4}$ 5	199 4 1	Def. N. Def. S. Mag. N. Mag. N.S.	33 38·7 30 43·2 28 32·2 38 15·0	30 30 30 30	s. s. s.	1·959 1·984 1·975 1·977	\\ 011	<u> </u>	
			Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs.	19 15·9 11 08·5 16 55·4 22 31·5	30 30 30 30	S. S. S. $\frac{1}{2}$ E. S.	1.984 1.974 2.015	_·011	w Y	÷
		*	wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N.	29 00·9 35 06·1 42 35·6 33 38·8	30 30 30 30	s. s. s. by E. s. by E.	1.963 1.983 1.952 1.959	\right\{ \011 \right\} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	>1·961	Table steady.
5.	-68 49 $-68 52$		Def. S. Def. N. Def. N. Def. S.	31 04·3 33 59·1 33 46·1 30 46·1	30 30 32 32	s. by E. s. by E. n.n.w. s.w. s.w.	1.963 1.938 1.952 1.981	+.010		
			Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	28 35·2 38 24·0 19 18·6 11 08·8	32 32 32 32		1.970 1.965	\rightarrow \cdot	1.966	Fresh breeze, table
			wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs.	16 59·2 22 30·9 28 49·9 35 33·8	32 32 32 32	$s.w. \frac{1}{2} w.$	1.966 2.016 1.974 1.961	005		scau,
6.	-69 55	192 17	wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N.	42 40·2 33 46·5 30 44·6 28 21·7	32 34 34 34	s.w. $\frac{1}{2}$ w. s. by w. s. by w. s. by w.	1.949 1.952 1.982 1.990	}-·010	٠ ٦	A swell from the N.N.W., unsteady.
7.	-70 05	191 03	Mag. N.S. Mag. S. Def. N. Def. N.	38 08·0 18 54·1 33 44·5 33 53·9	34 34 34 30	s. by w. s. by w. s. s. s.s.w.	1.987 1.953 1.943	•010	1.965	Steering well.
		1=	Def. S. Mag. N. Mag. N.S. Mag. S.	30 47 4 28 38·8 37 43·3 17 52·3	30 30 30 30	s.s.w. s.s.w.	1·980 1·965 2·021	009	J	Swell from W.N.W., steering badly, very unsteady.
8.	-70 08	186 39	Def. N. Def. N. Def. S. Mag. N.	33 48·7 33 49·3 30 38·2 28 30·9	31 31 31 31	s.w.		004	7	Steering wildly, unsteady.
	-70 17	186 04	Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	37 43·8 17 38·4 11 15·2 16 52·1	31 31 31 31	s.w. by w. s.w. by w. s. s.	2·020 1·961 1·979	J ገ	1.976	
			wt. 2 grs. wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3½ grs.	22 37·0 28 35·7 34 59·8 41 52·3	31 31 31 31	s. s.	2·007 1·989 1·988 1·980	009		Table steady.
1	* -		Def. N. Def. S. Mag. N. Mag. N.S.	33 38·4 30 34·2 28 26·8 37 33·2	31 31 31 31	s. s. s.	1.960 1.960 1.995 1.983 2.034		e e	
			Mag. S.	17 17.7	31	s. s.	~ 004	J		

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera-	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 9.	-70 32	185 3 8	Def. N. Def. S. Mag. N.S.	33 37·4 30 50·6 37 30·0	30 30 30	s. s.	1.961 1.976 2.039	009		
10.	—69 56	184 43	Def. N. Def. S. Mag. N.S. Def. N. Def. S. Mag. N.	33 43·4 30 29·7 37 29·7 33 37·7 30 47·2 28 34·0	30 30 30 32 32 32 32	s.e. by s. s. \frac{1}{2} E. s. \frac{1}{2} E. w. by s. w. by s. w. by s.	1.955 1.997 2.039 1.960 1.980 1.972	006 009	1.983	Head swell, very unsteady. Head swell, not
11.	—69 5 1	183 02	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 56·0 17 58·6 33 37·5 30 30·3 28 18·6	32 32 32 32 32 32	w. by s. w. by s. w.s.w. w.s.w.	2·004 1·960 1·997 1·994	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		Strong breeze, swell from the west, table not steady.
12.	71 0 3	180 56	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 44·4 18 08·6 33 38·3 30 37·8 28 18·2	32 32 33 33 33	w.s.w. w.s.w. s.e. by s. s.e. by s. s.e. by s.	1.960 1.989 1.995	006	1.988	Cross sea, table very unsteady.
13.	—72 07	181 50	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 51·2 18 05·3 33 22·3 30 42·3 28 04·6	33 33 31 31 31	s.E. by s. s.E. by s. s.E. by s. s.E. by s.	2.011 1.976 1.985 2.017	006		Swellfrom N.W., steering wildly, table unsteady.
14.	—72 55	181 33	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 27.2 17 43.3 33 14.6 30 22.9 28 12.1	31 30 30 30	s.e. by s. s.e. by e. s.e. by e. s.e. by e.	1.983 2.004 2.006	004	2.001	N.W. swell, ship unsteady.
16.	74 51	174 02	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 31·9 17 56·7 33 12·5 30 26·1 27 52·3	30 30 28 28 28	1	2.036 1.986 2.001 2.036	006		Table steady.
	-75 09	173 16	Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	37 19·9 17 45·9 11 09·7 16 40·5 21 41·0 28 13·7	28 28 28 28 28 28	S.S.E. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	2.052 1.976 2.001 2.090 2.013	} ·000	200 8	N.W. swell, mo-
		-	wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N.S.	34 53·1 42 16·6 33 04·9 30 23·8 37 27·9	28 28 28 28 28	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. by S. E. by S.	1.995 1.964 1.990 2.003 2.042	.000		tion slight.
17.	-76 06	174 57	Def. N. Def. S. Mag. N. Mag. N.S.	33 25·4 30 37·3 28 16·2 37 28·6 17 38·4	32 32 32 32 32	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.	1.973 1.990 1.999	+.002	•2006	Steering wildly, table unsteady.
18.	-77 02	181 37	Mag. S. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	33 12·4 30 36·1 28 17·4 37 31·7 17 49·0	27 27 27 27 27 27	E.N.E. E.N.E.	1.987 1.991 1.998 2.036	-+ •004	2.007	Cross sea, table un- steady.

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 19.	-76 4 8	184 46	Def. N. Def. S. Mag. N. Mag. N.S.	33 16·1 30 30·3 28 14·8 37 34·7	25 25 25 25 25	n. by e. n. by e. n. by e. n. by e.	1.983 1.997 2.002 2.031	+.006	2.009	Head sea, ship un- steady.
20.	—76 20	191 26	Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	17 30·6 33 10·8 30 30·9 27 55·8	25 28 28 28 28 28	N. by E. N.E. N.E. N.E.	1.988 1.996 2.030 2.062	+.005	2.024	Head sea, ship un-
22.	—7 6 24	184 54	Mag. S. Def. N. Def. S. Mag. N.	37 12·8 17 14·3 33 09·1 30 25·3 28 11·1	28 30 30 30	N.E. N.E. s.E. by s. s.E. by s. s.E. by s.	1.990 2.002 2.007	005	2.004	Strong wind, head sea, unsteady.
	_77 13	193 52	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 30·2 17 41·0 33 12·9 30 39·5 28 21·0	30 30 30 30 30 30	s.e. by s. s.e. by s. e. by s. e. by s.	1.986 1.987 1.991) }		
71			Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs.	37 31·9 17 13·0 10 55·0 16 28·5 22 23·3	30 30 30 30 30	E. by s.	2·036 2·021 2·026 2·028	-000	2.011	Light swell, motion gentle.
23.	-77 47	197 25	wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N.	28 07.5 34 16.6 41 32.7 33 28.8 30 36.2	30 30 30 29 29	E. by s. E. by s. E. by s. N.E. by E.	2.020 2.025 1.992 1.969 1.991	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	J	
24.	-77 14	199 29	Mag. N. Mag. N.S. Mag. S. Def. N. Def. S.	28 08·2 37 45·3 17 17·8 33 10·3 30 41·2	29 29 29 29 30 30	E.N.E. E.N.E. s.w. by s.	2.011 2.018 1.989 1.980	+.004	2.001	Table steady.
CONTRACTOR			Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	28 22·9 37 30·5 17 25·3 11 02·2	30 30 30 30	s.w. by s. s.w. by s. s.w. by s. s.w. by s. s.w. by s.	1.989 2.038 2.000	005	1.992	Fresh breeze, swell from N.E., table
AND THE PROPERTY OF THE PROPER			wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs.	16 31·1 22 33·5 28 40·4 34 58·0 42 08·1	30 30 30 30 30	s.w. by s.	2.020 2.010 1.983 1.989 1.970			steady.
25	75 20	194 36	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	33 05·2 30 34·4 28 14·8 37 43·8 17 38·2	29 29 29 29 29	w. w. w. w.	1.994 1.993 2.000 2.020		2.003	Fresh breeze, swell from N.E., table steady.
26	-73 10	189 21	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	33 17·7 30 34·9 28 06·6 38 01·7	29 29 29 29	n.w. by w. n.w. by w. n.w. by w. n.w. by w.	1.992 2.012	+.005	2.000	Strong breeze, mo- tion great.
27	. —72 03	187 40	Def. N. Def. S. Mag. N. Mag. N.S.	17 13·8 33 22·8 30 36·3 28 11·4 37 39·4		s.w. s.w. s.w. w. by n. ½ n		\right	1.000	Easterly swell, slight
			Mag. S.	17 28.8	26	w. by N. $\frac{1}{2}$ N	1		>1.999	motion.

								,		
1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 27.	−7 2 0′3	187 40	wt. 1 gr. wt. 1½ gr. wt. 2 grs.	11 01·0 16 26·3 22 13·8	26 26 26	S.W. $\frac{1}{2}$ W. S.W. $\frac{1}{2}$ W.	2·002 2·029 2·040	005	1. 999	Easterly swell, slight motion.
	—7 1 43	187 15	wt. $2\frac{1}{2}$ grs. wt. 3 grs. wt. $3\frac{1}{2}$ grs. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	28 25·7 34 35·3 42 33·7 11 04·8 16 01·3 22 29·5 28 37·6	26 26 26 26 26 26 26 26	s.w. ½ w.	2·081 2·016	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		
28.	—7 1 20	184 30	wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N.	34 56·6 42 04·9 33 44·8 30 47·1 28 22·8	26 26 25 25 25 25	w. by N. ½ N. w. by N. ½ N. w. by S. w. by S. w. by S.	1.990 1.971 1.952 1.980 1.988	·000	1.999	Easterly swell, slight motion.
Mar. 1.	69 54	179 55	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	37 39·1 17 44·3 33 24·5 30 38·5 28 17·3	25 25 32 32 32	w. by s. w. by s. w.n.w. w.n.w.	1.974 1.989 1.998	+.005	1.999	Easterly swell,
2.	68 09	183 10	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	37 47·1 17 43·2 33 34·6 31 01·2 28 30·9 38 05·3	32 32 32 32 32 32 32	W.N.W. W.N.W. N.N.E. N.N.E. N.N.E.	2.015 1.963 1.966 1.977 1.990	+.007	1.981	Swell from east- ward.
3.	-67 3 5	185 18	Mag. S. Def. N. Def. S. Mag. N.	18 05·9 33 30·0 31 15·6 28 29·3	32 31 31 31	N.N.E. N.E. by E. N.E. by E. N.E. by E.	1·968 1·951 1·979	}+·006	<u> </u>	
			Mag. N.S. Mag. S. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs.	37 54·8 18 00·1 11 07·4 17 00·0 22 48·2 28 54·6	31 31 31 31 31 31	N.E. by E. N.E. by E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	2.005 1.986 1.965 1.993 1.970	+.006	1.978	Cross sea, ship unsteady.
4.	-67 40	187 40	wt. 3 grs. wt. $3\frac{1}{2}$ grs. Def. N. Def. S. Mag. N.	35 30·5 42 54·1 33 43·9 31 04·0 28 23·5	31 31 33 33 33	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N. by w. N. by w. N. by w.	1.965 1.942 1.954 1.963 1.988	}+.011		
5.	67 09	188 02	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	37 47.2 17 59.9 33 43.6 31 47.7 28 36.4 37 57.1	33 33 35 35 35 35	n. by w. n. by w. n. n.	2.015 1.954 1.917 1.968 2.003	+.012	1.981	Strong gale, heavy sea, ship unsteady.
6.	-65 28	191 24	Mag. N.S. Mag. S. Def. N. Def. S. Mag. N. Mag. N.S.	17 50·3 33 56·8 31 20·9 28 44·3 38 07·4	35 33 33 33 33	N. by E.	1.940 1.945 1.956 1.988	}+.012		Heavy sea from W.S.W., ship very unsteady.
	-64 49	192 21	Mag. S. wt. 1 gr. wt. 1½ gr. wt. 2 grs.	18 29·3 11 29·7 17 20·6 23 10·9	33 33 33 33	N. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E.	1.928	+.012	1.955	Swell from the S.S.W., table steady.

1842.	Lat.		Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 6.	_6 4	4 9	192 ź1	wt. 2½ grs.	29 34·9	33	n. by E. ½ E.		>+·012	>1.955	Swell from the S.S.W., table
		,		wt. 3 grs.	36 02.8	33	N. by E. $\frac{1}{2}$ E.				steady.
7	-63	20	194 15	wt. $3\frac{1}{2}$ grs. Def. N.	43 37·5 34 42·3	33	N. by E. $\frac{1}{2}$ E.		K	ט	P
7.	-03	30	194 15	Def. S.	31 50.8	33	n. by E.	1.895 1.914			
				Mag. N.	29 04.3	33	N. by E.	1.926	>+.012	1.942	Table steady.
				Mag. N.S.	38 11.2	33	N. by E.	1.983	J	· ·	
		l		Mag. S.	18 24.5	33	n. by E.				
8.	-62	17	195 55	Def. N.	34 47.8	35	n. by E.	1.889			
				Def. S.	32 05.4	35	N. by E.	1.900		-	*
				Mag. N.	29 00·5 38 35·2	35	N. by E.	1.931 1.950			
0.5				Mag. N.S. Mag. S.	18 46.6	35	n. by E.	1.950			
				wt. 1 gr.	11 47.0	35	N. by E.	1.875	>+.014		Table steady.
				wt. 1½ gr.	18 01.9	35	N. by E.	1.857			
	-			wt. 2 grs.	23 47.3	35	N. by E.	1.916			
				wt. $2\frac{1}{2}$ grs.	30 03.9	35	N. by E.	1.902		1010	
	1			wt. 3 grs.	37 04.3	35	N. by E.	1.894		>1.916	
				wt. $3\frac{1}{2}$ grs.	45 00.2	35	N. by E.	1.870	Ϊ		
. 9	-61	06	198 08		34 50.2	35	$N \cdot E \cdot \frac{1}{2} N \cdot$	1.887			
				Def. S.	32 03·8 29 15·0	35	$N_{\bullet}E_{\bullet} \stackrel{1}{\stackrel{1}{2}} N_{\bullet}$	1.901	>+.013	IJ	Sea getting up, un
				Mag. N.	38 35.4	35	N.E. $\frac{1}{2}$ N.	1.950		. *	steady.
				Mag. N.S. Mag. S.	18 55.7	35	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N.	1 300)		
10	-60	19	203 42		34 45.6	34	E.N.E.	1.891)		
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Def. S.	32 05.7	34	E.N.E.	1.899	+.010	1.000	Ship unsteady.
				Mag. N.	29 15.1	34	E.N.E.	1.910		1.920	Simp unsteady.
				Mag. N.S.	38 40.9	34	E.N.E.	1.942	J		
	60			Mag. S.	19 00.8	34	E.N.E.	1.070	5		
11	-60	15	208 06		35 04.8	35	E. by N.	1.872			Strong gale,
				Def. S.	31 58·7 29 04·3	35	E. by N.	1.906 1.926			heavy sea, shi
				Mag. N. Mag. N.S.	38 46.5	35	E. by N. E. by N.	1.935			very unsteady
				Mag. S.	18 53.1	35	E. by N.	- 0	>+.007	1.907	1
12	60	16	211 45	Def. N.	35 04.2	35	E. by N.	1.873			
				Def. S.	32 08.0	35	E. by N.	1.897			Heavy swell from S.W.,
				Mag. N.	29 25.5	35	E. by N.	1.894			unsteady.
				Mag. N.S.	39 14.9	35	E. by N.	1.897	IJ		J
19	=0	E 9	016 00	Mag. S.	18 53.3	35	E. by N.	1.877	1		
10	-59	99	216 28	Def. N. Def. S.	35 00·2 32 11·9	36	N.E. ½ E.	1.893			
				Mag. N.	29 23.2	36	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	1.898		1.910	Heavy swell, steer-
				Mag. N.S.	39 02.3	36	N.E. 1/2 E.	1.914			
				Mag. S.	18 59.1	36	N.E. 1 E.				
14	-59	22	218 14	Def. N.	35 07.5	37	N.E. $\frac{1}{2}$ E.	1.870			
				Def. S.	32 32.6	37	N.E. $\frac{1}{2}$ E.	1.871		1.900	Heavy swell, very
				Mag. N.	29 36·2 38 56·5	37	N.E. $\frac{1}{2}$ E.	1.000	' [unsteady, steer- ing badly.
				Mag. N.S.	19 00.9	37	N.E. $\frac{1}{2}$ E.	1.922	,	100	
15	58	40	221 2	Mag. S. Def. N.	35 14.8	37		1.862	רוֹיַ		-
		x o	221 20	Def. N.	31 38.8	37		1.927	,	1.010	Heavy swell, steer
· .				Mag. N.	29 10.9	37	231111231	1.917		1.913	ing badly.
				Mag. N.S.	39 11.3			1.90%			
	1		1	Mag. S.	19 05.6	37	E.N.E.				-

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 16.	_s9 ó1	227 43	Def. N.	34 39·9	3°9	Е.	1.897	 }		
			Def. S. Mag. N.	32 14.2 $29 30.9$	39 39	E. E.	1·891 1·887	>+·003	1.897	Heavy swell, steering badly.
			Mag. N.S. Mag. S.	39 10·7 18 51·8	39 39	E. E.	1.903	J		
18.	-60 05	235 56	Def. N.	35 07.2	38	E. by s.	1.870	۱ ۱		
			Def. S. Mag. N.	32 36·0 29 27·6	38 38	E. by s. E. by s.	1.868 1.892	000	1.884	Heavy sea from
			Mag. N.S.	39 08.7	38	E. by s.	1.904			S.W. by W., ship unsteady.
	CO 7 #	096 90	Mag. S. Def. N.	18 50.6	38	E. by s.	1.875			
	-60 17	236 38	Def. N.	$35 02.5 \\ 32 29.4$	38 38	E. E.	1.875		1.000	The ship means steed in
			Mag. N.	29 25.4	38	E.	1.896	>+·003	1.892	The ship more steady.
			Mag. N.S. Mag. S.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	38 38	E. E.	1.911	J		·
	-60 24	237 29	Def. N.	35 05.5	38	E. by N.	1.872	۱ ۱		
			Def. S. Mag. N.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	38 38	E. by N.	1.898 1.923	>+.007	1.907	Ship steady.
		···	Mag. N.S.	39 05.9	38	E. by N.	1.909	IJ		
21.	50.05	247 27	Mag. S. Def. N.	18 23·6 35 50·2	38 38	E. by N.	1.830	2	-)(-	
χ1.	-59 05	241 21	Def. S.	32 49.7	38	E. by N.	1.853	1.007	1.075	Cross sea, motion
			Mag. N.	29 27.6	38	E. by N.	1.892	+.007	1.875	gentle.
			Mag. N.S. Mag. S.	39 13·5 19 10·0	38 38	E. by N.	1.898	J		
22.	-58 26	251 42	Def. N.	35 29.5	38	E. by N.	1.848	n l		
			Def. S. Mag. N.	32 41·7 29 27·9	38 38	e. by n.	1.862 1.891	>+·007	1.885	Cross sea, ship un- steady.
			Mag. N.S.	39 05.7	38	E. by N.	1.909	J		
0.9	-58 33	054 45	Mag. S. wt. 1 gr.	19 23·5 12 12·4	38 33	E. by N. E. ½ N.	1.812		,	
23.	-38 33	204 40	wt. 1½ gr.	18 20.0	33	E. ½ N. E. ½ N.	1.828			
			wt. 2 grs.	25 22.7	33	$E.\frac{1}{2}N.$	1.803			
			wt. $2\frac{1}{2}$ grs. wt. 3 grs.	$31 29.0 \\ 39 04.8$	33 33	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.825 1.812		7.004	7 14 1
-			wt. $3\frac{1}{2}$ grs.	47 40.6	33	$E_{\bullet} \frac{1}{2} N_{\bullet}$	1.780	\>+.006	1.824	Little motion.
			Def. N. Def. S.	36 13·8 33 24·9	33 33	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.806 1.818	-		
			Mag. N.	29 55.5	33	E. $\frac{1}{2}$ N.	1.850			
			Mag. N.S. Mag. S.	39 49·9 19 52·7	33 33	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.851	J		
24.	-58 40	257 32	Def. N.	36 09.9	35	E. by N.	1.810	n		
		-	Def. S.	33 27.9	35	E. by N.	1.815 1.862			Little motion.
			Mag. N. Mag. N.S.	$\begin{vmatrix} 29 & 47.9 \\ 39 & 36.0 \end{vmatrix}$	35	E. by N.	1.869		7	
		250 55	Mag. S.	19 56.5	35	E. by N.	1.770	\ \rightarrow + \cdot 010	1.832	K
1	-58 53	258 55	wt. 1 gr. wt. $1\frac{1}{2}$ gr.	$\begin{vmatrix} 12 & 30 \cdot 1 \\ 18 & 17 \cdot 1 \end{vmatrix}$	35 35	E. by N.	$ 1.770 \\ 1.837$			Little motion;
CONTRACTOR			wt. 2 grs.	25 22.4	35	E. by N.	1.803			overcast and damp.
96	58 59	267 50	wt. $2\frac{1}{2}$ grs. Def. N.	$\begin{vmatrix} 31 & 46.5 \\ 36 & 48.2 \end{vmatrix}$	35 45	E. by N. E. by N. $\frac{1}{2}$ N.	1.810 1.773	K)
20.	-30 39	201 00	Def. S.	34 31.2	45	E. by N. $\frac{1}{2}$ N.	1.753	\ \ \ +·012	1.783	Motion gentle.
			Mag. N.	30 53.2	45	E. by N. $\frac{1}{2}$ N.	1.771	T 012	1,00	
			Mag. N.S. Mag. S.	40 39·9 20 37·6	45	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N.]		
			p. ~.		-	J 1. 2 1.				

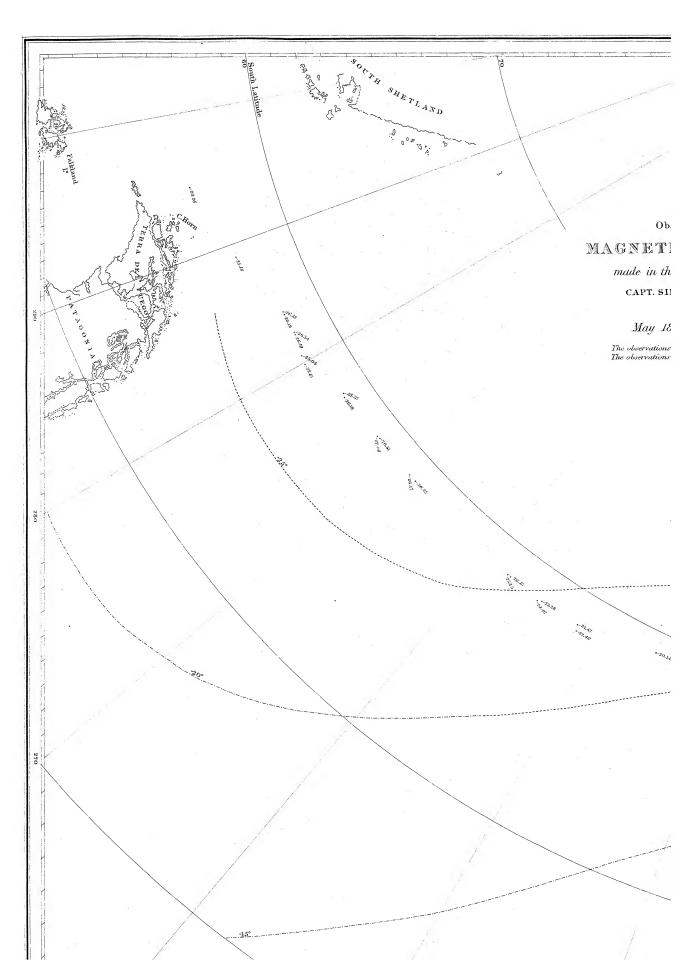
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1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 27.	-59 01	2 ⁵ 72 0 ⁶	Def. N. Def. S. Mag. N.	37 29·4 35 37·2 31 21·2	36 36 36	E.N.E. E.N.E.	1·734 1·687 1·734	+.013	1.747	Ship unsteady.
28.	-58 24	276 18	Mag. N.S. Mag. S. Def. N. Def. S.	40 47·4 20 48·3 38 14·0 35 38·0	36 36 39 39	E.N.E. E.N.E. N.E. by E. N.E. by E.	1.780 1.690 1.686	\right	1.722	Swell from S.W.,
29.	-58 25	279 44	Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	31 57·2 40 59·0 20 51·8 13 14·6	39 39 39 45	N.E. by E. N.E. by E. N.E. by E.	1.684 1.763)	1,7~	slight motion.
ż		*	wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. $2\frac{1}{2}$ grs. Def. N. Def. S.	20 00·5 28 08·5 36 37·1 38 49·8	45 45 45 45	n.e. by e. n.e. by e. n.e. by e.	1.684 1.642 1.601 1.656 1.658	+.017		Slight motion. Needle very unsteady (omitted in the mean).
30.	-58 31	281 33	Mag. N. Mag. N.S. Mag. S. Def. N.	36 09·1 32 21·1 41 45·0 21 53·0 38 25·5	45 45 45 45 40	n.e. by e. n.e. by e. n.e. by e.	1.651 1.705 1.680		1.672	Slight motion.
50.	-00 01	201 00	Def. N. Def. S. Mag. N. Mag. N.S. Mag. S.	36 04·1 32 15·8 41 37·5	40 40 40	E.N.E. E.N.E. E.N.E.	1.661 1.658 1.714	+.015		
31.	-58 36	285 33	Def. N. Def. S. Mag. N. Mag. N.S.	21 26·3 39 35·3 36 46·6 32 48·3 42 15·6	40 44 44 44 44	E.N.E. N.E. N.E. N.E.	1.611 1.619 1.613 1.664	+•021	1.648	Slight motion.
Apr. 1.	-57 21	289 36	Mag. S. Def. N. Def. S. Mag. N.	22 13·4 40 12·8 36 33·8 33 28·9	44 47 47 47	N.E. by N. N.E. by N. N.E. by N.	1.573 1.632 1.554	1.004		Strong breeze, ship unsteady,
2.	-57 26	291 32	Mag. N.S. Mag. S. Def. N. Def. S.	42 50·4 22 29·8 40 13·1 37 44·6	47 47 44 44	N.E. by N. N.E. by N. S.E. S.E.	1.622 1.573 1.561	J h	1.592	Heavy sea, ship unsteady.
3.	-56 37	294 34	Mag. N. Mag. N.S. Mag. S. Def. N.	33 23·9 42 47·3 23 07·7 41 28·4	44 44 44 44	S.E. S.E. S.E. N.E.	1.562 1.627 1.505	J	ر ا	
			Def. S. Mag. N. Mag. N.S. Mag. S.	38 40·8 33 47·9 44 02·5 24 06·6	44 44 44 44	N.E. N.E. N.E.	1·506 1·527 1·523		1.495	Heavy sea, ship un-
4.	54 48	297 21	Def. N. Def. S. Mag. N. Mag. N.S.	42 33·1 40 06·6 35 00·8 45 01·4	44 44 44 44	N.E. N.E. N.E.	1·443 1·428 1·420 1·440			steady.
5	_52 40	299 52	Mag. S. Def. N. Def. S. Mag. N.	25 06·5 44 47·8 42 29·0 36 03·2	44 44 44 44	N.E. N.N.E. N.N.E. N.N.E.	1·325 1·307 1·326			
	3		Mag. N.S. Mag. S. wt. 1 gr. wt. 1½ gr.	46 17·6 25 40·2 17 23·4 26 11·2	44 44 44 44	N.N.E. N.N.E. N.N.E. N.N.E.	1·326 1·284 1·304		1.355	Ship steady.

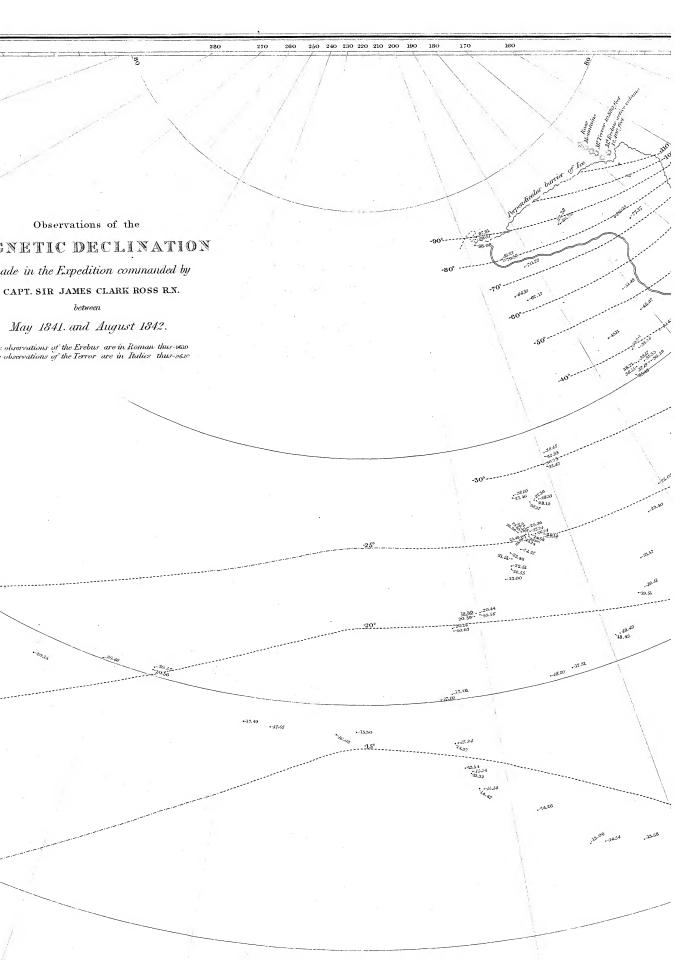
1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Apr. 5.	$-\overset{\circ}{52}\overset{\prime}{40}$	299 52	wt. 2 grs. wt. $2\frac{1}{2}$ grs.	34 54·7 45 13·0	°44 44	N.N.E. N.N.E.	1·351 1·344	>+.025	1•355	Ship steady.
	-52 28	301 42	wt. 3 grs. Def. N. Def. S.	54 16·9 44 40·6 42 04·5	44 44 44	N.N.E. N.N.E. N.N.E.	1·408 1·327 1·326			
6.	— 51 42	301 36	Mag. N. Mag. N.S. Mag. S. Def. N. Def. S. Mag. N.	36 12·5 46 43·3 25 58·0 44 52·9 42 26·1 36 14·5 46 16·5	44 44 44 44 44	N.N.E. N.N.E. N.N.E. N.N.W. $\frac{1}{2}$ W. N.N.W. $\frac{1}{2}$ W. N.N.W. $\frac{1}{2}$ W.	1·308 1·309	+.025	1:340	Ship steady. Slight motion.
9.	Falkland	l Islands.	Mag. N.S. Mag. S. Def. N. Def. S.	26 08·0 44 21·2 42 02·4	44 44 44 44	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1·346 1·328	} + •009	1.346	Single anchor in Port Louis, Berkeley Sound.
10.	-51 32	301 53	Def. N. Def. S. Mag. N. Mag. N.S.	44 58·5 41 52·8 35 57·0 46 13·9	43 43 43 43		1·314 1·335 1·336 1·335		-	
July 25.			Mag. S. wt. 1 gr. wt. 1½ gr. wt. 2 grs. wt. 2½ grs. wt. 3 grs. Def. N. Def. S. Mag. N. Mag. N.S. Mag. S. wt. 1 gr.	40 13'9 25 37.0* 16 56.5 25 36.6 34 47.2 45 34.1 57 39.1 44 27.0 42 00.4 36 00.0 46 13.2 25 42.8 16 51.2 25 34.3		Observed on shore.	1·316 1·331 1·356 1·356 1·353 1·340 1·330		Mean of all the results obtained with weights at Port Louis 1·336.	
Aug. 15.			wt. 1½ gr. wt. 2 grs. wt. 2½ grs. wt. 3 grs. Def. N. Def. N. Mag. N. Mag. N.S.	25 34·3 34 47·8 45 29·7 57 48·7† 44 29·0 41 58·0 36 00·9 46 14·8	43 43		1·333 1·355 1·338 1·350 1·339 1·332 1·333		Mean of all the re at Po	At the Magnetic Station.

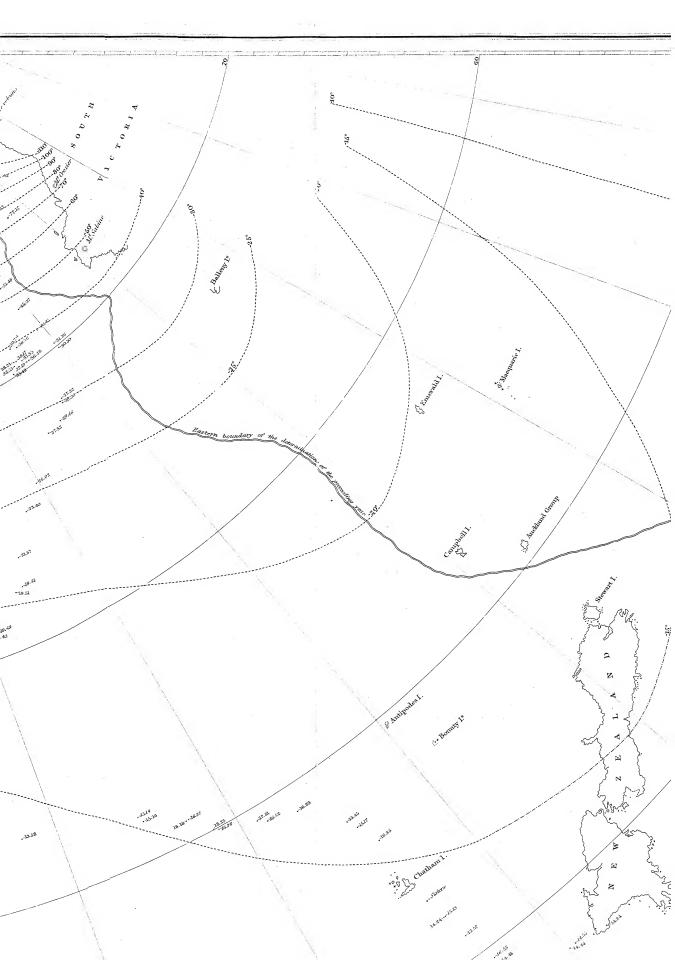
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Intensity.
                          wt. 1 gr. 16 14.1
                                                   1.316
                         wt. 1\frac{1}{2} gr. 24 36.9
                                                    1.338
* Observed on shore;
                         wt. 2 grs. 33 44.9
                                                    1.342
       face west.
                         wt. 2\frac{1}{2} grs. 44 31·3
                                                    1.334
                        wt. 3 grs. 58 17.8
                                                    1.333
                          wt. 1 gr. 16 26·1
                                                    1.301
                         wt. 1\frac{1}{2} gr. 24 27.9
                                                    1.345
† Observed on shore;
                         wt. 2 grs. 33 49.5
                                                   1.339
       face west.
                         wt. 2\frac{1}{2} grs. 44 17·1
                                                   1.339
                        Uwt. 3 grs. 58 19.5
                                                   1.333
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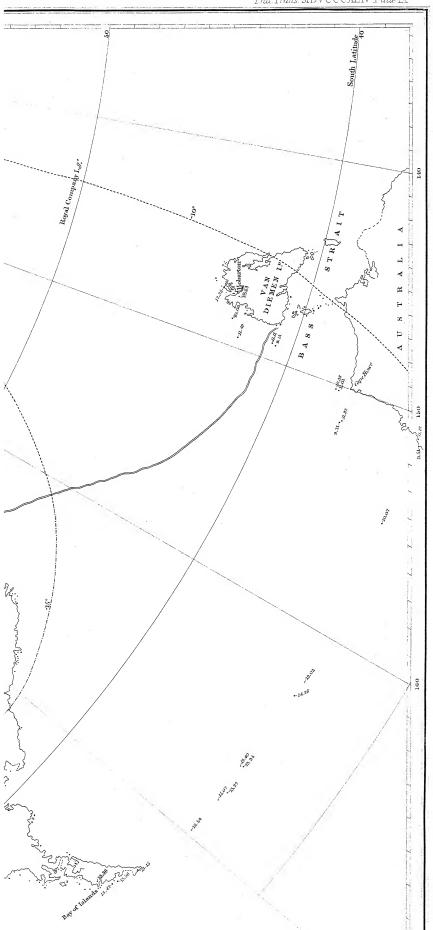
1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Aug. 15.	0 /	• ,	Mag. S. wt. 1 gr. wt. 1½ gr. wt. 2 grs.	25 52·1* 17 00·4 25 37·3 34 24·4	38 38 38 38		1·311 1·331 1·369	-	esults ob-	At the Magnetic Station.
18.	-		wt. $2\frac{1}{2}$ grs. wt. 3 grs. Def N. Def S. Mag. N. Mag. N.S. Mag. S.	45 20·1 57 43·6 44 27·0 41 59·6 35 59·3 46 12·2 25 43·8	38 38 38 38 38 38	Observed on shore.	1.341 1.352 1.340 1.330 1.332 1.338		& Mean of all the results obtained with weights at Port Louis 1-336.	
Aug. 15.	At anc Berkeley	for the ship's nong.	Def. N.	44 59·4 44 32·3 44 10·0 43 52·8 43 55·3 43 52·3 43 57·8 44 05·9 44 22·3	40 40 40 40 40 40 40 40	E. ½ S. E. E.S.E. S.E. S.S.E. S.S.W. S.W.	1·313 1·336 1·355 1·370 1·368 1·370 1·366 1·359 1·345	+:007 +:009 -:003 -:014 -:023 -:024 -:023 -:014 -:003	1·320 1·345 1·352 1·356 1·345 1·343 1·343 1·345 1·342 > 1·342	
		To obtain corrections attraction.	Def. N.	44 47·5 45 06·1 45 01·7 44 59·7 44 52·2 44 57·2 44 59·0 44 32·5	40 40 40 40 40 40 40 40	W. W.N.W. N.W. N.N.W. N. N.N.E. N.E.	1·324 1·308 1·312 1·313 1·320 1·315 1·314 1·336	+·009 +·017 +·023 +·025 +·026 +·025 +·023 +·017	1.333 1.325 1.335 1.335 1.346 1.340 1.337 1.353	

* Observed on shore; $\begin{cases} \text{wt. 1 gr. 1\^{6} 15.4} & \text{Intensity.} \\ \text{wt. } 1\frac{1}{2}\text{ gr. } 24 \ 30.1 & 1.315 \\ \text{wt. } 2\text{ grs. } 33 \ 57.8 & 1.335 \\ \text{wt. } 2\frac{1}{2}\text{ grs. } 44 \ 32.3 & 1.333 \\ \text{wt. } 3\text{ grs. } 57 \ 35.7 & 1.344 \end{cases}$





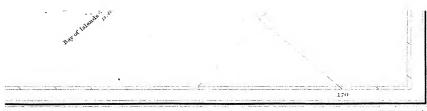




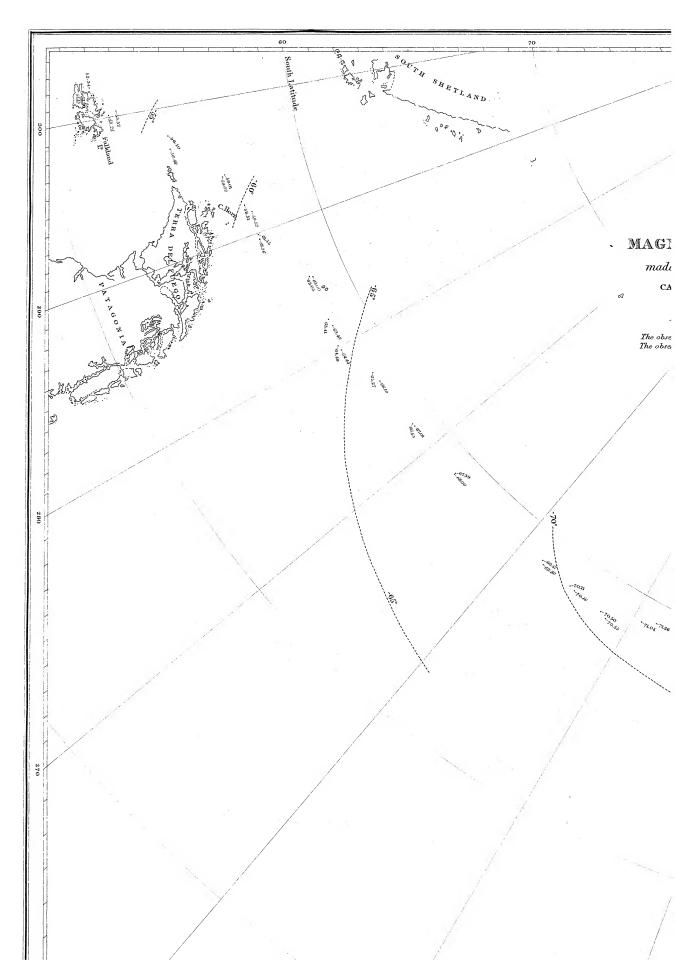


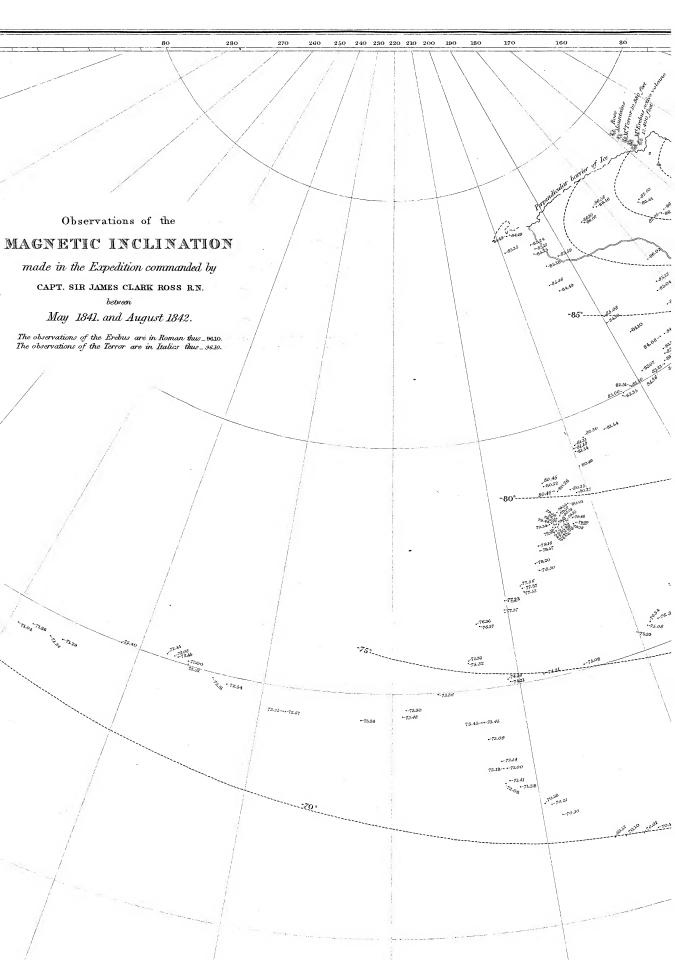
Longitude East of Gr

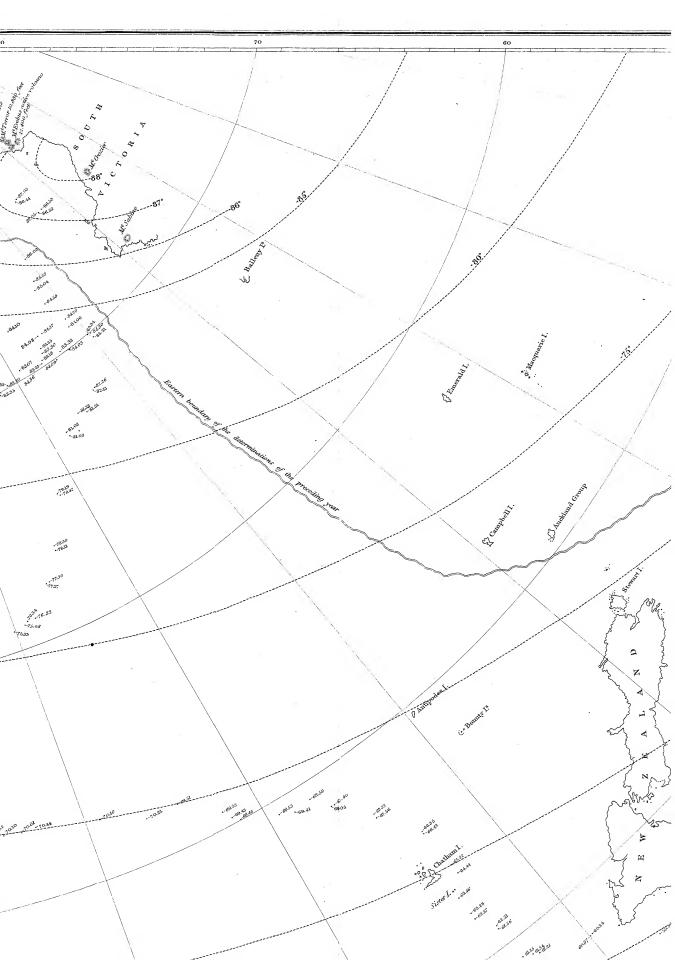
East of Greenwich 200 190

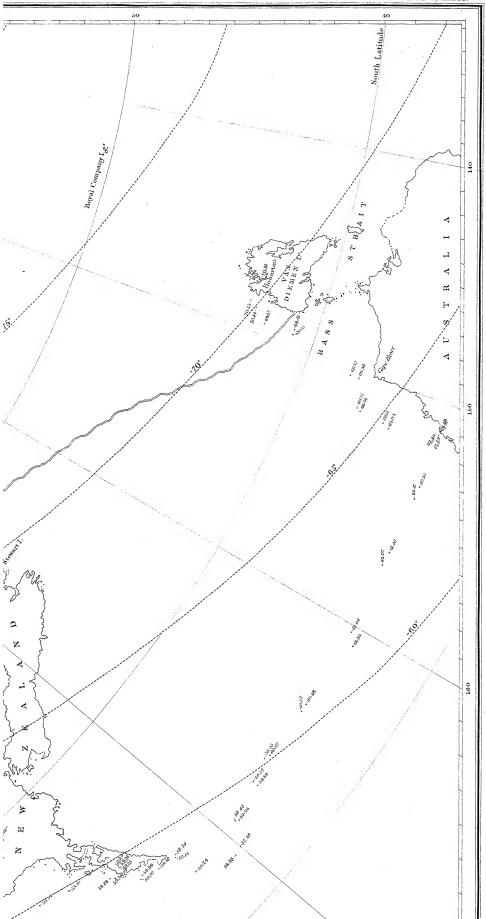


J.&C.Walker Sculp!

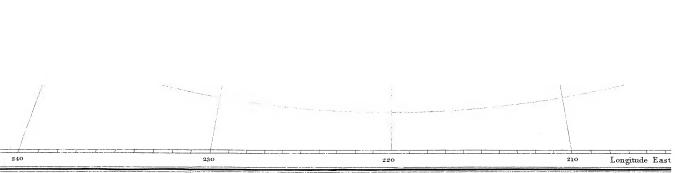


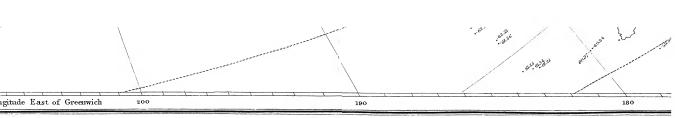


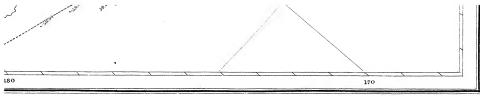




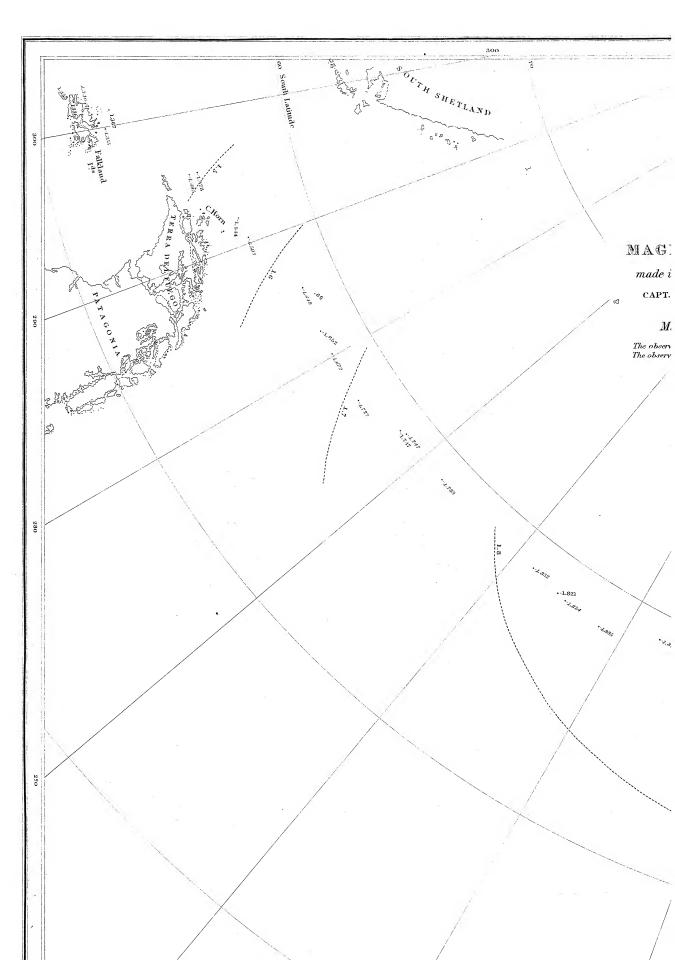


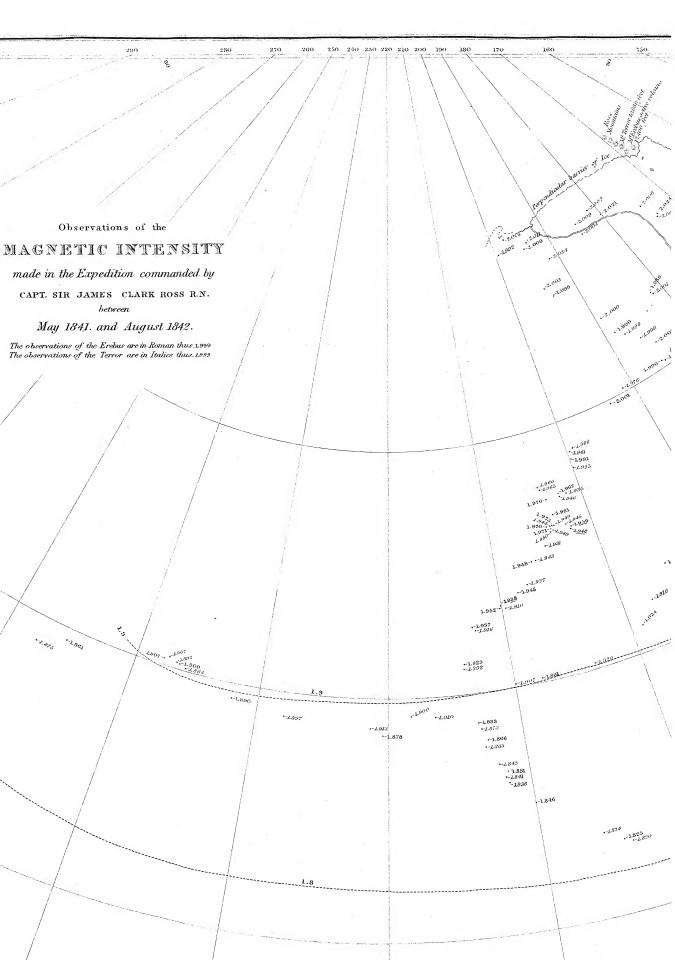


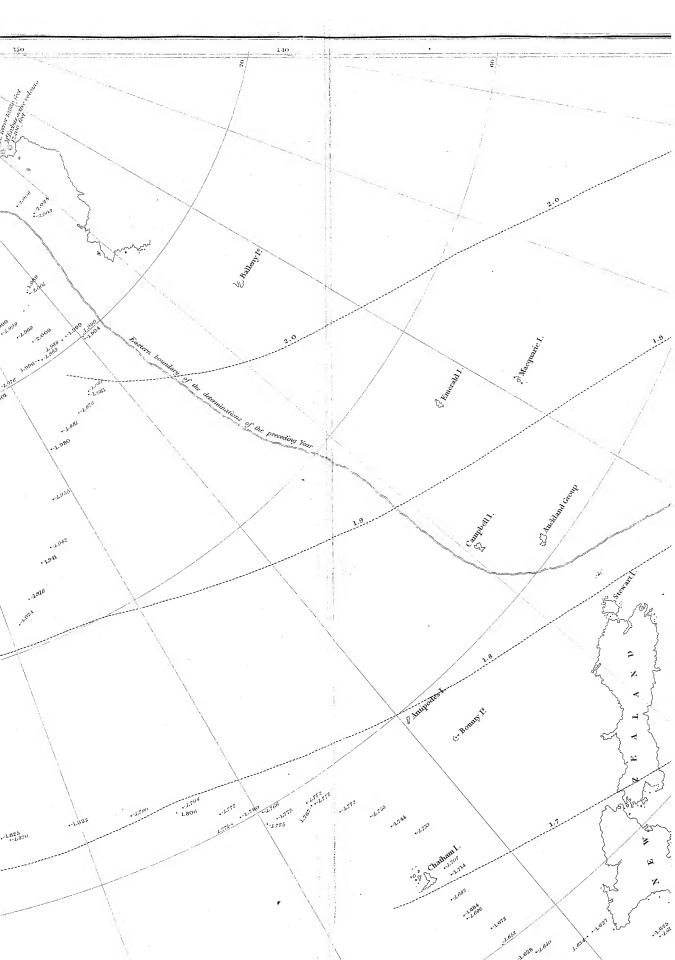


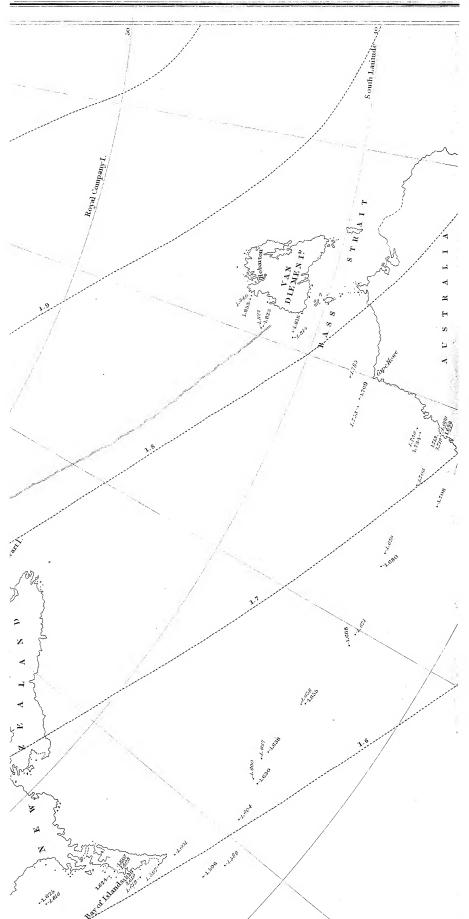


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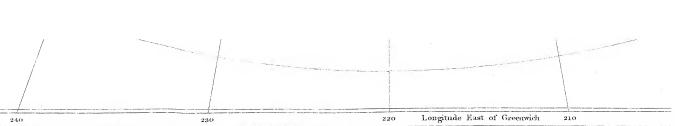


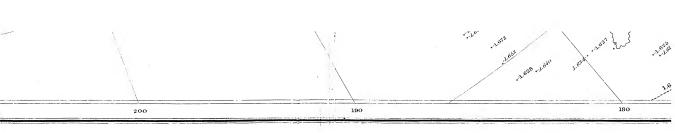


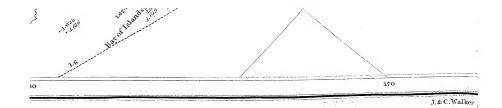












OFT Engraved by J.& C.Walker Phil. Trans. MDCCCXLIV. Plate XIII. Longlade East of Greenwich M.Gauss's fleoretical Lines
Lines deducal jron the Observations of the Antarctic Expedition 18 80 200 80 20 220 260 240

PLATE SHOWING THE LINES OF EQUAL INTENSITY DEDUCED FROM THE OBSERVATIONS OF THE ANTARCTIC B""EDITION IN COMPARISON WITH M. GAUSS'S THEORETICAL LINES.

Plate, shewing the progressive westerly movement of the Magnetic Phenomena in the Southern Pacific Ocean.

1. Between the Longitudes of 270° and 340° East.

